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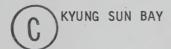




THE UNIVERSITY OF ALBERTA

AN EMPIRICAL INVESTIGATION OF THE SAMPLING DISTRIBUTION OF THE RELIABILITY COEFFICIENT ESTIMATES BASED ON ALPHA AND KR20 VIA COMPUTER SIMULATION UNDER VARIOUS MODELS AND ASSUMPTIONS

by



A THESIS

SUBMITTED TO THE FACULTY OF GRADUATE STUDIES AND

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ABSTRACT

The exact sampling distribution of reliability estimates of a composite test is known only for the case when the test scores of the parts can be expressed in a linear model and satisfy all the assumptions of the two way mixed model ANOVA with one observation per cell including normality of true and error scores. For more general cases, the sampling distributions have been in general unknown or ignored by the psychometricians.

This study examined the more liberal concepts of test theory and reliability in terms of the underlying models and assumptions, and investigated the sampling distribution of reliability estimates by performing a number of computer simulated sampling experiments under various models and distributional assumptions for true and error scores. The models employed were a mixed model ANOVA, essentially τ equivalent measurements, congeneric and multi-factor true score models for continuous cases, and the normal ogive model for binary item cases. For the distribution of true or latent and error scores, uniform, normal and exponential distributions were used.

The most general model was found to be a multi-factor true score model and all others could be shown to be special cases of this model. The most important factors influencing the sampling distribution are found to be uni-factorness and normality of true scores for continuous cases, and homogeneity of item difficulty parameters for binary cases. The distributions of error scores were found to be unimportant for both cases.

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To determine the robustness conditions of the traditional F-test, the empirical distributions obtained by the sampling experiments were compared with those theoretical distributions obtained under the ANOVA and normal theory model. A number of conditions for robustness are given.

A new formula for the standard error of reliability estimates is introduced by analytical means and the validity of the formula was examined through computer simulated experiments. The new formula was found to be superior to traditional formulas based on normal theory when the normality of true score is not valid. Though the formula is derived under the ANOVA model, it was also found to be better than the traditional formulas under more general models.

Implications of these findings to test theory and applications are discussed and some numerical examples are given to show how the findings and the computer programs developed might be applied in practical situations.

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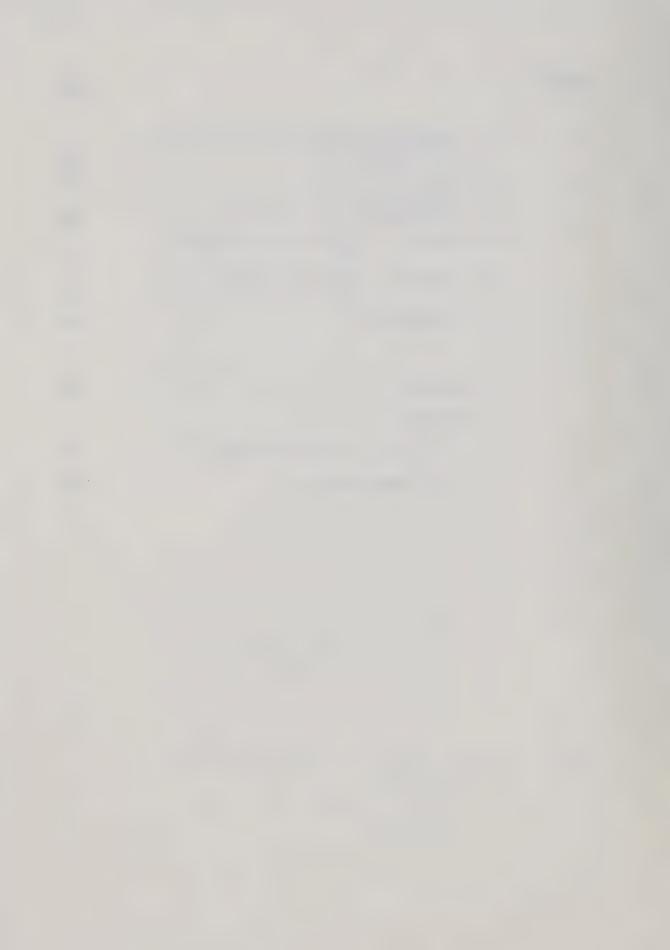
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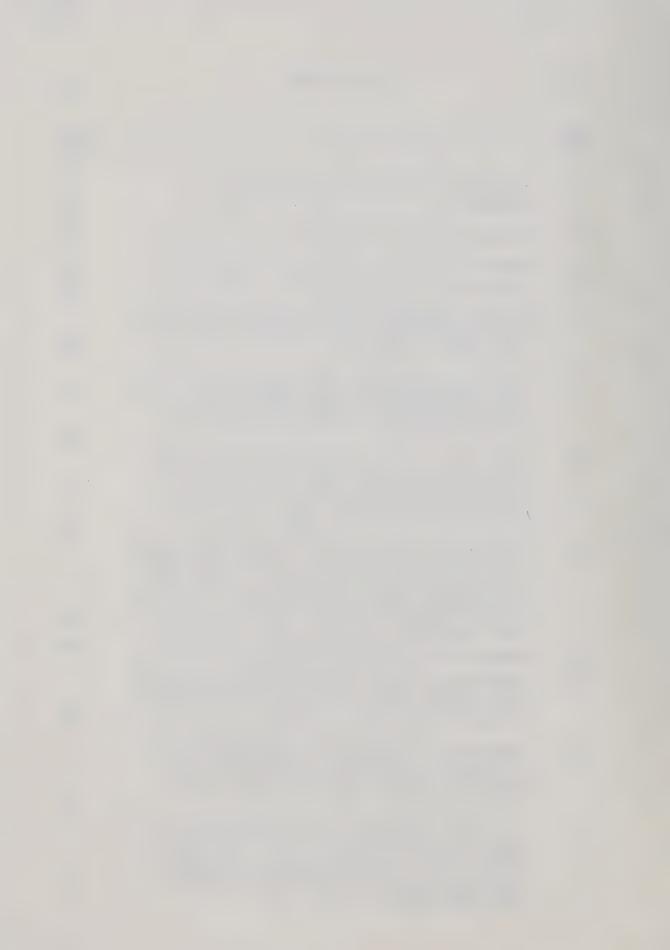


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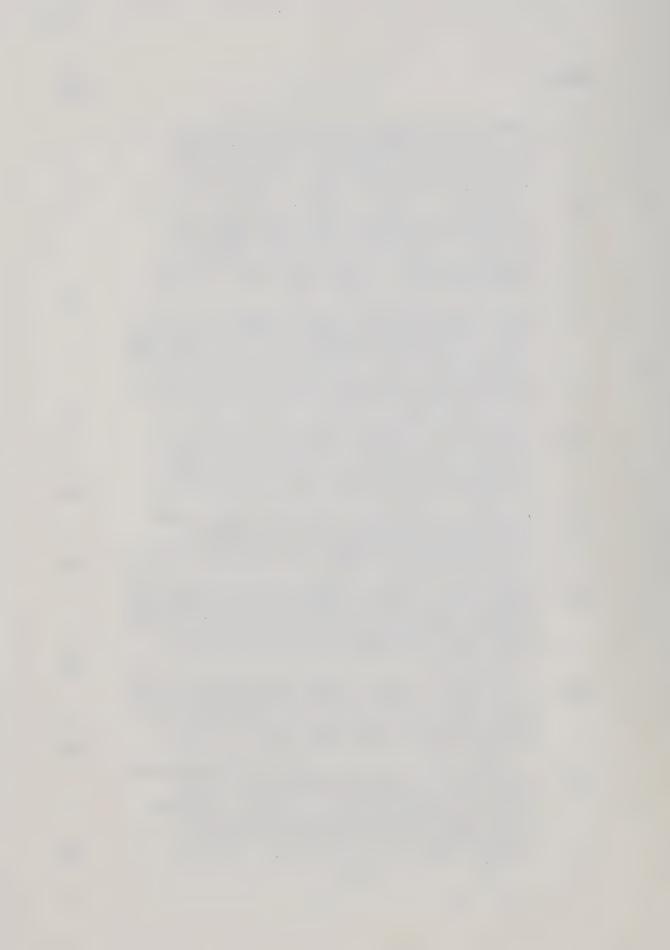


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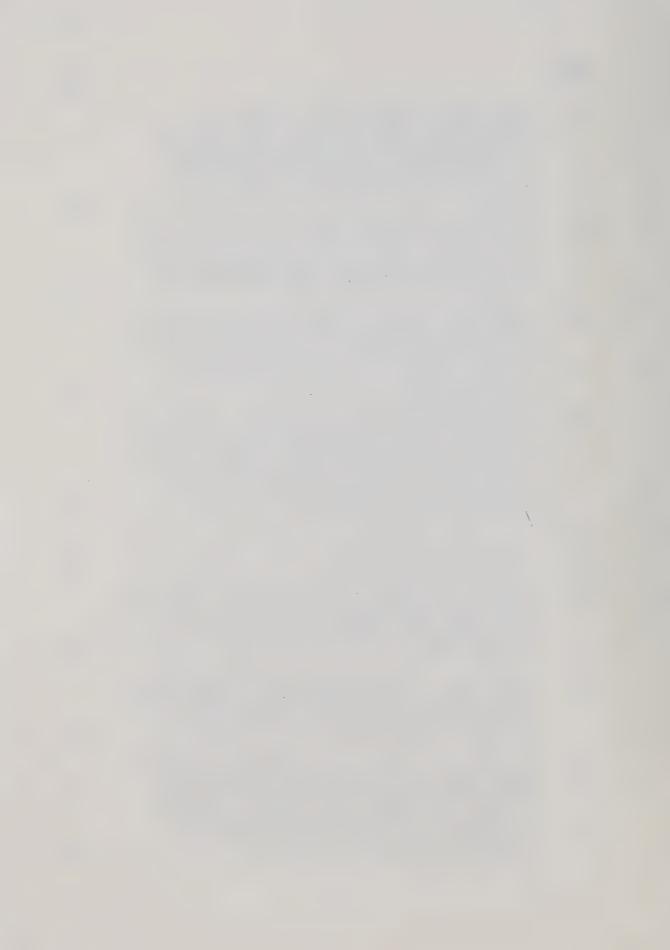
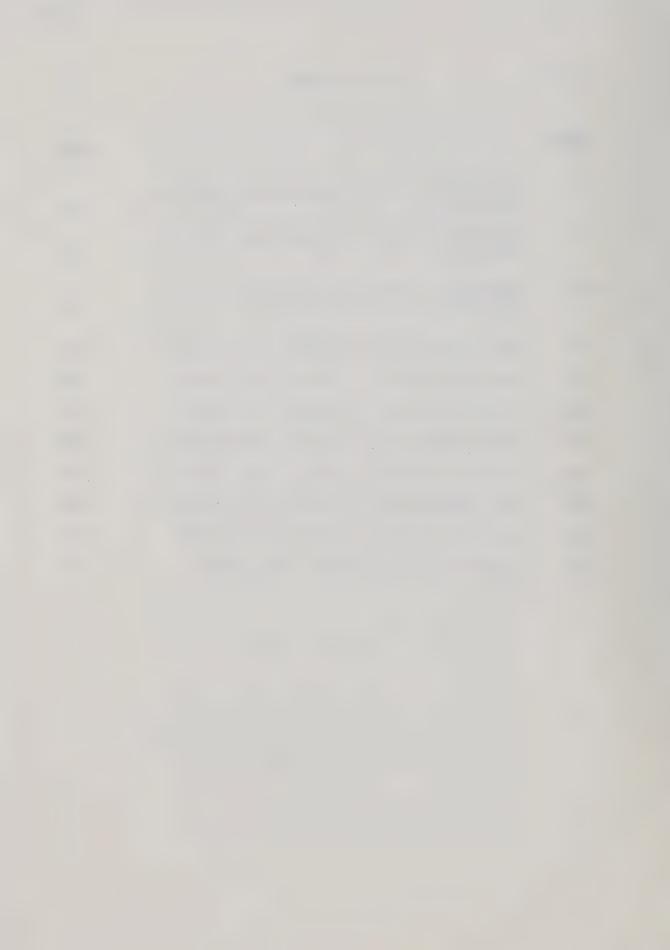


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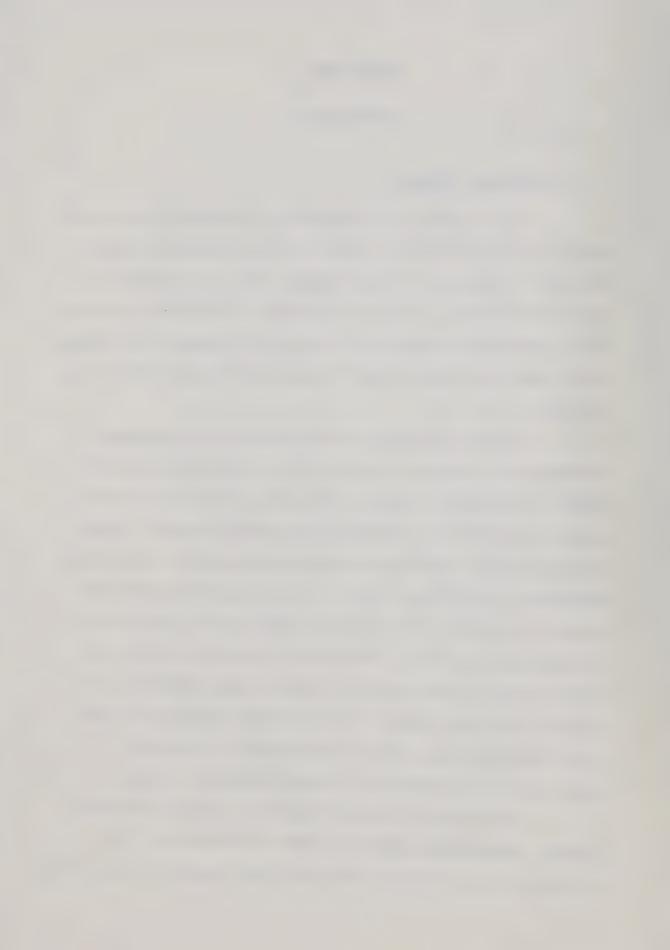
INTRODUCTION

1.1.0 The General Problem

The estimation and interpretation of reliability has been a central issue for psychometric theorists and test authors as well as the users of educational and psychological tests. The reliability coefficient of a test, a population parameter, is defined as the ratio of the true score variance due to individual differences of the subjects, to the total test score variance in a population for which the test is developed.

A number of formulas for measuring reliability have been derived by many theorists since the initial formulation by Spearman (1910) of his theory of true and error scores. Most of the formulas express reliability as a function of the moments of the part scores and the total test scores under assumptions of parallel or equivalent measurements among the part tests, or, as a correlation coefficient between the observed test scores and a second set of scores on a real or hypothetical variable. In most cases, the formulas involve only point estimation of the reliability, and have been obtained by substituting the sample moments of the part-scores and the total scores into formulas which are valid in the population. Statistical properties of such estimates are in general unknown or ignored.

Investigation of the distribution of reliability estimates requires a mathematical model and a number of assumptions. The validity of the estimates of reliability largely depends on the validity



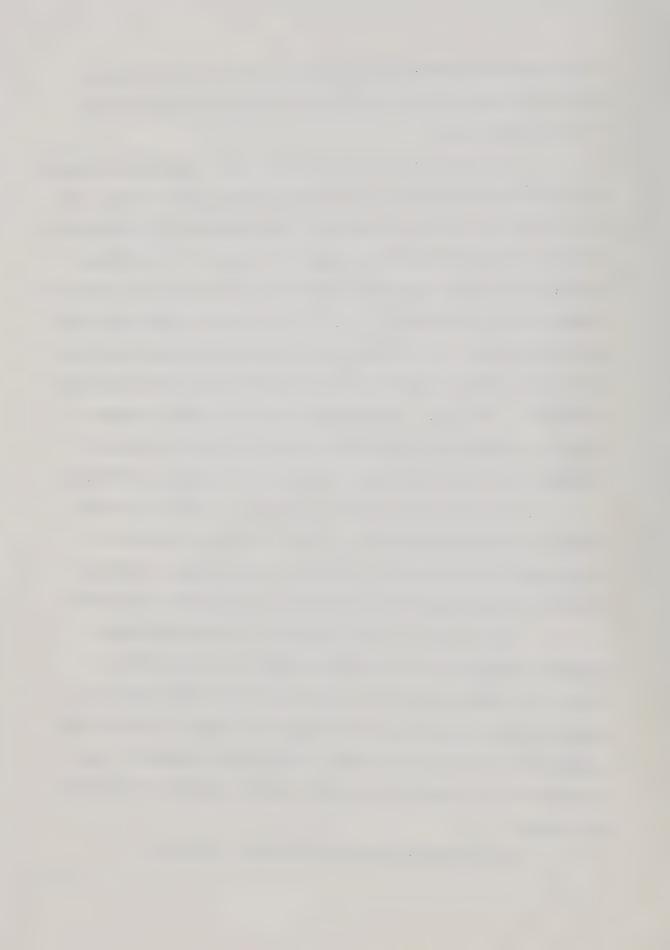
of the model and underlying assumptions. Even for rather rigorous models and assumptions the sampling distributions are unknown except in some special cases.

For a valid statistical inference about a population parameter the sampling distribution of the parameter estimate must be known, and the reliability cannot be an exception. For example, if a standardized test has been administered to a sample of subjects, it is sometimes necessary to compare the sample reliability estimate with the reliability claimed by the test authors, i.e., it is desirable to know whether the difference between the two values can be attributed to sampling fluctuations, or, whether there is a significant difference due to population difference. If a test is administered to two independent samples of subjects, a comparison of the two estimates of reliability may be necessary to determine the underlying cause of any observed difference.

The standard error of the reliability estimate is another useful measure of the precision of the estimates, but without any knowledge of the sampling distribution of the estimates, confidence intervals for the population reliability are impossible to calculate.

Most of the available formulas for reliability estimate depend on the estimation of variance components, using various, explicit or implicit, parallel or equivalent test form assumptions among the part test scores. Even though the estimates of the variance components thus obtained are usually unbiased, the estimates of the reliability are, in most cases, biased, and the statistical properties are unknown.

Since the early years of test theory, it has been



recognized by theorists and test users that the calculated reliability is, in fact, nothing more than an estimate of the true or population reliability, and therefore subject to sampling fluctuations. Even with this recognition, little work has been done to investigate the distribution of such estimates.

This study will investigate properties of the sampling distribution of reliability estimates based on Alpha or KR20 formulas using computer simulation techniques, and will employ various models and distributional assumptions for true or latent, and error scores described in the following two chapters.

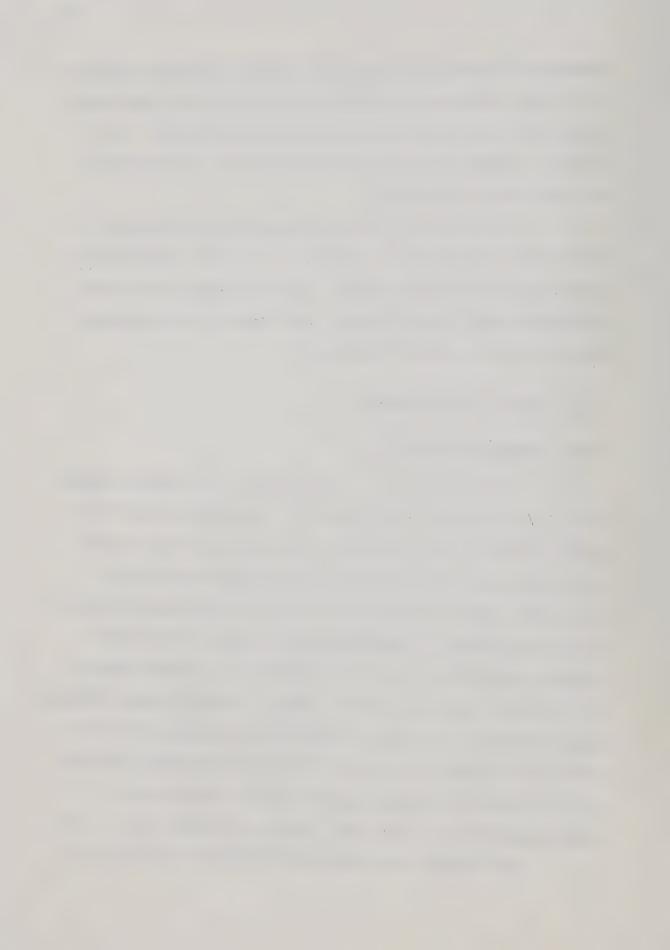
1.2.0 Review of Related Studies

1.2.1 Concepts of Reliability

Even during the initial developments of test theory, psychologists showed interest in the formula for the standard error of reliability estimates as an indicator of the precision of such estimates.

During this period most psychologists interpreted reliability as a correlation coefficient between classically defined parallel measures. Using this definition, attempts were made to apply the well known sampling distribution of correlation coefficient with the assumption of a bivariate normal distribution. However, unlike the usual inference about correlation coefficients, in most cases, the population reliability is considered to be close to unity rather than zero, and hence its distribution has extreme negative skewness making the usual normal approximation of little use (Jackson and Ferguson, 1941, p. 12).

When the split half method was introduced, the reliability



estimate was seen to depend on the way the test was split. As a result, the reliability estimate based on Alpha or KR20 was considered to be superior to the split half estimate since the former gave a unique estimate.

Cronbach (1951) has shown that Alpha or KR20 is an average of all possible split half reliabilities in the population. He thoroughly investigated the coefficient Alpha from the point of view of factorial structure. The Alpha coefficient was interpreted as the proportion of the test variance due to all common factors among the part scores, and as an index of consistency, an estimate of first factor concentration. He also showed that Alpha is a lower bound of the test reliability, but did not explicitly discuss the sampling aspect of the Alpha estimate.

The concept of test reliability has been under continuous change: the classical concept based on parallel tests has been modified and the assumptions relaxed. Burt (1955) and Tryon (1957) initiated a new concept of domain sampling, and the reliability as an index of generalizability has been advocated by Rajaratnam (1960), Cronbach, Rajaratnam and Gleser (1963), and Rajaratnam, Cronbach and Gleser (1965). Their conceptual framework relied heavily on ANOVA models, and initiated a process of liberalization of reliability theory from the rather restrictive classical orthodoxy of test parallelism. However their efforts concentrated on the problem of point estimation, and little attention was paid to sampling aspect of the estimates.

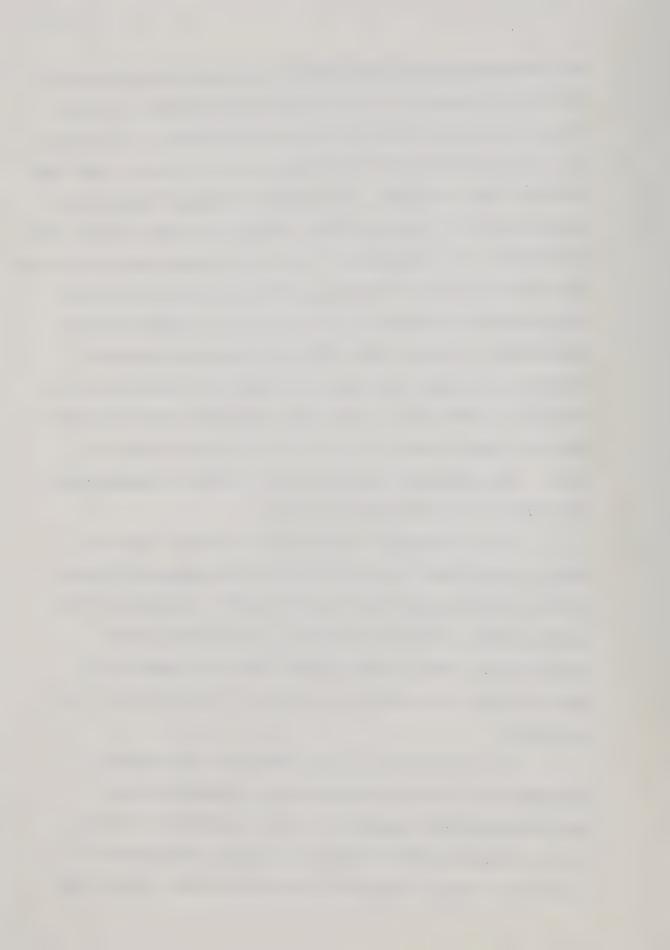
Lord and Novick (1968, p. 50) defined the concept of $\mbox{'essentially} \quad \tau \quad \mbox{equivalent measurements', and Novick and Lewis} \ \, \mbox{(1967)}$



have shown that the coefficient Alpha is identical to the reliability coefficient if and only if a test consists of essentially τ equivalent parts. If this condition is not satisfied Alpha is a lower bound for the reliability, confirming previous studies of Guttman (1945, 1953), Cronbach (1951), and others. To evoke the principle of essentially τ equivalent parts, it has been argued that only true score variances need be identical, i.e., homogeneity of true score variances, and not identical error score variances nor identical true scores among the part tests. The assumptions of classical parallel tests are, therefore, relaxed substantially. Jöreskog (1968, 1970, 1971) defines the concept of congeneric test scores which measure the same trait except for errors, relaxing the essentially τ equivalent measurement conditions further. Under this model any pair of such tests have linearly related true scores. The sampling distributions of the reliability estimates under these models are not yet generally known.

As an alternative to conventional uni-factor true score models, a multi-factor true score model has been advocated by LaForge (1965) using the multiple factor analysis model. An estimate of the squared multiple correlation of a part score with the scores of remaining parts, which is one estimate of the test communality in factor analysis, is proposed as an estimate of the reliability of the part score.

For certain kinds of tests, especially in the field of achievement tests, this approach seems more reasonable than the conventional uni-factor approach, but the old controversial problem of determining the number of factors in a factor analysis must still be resolved. However, the multi-factor model provides a general model



for computer simulation purpose, as will be seen in the next chapter, since the ANOVA and other models may be considered as special cases of the multi-factor model.

1.2.2 Sampling Theories of Reliability Estimates

Lord (1955) defined three kinds of sampling arising in test theory; sampling of subjects (Type 1), part tests or items (Type 2), and a simultaneous combination of the two (Type 12). Lord also discussed the sampling distribution of KR20 under Type 2 sampling without the presentation of the standard error of the KR20 estimates in terms of the population parameters.

A statistical sampling theory of the reliability estimates has been made possible through the application of ANOVA techniques to test theory. Hoyt (1941), Jackson and Ferguson (1941), Ebel (1951), Burt (1955), Cronbach, Rajaratnam and Gleser (1963), Feldt (1965, 1969), Maguire and Hazlett (1969) and many others investigated the reliability estimate under some form of ANOVA models. However, most of their discussion was limited to point estimation and little attention has been paid to the sampling fluctuation of the estimates or interval estimates.

Since the ANOVA models usually provide unbiased, consistent estimates of the variance components by some linear combination of various mean squares, the reliability estimates thus obtained are in general consistent estimators. But, in most cases, they are biased and do not have the desirable minimum variance property.

Although Jackson and Ferguson (1941, p. 40) related the F-statistic to the so called 'sensitivity of a test', or the square



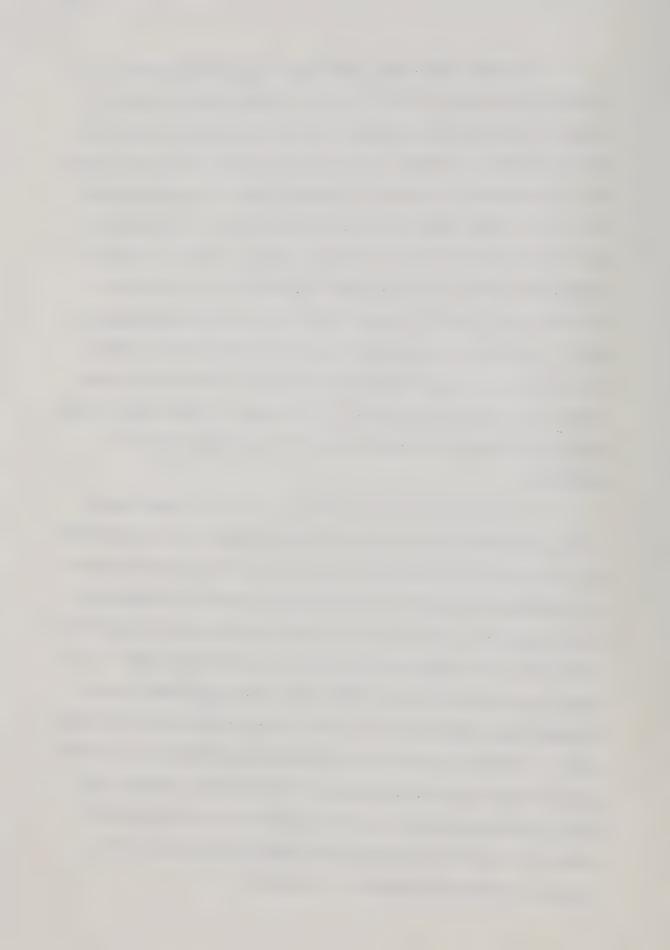
root of the commonly referred signal-noise ratio, it was Ebel (1951) who first explicitly linked the sampling distribution of the reliability estimate itself to an F-statistic. He applied the concept of 'intra-class' correlation coefficient to a rating data set, and by employing the well known F-distribution, has shown a way to obtain confidence intervals of the population intra-class correlation which he interpreted as the reliability of a judge. However, the assumptions underlying the ANOVA model were not explicitly specified.

Kristof (1963) presented a rather complete sampling theory of reliability estimates within the context of the assumptions of classical reliability theory with the exception that the means of the part tests were allowed to be different, i.e., the part test scores are 'essentially' parallel measurements. Under Type 1 sampling and the assumption of a multi-normal distribution of the part test scores, a maximum likelihood estimator of the common correlation among the parts was obtained, i.e., the intra-class correlation coefficient. It was shown to be biased. A bias-free formula was introduced and the sampling distribution of the estimates based on this formula is shown to be related to the F-statistic. A method of statistical inference about the intra-class correlation, which was interpreted as the reliability of a part test, was suggested. Kristof's results are in close agreement with those obtainable under an ANOVA model. He has also showed that the estimate of the Alpha coefficient, in terms of second moment sample statistics, is the same as the maximum likelihood estimator of the reliability when a test has been divided into essentially parallel parts, with an assumption that the parts have a multi-normal distribution.



Kristof (1964) also investigated the distribution of reliability estimates for the first time without relying on the classical equal variance assumptions among the part test scores. A working formula for testing the significance of the difference between the two reliability estimates was derived under the assumption that each part has been administered to the same sample of subjects and that each part test could be split into parallel halves. He also investigated (1969, 1970) the sampling distribution of reliability estimates under the multi-normal assumptions when a test has been split into two parts not necessary parallel in the classical sense. A likelihood ratio test of the point hypothesis concerning the population value of Alpha was derived. This method was then used to yield confidence intervals for the parameter for any chosen level of confidence.

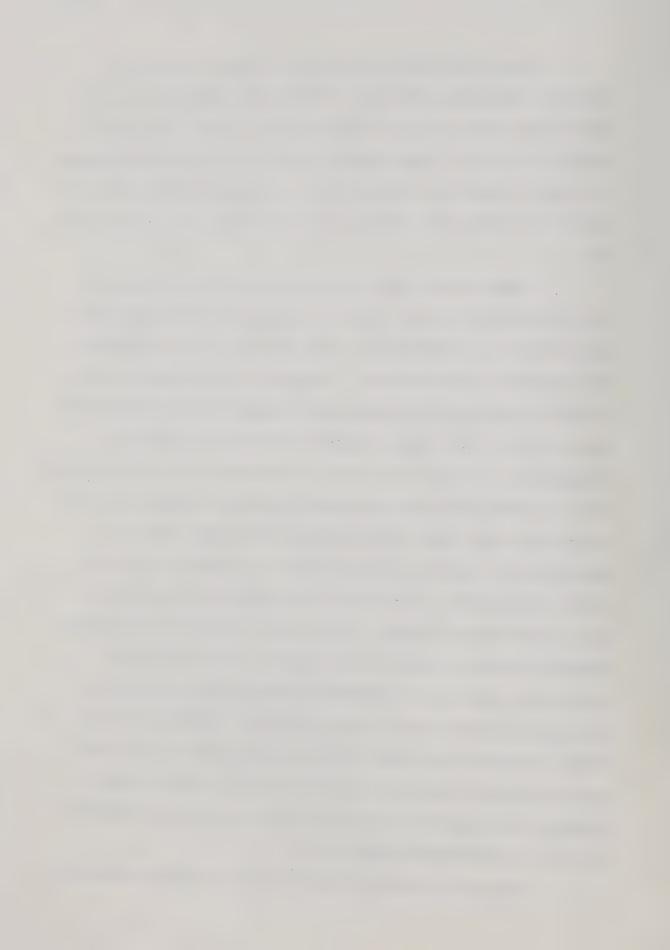
For the case where the parts of a test are simply binary items, the sampling distribution of KR20 estimates is more complicated than the case of continuous part scores. Most theorists have assumed an intermediate hypothetical variable between the item response and underlying true or latent trait score and linked the two variables with the help of the intermediate variable and a mathematical model. Lord (1952), and Lord and Novick (1968) used a normal ogive model, while Birnbaum (1967, 1968) proposed logistic, Poisson and other mathematical models. Although the latent trait approach provides means for investigation of the relationships among the item parameters and the test scores, nothing analytical has yet been done for the distributional theory of reliability estimates or its application even with the restrictive mathematical models and assumptions.



Aoyama (1957) has given explicit formulas, in terms of population parameters without any distributional assumptions, for the expected value and variance of KR20 estimates for Type 1 and Type 2 sampling situations. These results clearly indicate that the estimates are biased. However the formulas involve some approximations and calculation of higher order moments, and are too complex for any practical use.

Since the exact sampling distribution of KR20 estimates is not obtainable by analytical means, some researchers have attempted to approximate it by an ANOVA model. Feldt (1965) has investigated the applicability of the ANOVA model. He pointed out that imposition of a one-zero scoring scheme violates such assumptions of the ANOVA model as continuity of the scores, homogeneity of error variances and independence of true and error scores. He compared the results obtained under the ANOVA model with an empirical distribution based on real data reported by Baker (1962), and claimed the model robust when the assumptions are violated. Feldt referred to the model as a two way random effects model, but actually it was a mixed model as will be seen in the following chapter. Further applications were made of the method by deriving a scheme for testing the equality of two KR20 coefficients based on two independent samples using an approximate distribution of the product of two independent F-statistics (Feldt, 1969). Cleary and Linn (1968) adopted the same method as Feldt and gave an explicit formula for the standard error of KR20 estimates. However, their results are heavily dependent on normality assumptions which are not satisfied for KR20 cases.

Except for the case of approximation by employing unrealistic



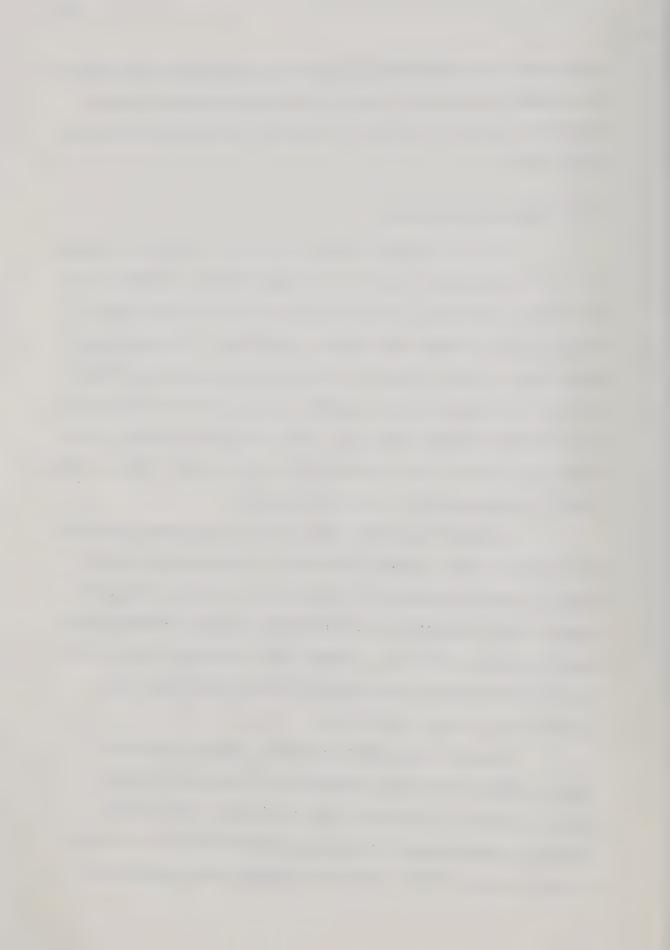
assumptions of the ANOVA model for essentially parallel tests, most of the attempts to obtain the sampling distribution of KR20 estimates have either failed or resulted in unuseable formulas such as given by Aoyama (1957).

1.2.3 Empirical Approaches

The use of empirical approach to solve a statistical problem is as old as statistics itself. For example "Student" (1908) derived the analytic expression for the t-statistic and also established the validity of his argument by a sampling experiment. In education and psychology, a number of empirical investigations have been performed, with or without the help of a computer, to ascertain the robustness of the F-test when certain assumptions underlying an ANOVA model are not satisfied. Norton (1950), Boneau (1960), Hsu and Feldt (1969), and Bay (1970) are some examples of such investigations.

In reliability theory, Baker (1962) investigated a sampling distribution of KR20 estimates under Type I sampling constraints by actually performing experiments using real test results. Payne and Anderson (1968) tabulated the sampling distribution of KR20 estimates based on computer simulation. However, their experiments were limited to the cases of equal item difficulty parameters and inter-item correlations, i.e., phi coefficients.

Nitko and Feldt (1969) performed a computer simulation study of KR20 estimates and reported that, in contrast to general belief, the effect of item difficulty is minimal. Nitko (1968) employed the same method to investigate power functions for the test of significance of KR20 in one and two sample cases as proposed by



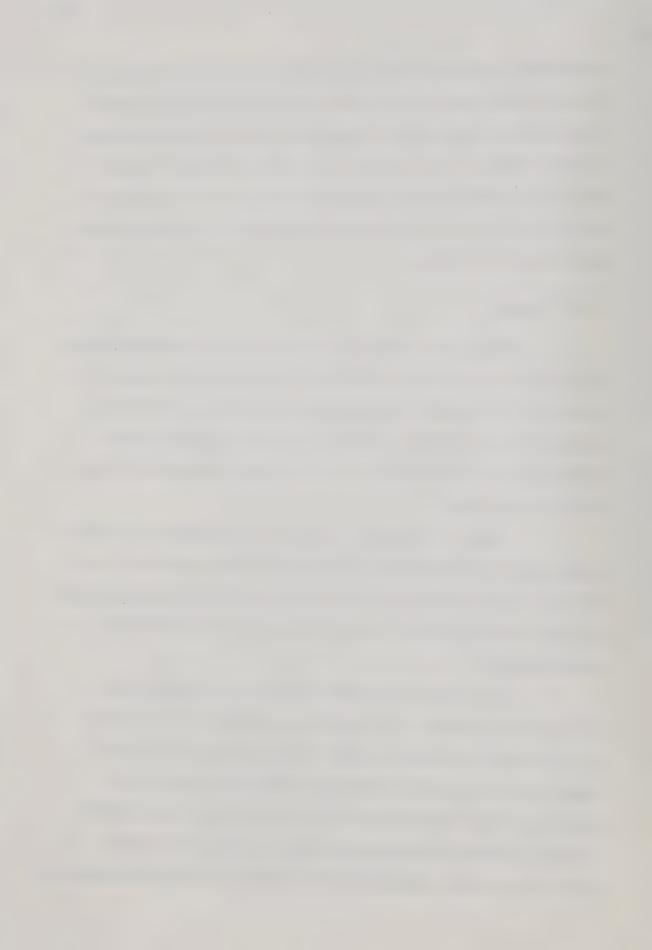
Feldt (1969). Weitzman (1967) reported the result of a simulation of test-retest reliability of a multi-choice test assuming a beta distribution of true scores. Shoemaker (1966) also used a computer simulation model to investigate the estimate of Cronbach's generalizability coefficient for unmatched data to clarify the extent to which stratification must be taken into account in the choice of the generalizability formula.

1.2.4 Summary

Recently, the concept of reliability has been modified and the restrictive classical assumptions of parallel tests relaxed substantially. However, the sampling distribution of reliability estimates based on Alpha or KR20 formulas are in general unknown except for the case when the unrealistic ANOVA model and underlying assumptions are used.

A number of fragmental attempts have been made recently to investigate the distribution by empirical methods, but there is no overall study into the statistical properties of the distribution under the more liberal concept of reliability either by analytical or empirical means.

The purpose of the present study is to investigate the statistical properties of the sampling distribution of reliability estimates when the classical parallel tests or more recent ANOVA models and the assumptions underlying these models are not all satisfied. More liberal concepts of reliability are to be examined in terms of models and assumptions underlying them, and sampling distributions under these models with various distributional assumptions

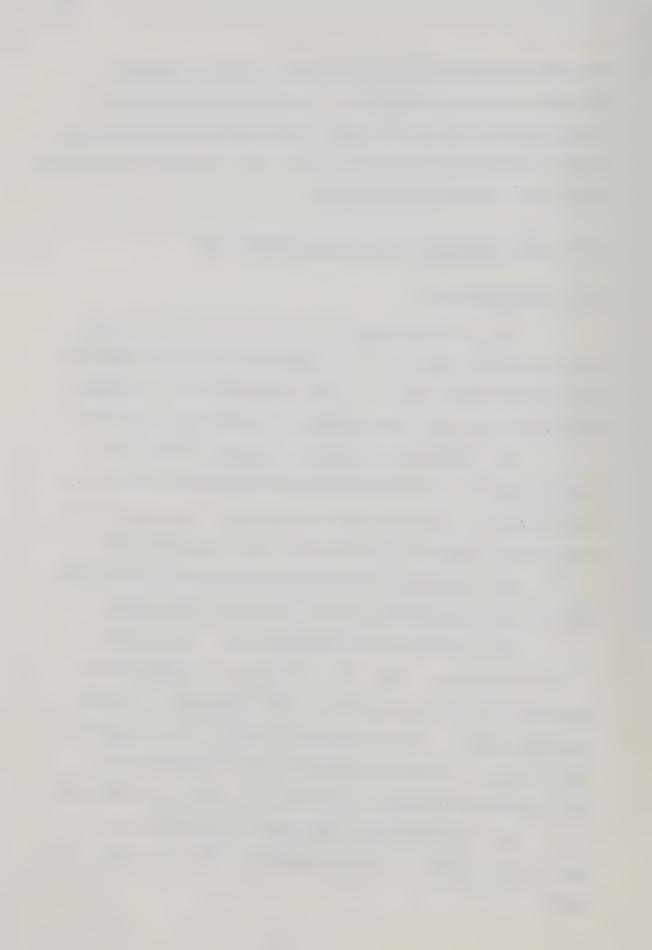


not necessary normal will be investigated by employing computer simulated statistical experiments. Comparisons are to be made of these results with those obtainable theoretically from the ANOVA model and normal theory to see the robustness of the theoretical distributions against the violation of assumptions.

1.3.0 Some Preliminary Specifications and Notations

1.3.1 Specifications

- (a) With some exceptions, Greek letters will be used to denote population values, while the observations and sample quantities are denoted by Roman letters. To make notation simpler, no attempts are made to distinguish random variables from their observed values.
- (b) Scalars will be denoted by capital and lower case letters, matrices will be denoted by underlined capital letters, and column vectors by underlined lower case letters. Row vectors will be indicated by transpose of column vectors, i.e., by priming them.
- (c) An estimator of the population parameter and its value will be indicated by placing a caret or 'hat' over the parameter.
- (d) The normal distribution with mean μ and variance σ^2 will be denoted by $N(\mu, \sigma^2)$. In general, a J-variate normal distribution having a mean vector $\underline{\mu}$ and a dispersion or variance-covariance matrix $\underline{\Sigma}$ will be denoted by $N(\underline{\mu}, \underline{\Sigma})$. The chi-square statistic with n degrees of freedom and the F-statistic with n and m degrees of freedom are denoted by χ^2_n and κ_n respectively.
- (e) The expectation, and dispersion operations for a vector random variable \underline{x} will be denoted by $\underline{E}(\underline{x})$ and $\underline{D}(\underline{x})$, namely,



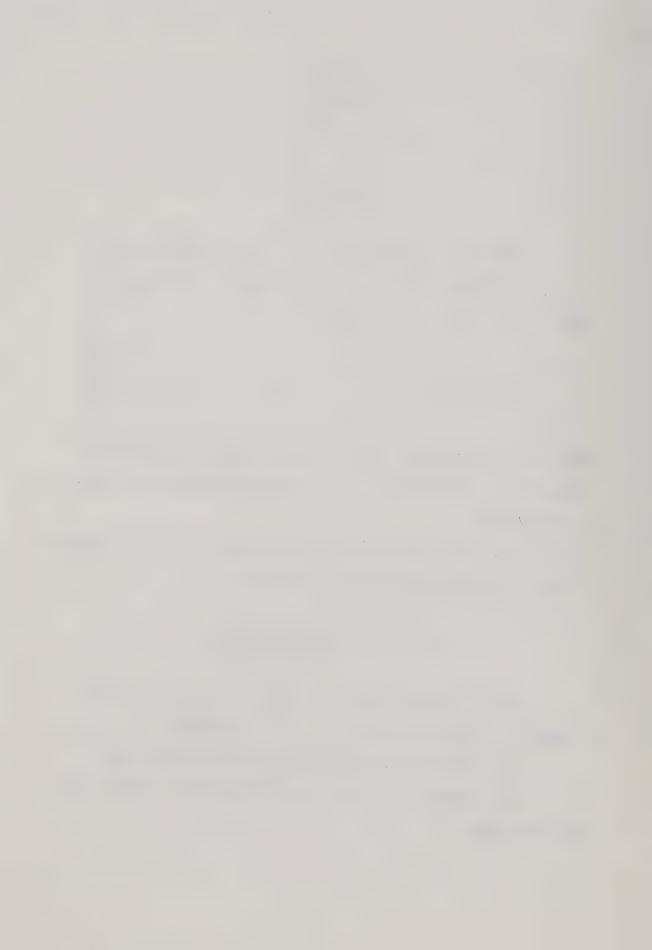
$$E(\underline{x}) = \begin{bmatrix} E(x_1) \\ E(x_2) \\ \vdots \\ E(x_J) \end{bmatrix},$$

where $E(x_i)$, $Var(x_i)$, and $Cov(x_i,x_j)$ denote the usual expectation of x_i , variance of x_i , and covariance between x_i and x_i respectively.

(f) The correlation coefficient between two random variables x and y is denoted by Cor (x,y), namely,

Cor
$$(x,y) = \frac{\text{Cov } (x,y)}{[\text{Var } (x) \text{ Var } (y)]^{\frac{1}{2}}}$$
.

- (g) An identity matrix is denoted by \underline{I} , while a vector of length J whose elements are all 1's is denoted by \underline{I} .
 - (h) Dot subscripts are used to indicate sample means.
- (g) Braces, { }, are used to indicate all elements in a set of variables.



1.3.2 Notations

The following is a brief glossary of important symbols used frequently.

- i indexing subscript for subjects in the sample, i = 1,2,...,I
- k indexing subscript for subjects in population, k = 1, 2, ...
- j indexing subscript for parts (items) of a test, j = 1, 2, ..., J
- I sample size, a fixed constant
- J number of parts (items) in the test, a fixed constant
- y ij the observed score random variable of subject i on the jth part test; it stands for the corresponding response strength variable for the binary item test
- the observed score random variable of subject i on the jth item, takes on values one or zero
- $\tau_{\mbox{\scriptsize i.i.}}$ the true score of subject $\mbox{\scriptsize i}$ on the jth part
- e_{ij} the error score random variable of y_{ij}
- m the true score of subject i after adjustment is made for difference in difficulty levels among the J part tests
- a, the effect or ability level of subject i in deviation form, $\ensuremath{\text{m}}_i\mbox{-}\mu$
- β the fixed effect of jth part, or the threshold constant for jth item; indicates the difficulty level of jth part (item)
- μ the expected value of m_i over the population
- σ_{A}^{2} the variance of m_{i} over the population, assumed to be common to all J parts under ETEM assumption
- the variance of e_{ij} over the replications, assumed to be common to all subjects for all specific part j; defined in terms of response strength variables for the binary case



```
\sigma_e^2 common value of \sigma_{e\,i}^2 among the J parts under the
       homogeneity of error variance assumption
       the unweighted sum of J part scores for subject i
  У:
       the unweighted sum of J items for subject i
       the variance of the jth part (item) score
       the variance of y.
       the variance of x.
       the regression coefficient of y_{ij} on f_i under the uni-
       factor true score model, or the standard deviation of the
       true score of the jth part; the biserial correlation between
       x. and f. for the binary item case
       the tetrachoric correlation between items j and j'
 \gamma_{ii}
       the inter item correlation coefficient between items j and j'
 Pril
       standardized error random variable, i.e., e_{ii} = \sigma_{ii}
  εii
  f,
       standardized true score random variable for continuous
       case i.e., a_i = \sigma_{\Lambda} f_i; for the binary item case the
       latent or factor score
       the factor loading matrix of size J \times r
  Λ
       the number of factors of the true score
P; (f)
       item characteristic function of the jth item
       item difficulty of the jth item
 \pi_i
```

 $\phi(z)$

 $\Phi(x)$

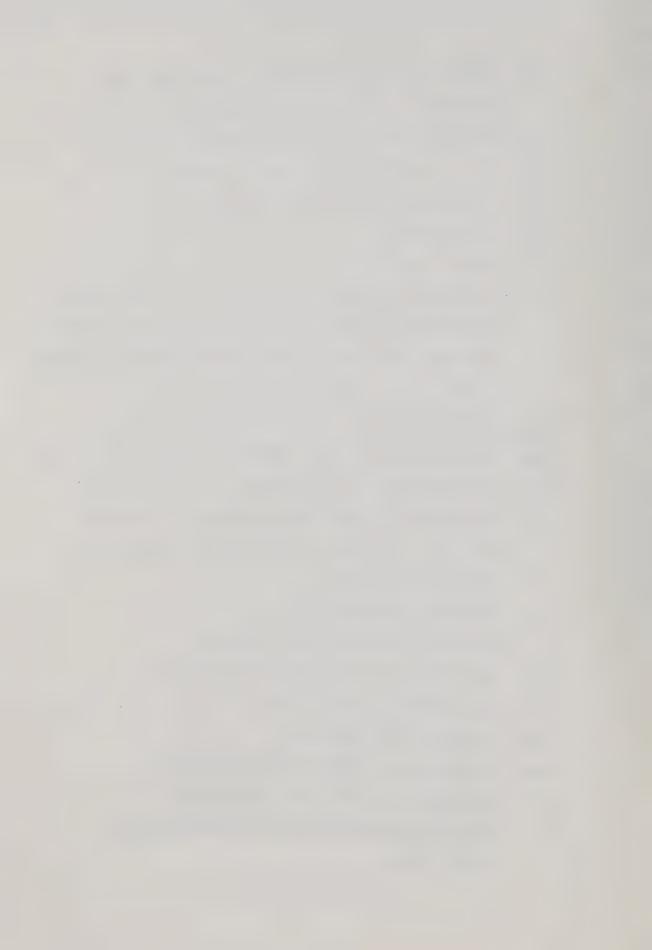
the normal density function

J parts (items)

the cummulative normal distribution function

the reliability coefficient of the jth part

the reliability coefficient of the unweighted sum of

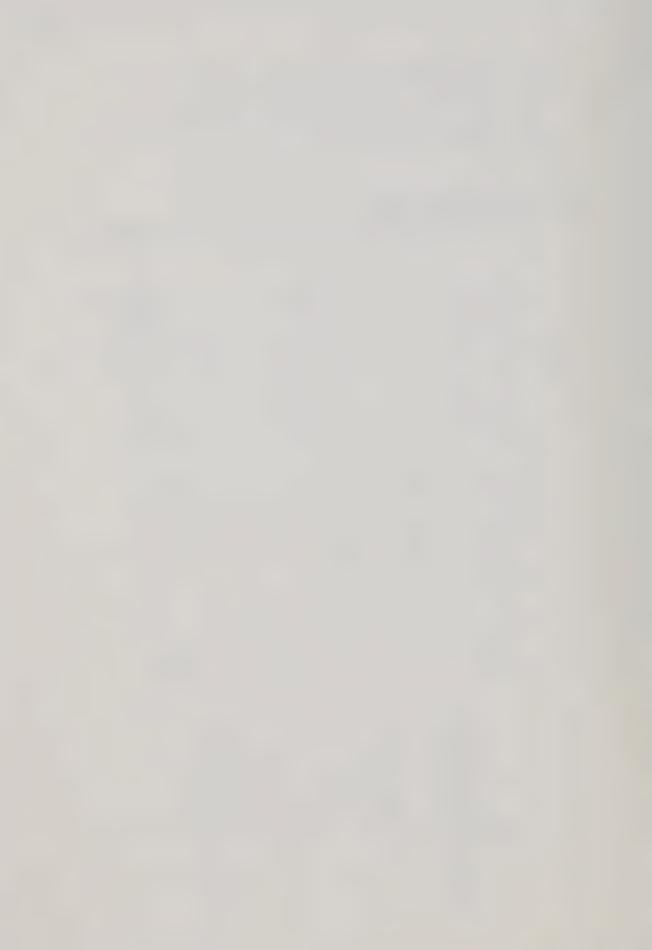


 γ_A the kurtosis of true score a_i or f_i γ_e the kurtosis of error score e_{ij} or ϵ_{ij} γ_y the kurtosis of test score γ_i

1.3.3 Vectors and Matrices

The following vectors and matrices are used frequently.

$$\underline{\mathbf{y}}_{i} = \begin{bmatrix} \mathbf{y}_{i1} \\ \mathbf{y}_{i2} \\ \vdots \\ \mathbf{y}_{iJ} \end{bmatrix}, \quad \underline{\boldsymbol{\varepsilon}}_{i} = \begin{bmatrix} \boldsymbol{\varepsilon}_{i1} \\ \boldsymbol{\varepsilon}_{i2} \\ \vdots \\ \boldsymbol{\varepsilon}_{iJ} \end{bmatrix}, \quad \underline{\boldsymbol{\lambda}} = \begin{bmatrix} \boldsymbol{\lambda}_{1} \\ \boldsymbol{\lambda}_{2} \\ \vdots \\ \boldsymbol{\lambda}_{J} \end{bmatrix}.$$



where λ_{jm} is the factor loading or regression coefficient of y_{ij} on the mth true or factor score under a multi-factor model.

1.3.4 Definitions

The following is a short list of definitions for the most often used terms in this paper.

ANOVA Model

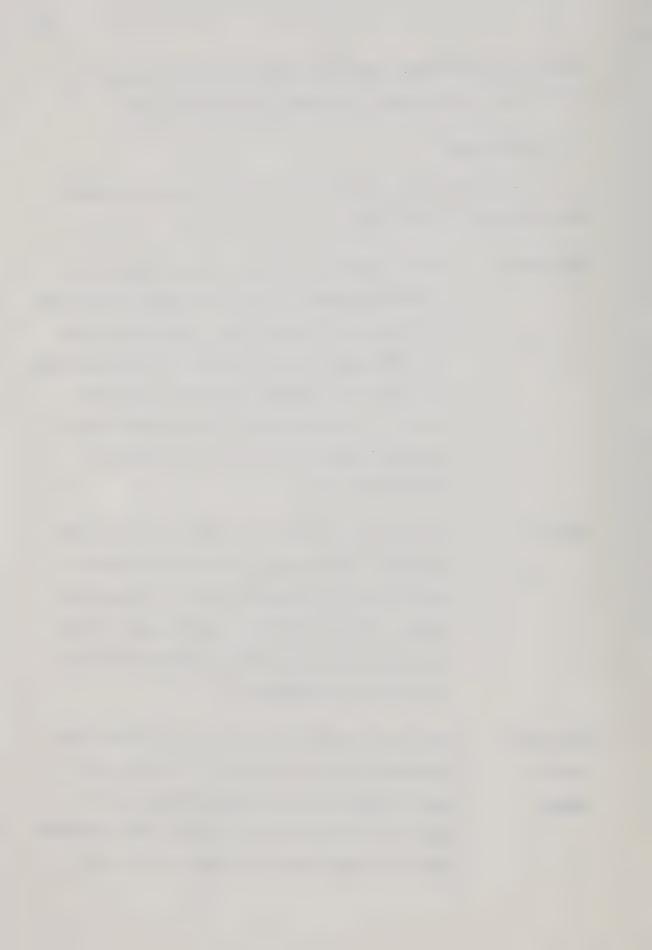
Unless specified otherwise, this term refers to a two way mixed model analysis of variance linear model with one observation per cell. The levels of the row factor stand for the subjects in the sample, and the effects are assumed to be random, while the levels of the column factor stand for part tests or items of a composite test, and the effects are assumed to be fixed.

Parallel

Two measures are said to be classically or strictly parallel if (a) the test score may be considered consisting of two independent parts, true and error scores, (b) true scores are identical, and (c) error and total scores have idenical means and variances for each of the two measures.

Essentially
Parallel
(ANOVA)

The same as parallel measures except that the true scores may differ by a constant. The true, error and test scores have identical variances, but the means of the true scores may differ. Under the ANOVA model, the measurements are essentially parallel.



τ Equivalent

The same as parallel measures except that the variances of the error scores may differ. The variances of test scores may differ, but the means must be equal.

Essentially

τ Equivalent

The same as τ equivalent measurements except that the true scores may differ by a constant. The variances of true scores must be identical, but means and variances of test scores may differ.

Congeneric
True Score

The same as essentially τ equivalent measurements except that the true score is required only to measure a single trait. The true scores of two measures are linearly related, but their means and variances may differ.

Multi-factor (M.F.)

The same as congeneric true score case except that the tests measure more than one trait, i.e., the factorial structure of the true score could be more than one factor.

The above definitions of different but related types of measurements are compared in Table 1.1.



TABLE 1.1

Comparisons of the Definitions of Various Measures

Type of Measures	True Scores			Error Scores		Test Scores	
	Score	Mean ²	Var. ³	Mean	Var.	Mean	Var.
Parallel	14	1	1	0.0	1	1	ı
Essentially Parallel (ANOVA)	D ⁵	D	1	0.0	1	D	ı
τ Equivalent	1	1	1	0.0	D	ı	D
Essentially τ Equivalent (ETEM)	D	D	1	0.0	D	D	D
Congeneric	D	D	D	0.0	D	D	D
Multi-Factor (M.F.)	D	D	D	0.0	D	D	D

Note:

True scores for the same subject.

²Means in the population.

3Variances in the population.

41: Identical among the measures.

 $^{5}\mathrm{D}:$ May differ among the measures.



CHAPTER TWO

TEST MODELS FOR THE CONTINUOUS PART SCORE CASES

Two distinct cases may be considered for a theory of reliability: the first is the case of continuous observed scores for the parts of a test, and the second is the case in which the scores of the parts are 'counter' or 'indicator' variables, i.e., a one is assigned for a correct response and zero for a wrong response. Due to the necessity of a different statistical treatment for each of the two cases, only the continuous case is duscussed in this chapter. The discussion is also limited to Type I sampling situations. The binary item situation will be discussed in the following chapter.

For the continuous score case, ANOVA type linear models are the most powerful and have a wide range of applicability. From among many possible models, the discussion is limited to a two way mixed model ANOVA with one observation per cell. Generalization to other more complex designs is a straight forward matter, however, complexity and difficulty of interpretation is a problem due to interaction effects.

2.1 ANOVA Model

A test consisting of J parts $(J \ge 2)$ is considered under the strict parallelism assumptions among the J part tests except that the means of the J parts may differ by a constant due to the difference in the difficulty levels of the parts. If the test is administered to a random sample of I subjects $(I \ge 2)$, the observed



score of the ith subject in the sample on the jth part, a random variable denoted by y_{ij} , may be written in a linear form in accordance with the classical theory of true and error scores, namely,

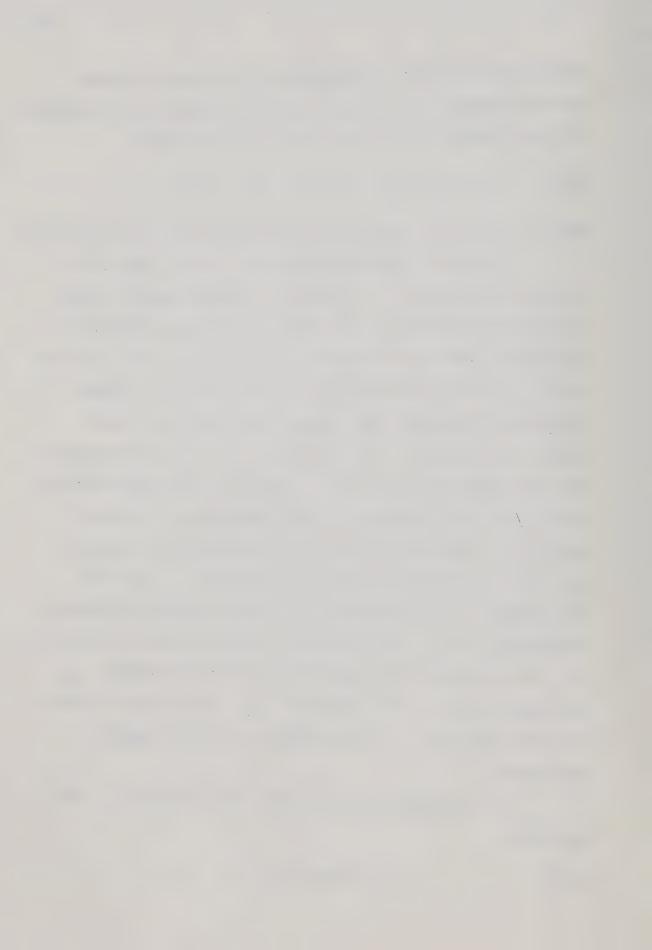
(2.1)
$$y_{ij} = \tau_{ij} + e_{ij}, \quad i = 1,2,...,l; \quad j = 1,2,...,J,$$

where τ_{ij} and e_{ij} denote the true score and error score respectively.

An infinite idealized population of subjects denoted by P, from which the sample of I subjects is supposedly drawn, is hypothesized and the findings on the sample are to be generalized to the population. Labelling the subjects in P as k (k = 1,2,...), the score y_{ki} may be conceptualized as the realization of a random process which may occur under repeated measurements on a single subject, labelled by k, on a fixed part test j with the assumption that the subject does not change or 'learn' over the repeated measurements, that is the replication is under experimentally independent conditions. Then the true score τ_{ki} may be considered the mean of y_{ki} over replications, or the expected value of y_{ki} over the distribution of y_{ki} for fixed k, or over the so-called 'propensity distribution' of yki (Lord and Novick, 1968, pp. 29-30). Mathematically τ_{ki} may be defined as the expectation of the random variable y_{ki} , for given k and j. The elements of yki have a joint distribution with respect to k in the population P and the number of replications.

By the assumption of parallelism, the true score $\boldsymbol{\tau}_{kj}^{}$ may be written,

(2.2)
$$\tau_{kj} = m(k) + \beta_j,$$



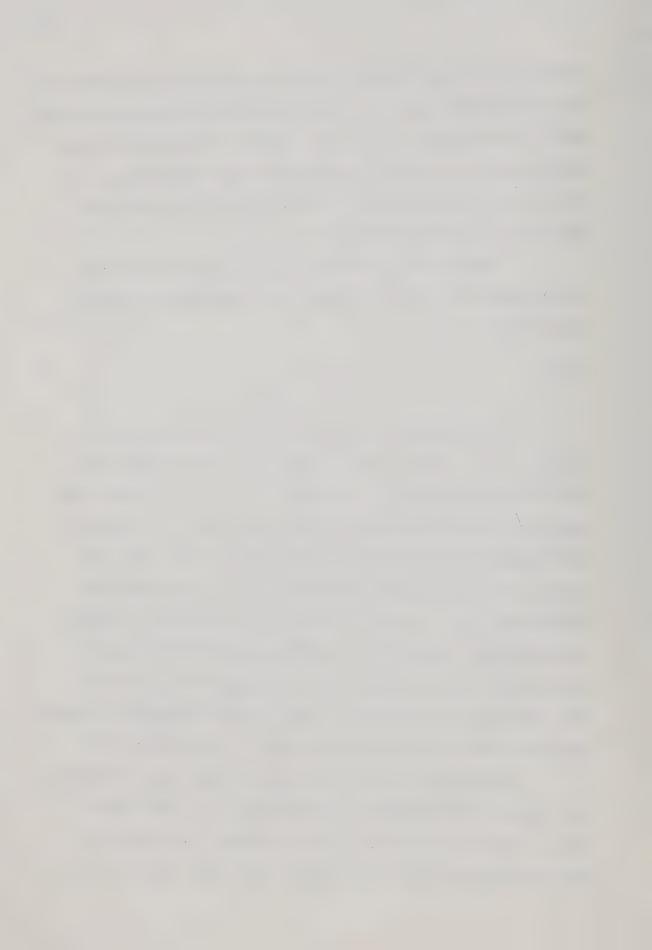
where β_j is a fixed constant specific to the jth part test representing the difficulty level of the part relative to the other parts, and m(k) is the adjusted true score for subject k indicating the real ability level of the subject, and assumed to be independent of j. Thus, m(k) may be considered a random variable with repsect to k distributed over the population P.

Since the $\{\beta_j\}$ indicate only the relative difficulty levels among the J parts, without loss of generality it may be assumed that,

$$(2.3) \sum \beta_{j} = 0.$$

The labels of the subjects in the sample may be given by $\{k_1,k_2,\ldots,k_l\}$, and $m_i=m(k_i)$ where m_i is the adjusted true score of the ith subject in the sample. If μ and σ_A^2 denote the mean and variance of the adjusted true score m(k), then they are the expected value and variance of the random variable m(k) calculated with respect to the distribution of k in the population. Since each of the I subjects may also be considered as a randomly selected subject drawn from I identical populations with mean μ and variance σ_A^2 , one subject chosen per population, each of the $\{m_i\}$ may also be considered as a random variable distributed independently and identically with expected value μ and variance σ_A^2 .

The variance of the error random variable e_{kj} , calculated with respect to the propensity distribution of y_{kj} , for fixed k and j, shall be denoted by $\sigma_{ej}^2(k)$. Although it is conceivable that the brighter subjects with higher m(k) might respond to the



test more consistently over replications, and have smaller variances, for the present discussion, it is assumed that $\sigma_{ej}^2(k)$ is the same for all subjects in the population and the common error variance is denoted by σ_{ej}^2 , which depends only on j. This assumption is rather restrictive, but it is necessary since only one set of part test scores is assumed to be available for each subject in the sample, and therefore $\sigma_{ej}^2(k)$ would not be an observable quantity without this assumption.

Furthermore, following the assumptions of classical parallelism (e.g., Gulliksen, 1950, pp. 14-25), under the ANOVA model, it shall also be assumed that the error scores $\{e_{kj}\}$ have expected value zero and equal variance, denoted by σ_e^2 , for all the J parts, i.e., homogeneity of error variance is also assumed among the part tests. In addition they are assumed to be independently and identically distributed, and independent of $\{m(k)\}$.

The effect of a subject labelled $\,k\,$ in the population is defined as,

(2.4)
$$a(k) = m(k) - \mu$$
,

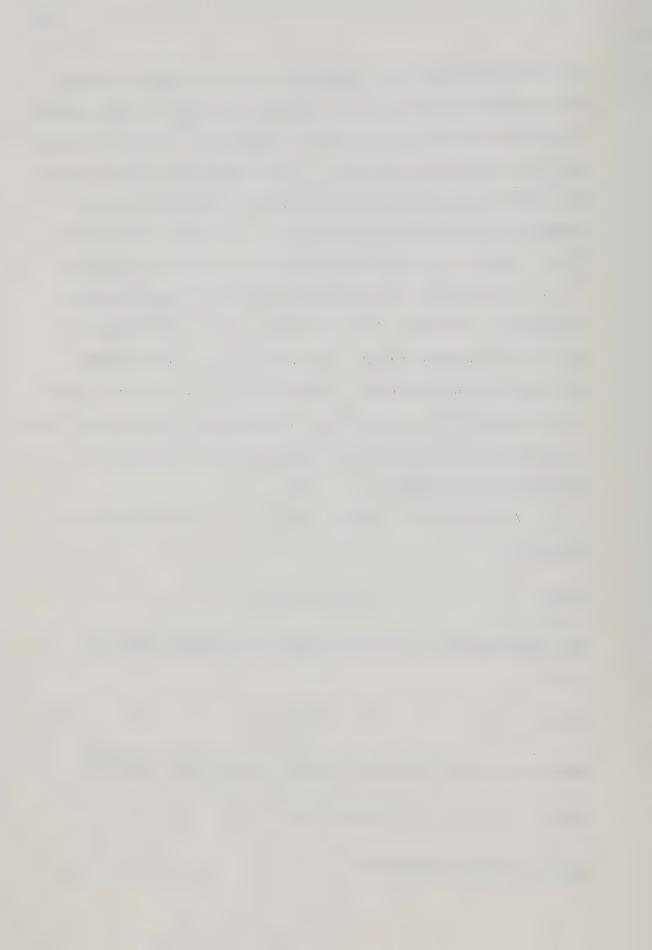
such that the effect of the ith subject in the sample, denoted by a;, is

(2.5)
$$a_{i} = m_{i} - \mu$$
.

Applying (2.2) and (2.5), (2.1) becomes the basic model equation,

(2.6)
$$y_{ij} = \mu + a_i + \beta_j + e_{ij}$$
,

with the following assumptions,



Thus the expected value and variance of an observation y ij is,

(2.8)
$$E(y_{ij}) = \mu + \beta_j; \quad Var(y_{ij}) = \sigma_A^2 + \sigma_e^2.$$

If y_i denotes the unweighted sum of the J part scores for subject i, namely,

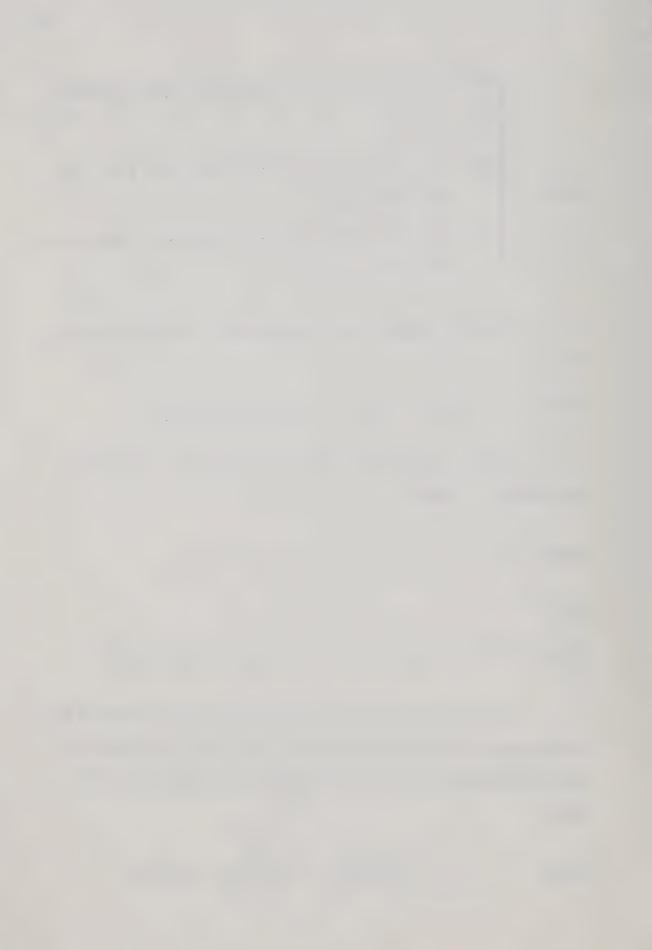
(2.9)
$$y_{ij} = \sum_{j} y_{ij} = J_{\mu} + J_{a_{i}} + \sum_{j} e_{ij}$$
,

then,

(2.10)
$$E(y_i) = J\mu$$
; $Var(y_i) = J^2 \sigma_A^2 + J \sigma_e^2$.

The reliability of a test is defined to be the ratio of the variance due to individual difference or the 'effect' of subjects to the total test score variance (Lord and Novick, 1968, p. 61). For a part j,

(2.11)
$$\rho_{j} = \frac{\text{Var } (a_{i})}{\text{Var } (y_{ij})} = \frac{\sigma_{A}^{2}}{\sigma_{A}^{2} + \sigma_{e}^{2}} = \frac{\theta}{(1 + \theta)} ,$$



where $\theta = \sigma_A^2/\sigma_e^2$ is the so-called signal-noise ratio or the square of sensitivity of a part test score (Jackson and Ferguson, 1941, p. 40).

For the total score,

(2.12)
$$\rho = \frac{\sigma_{A}^{2}}{\sigma_{A}^{2} + \sigma_{e}^{2}/J} = \frac{J\theta}{1 + J\theta} .$$

Because,

Cov
$$(y_{ij}, y_{ij}) = E\{[y_{ij} - E(y_{ij})][(y_{ij} - E(y_{ij})]\}$$

$$= E[(a_i + e_{ij})(a_i + e_{ij})]$$

$$= \sigma_A^2,$$

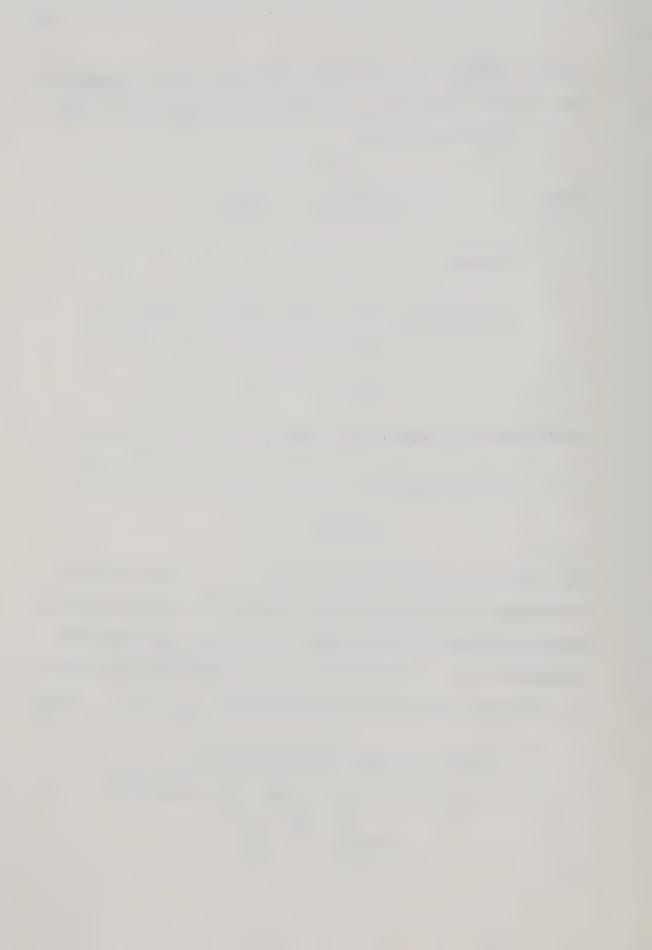
and the correlation coefficient between part j and j' $(j \neq j')$ is

Cor
$$(y_{ij}, y_{ij}) = Cov (y_{ij}, y_{ij})/[Var (y_{ij}) Var (y_{ij})]^{\frac{1}{2}}$$

= $\sigma_A^2/(\sigma_A^2 + \sigma_e^2) = \rho_i$.

The common reliability among the J parts, ρ_j , is the so-called 'intra-class' correlation coefficient which is the ordinary correlation coefficient between the part scores y_{ij} and y_{ij} , under the ANOVA assumptions above. Or alternatively, ρ_j is the square of the index of reliability, which is the correlation between y_{ij} and a_i , since,

Cov
$$(y_{ij}, a_i) = E[(a_i + e_{ij})(a_i)] = \sigma_A^2$$
,
Cor $(y_{ij}, a_i) = Cov (y_{ij}, a_i)/[Var (y_{ij}), Var (a_i)]^{\frac{1}{2}}$
 $= \sigma_A/(\sigma_A^2 + \sigma_e^2)^{\frac{1}{2}} = \rho_j^{\frac{1}{2}}$.



Under this model no assumption of random sampling of parts is required. The models used by Hoyt (1941), Ebel (1951), Winer (1962, p. 124), Lord (1964), Feldt (1965), and Maguire and Hazlett (1969) are essentially the same as this, although some treat the fixed effect $\{\beta_j\}$ as random effects assuming the existence of a population of part tests and random sampling of J parts from it. As has been shown, the assumption is not necessary.

By the usual mathematical presentation (e.g., Scheffé, 1959, p. 261) the unbiased estimator of σ_A^2 and σ_e^2 are given by,

$$\hat{\sigma}_A^2 = (MS_A - MS_e)/J;$$
 $\hat{\sigma}_e^2 = MS_e$,

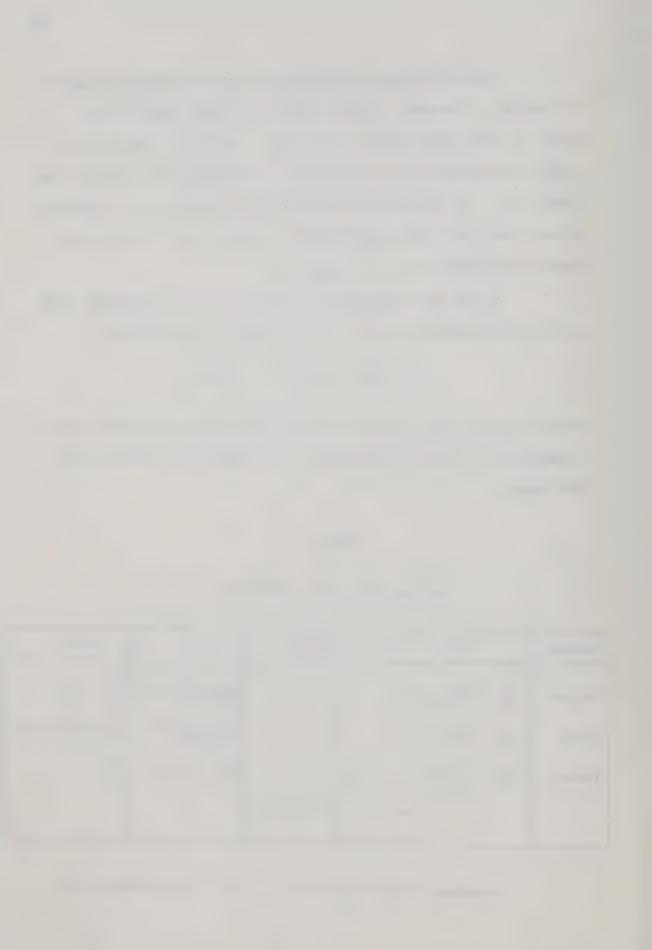
where ${\rm MS}_{\rm A}$ and ${\rm MS}_{\rm e}$ are mean squares for subject effects and errors respectively. They are obtainable from an ANOVA table given as the following:

TABLE 2.1

Two Way Mixed Model ANOVA Table

Source	S.S.	D.F.	M.S.	E(M.S.)
Subject	$SS_A = J\sum (y_i - y_i)^2$	1 - 1	MS _A =SS _A /(1-1)	$\sigma_{\rm e}^2 + J\sigma_{\rm A}^2$
Parts	$SS_{B} = I\sum_{j=1}^{\infty} (y_{j} - y_{j})^{2}$	J - 1	$MS_B = SS_B/(J-1)$	$\sigma_{e}^{2}+I(\sum_{\beta}\beta_{j}^{2})/(J-1)$
Errors	$SS_{E} = \sum_{i} \sum_{j} (y_{ij} - y_{i} - y_{j})$	ν =	$MS_e = SS_e/v$	σ <mark>2</mark>
	+y) ²	(I-1) (J-1)		

Therefore if the reliability ρ_i or ρ is estimated by



substituting the unbiased estimator of variance components into (2.11) or (2.12),

(2.13)
$$\begin{cases} (a) & \hat{\rho}_{j} = \frac{\hat{\sigma}_{A}^{2}}{\hat{\sigma}_{A}^{2} + \hat{\sigma}_{e}^{2}} = \frac{MS_{A} - MS_{e}}{MS_{A} + (J-1)MS_{e}} = \frac{F-1}{F+J-1} \\ (b) & \hat{\rho} = \frac{\hat{\sigma}_{A}^{2}}{\hat{\sigma}_{A}^{2} + \hat{\sigma}_{e}^{2}/J} = \frac{MS_{A} - MS_{e}}{MS_{A}} = 1 - 1/F, \end{cases}$$

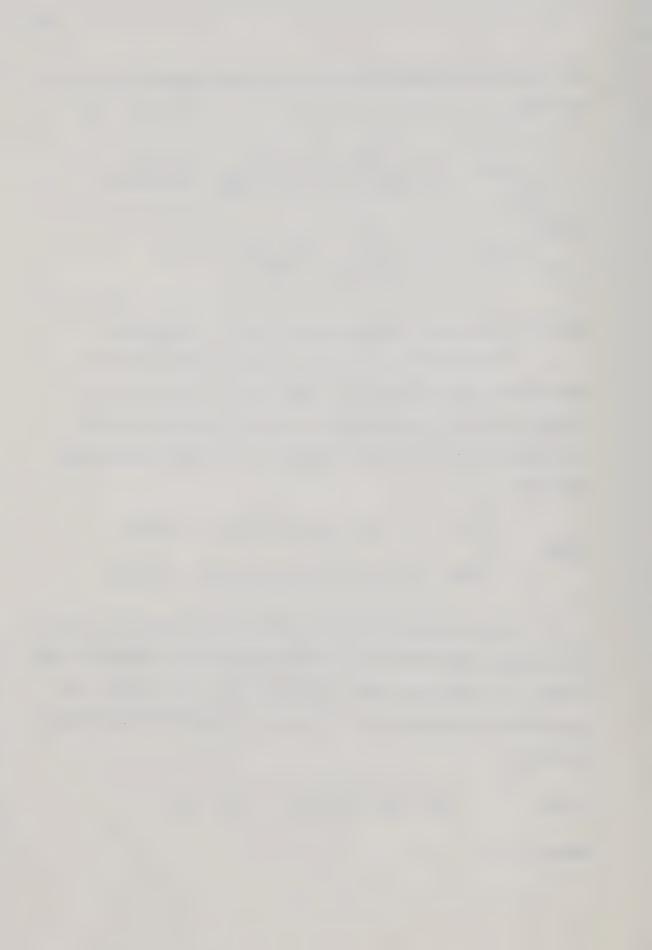
where F is the ratio of mean squares, namely $F = MS_A/MS_e$.

The derivations up to and including equation (2.13) are valid without any distributional assumptions on $\{a_i\}$ and $\{e_{ij}\}$. In order to obtain a sampling distribution of the estimate (2.13), distributional assumptions are necessary. The simplest normal assumptions are

With the above assumptions, model (2.6) is identical to the two way mixed model ANOVA with one observation per cell (Scheffé, 1959, p. 261). It can be shown that $SS_A/(J\sigma_A^2 + \sigma_e^2)$ and SS_e/σ_e^2 are distributed as chi-square with I-1 and γ degrees of freedom respectively, or

(2.15)
$$SS_{A} = (J\sigma_{A}^{2} + \sigma_{e}^{2}) \chi_{I-1}^{2}; \qquad SS_{e} = \sigma_{e}^{2} \chi_{v}^{2},$$

hence, F is



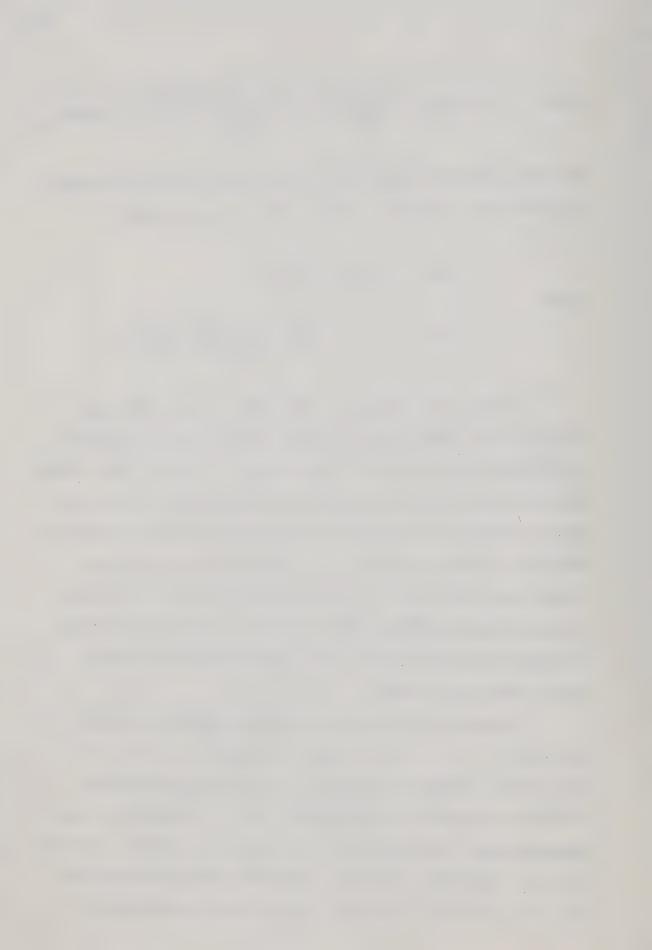
(2.16)
$$F = MS_A/MS_e = \frac{SS_A/(1-1)}{SS_e/\nu} = \frac{(J\sigma_A^2 + \sigma_e^2)\chi_{1-1}^2/(1-1)}{\sigma_e^2 \chi_\nu/\nu} = (1+J\theta)F_{1-1;\nu}.$$

Therefore, from (2.13) and (2.16), the following relationship between F-statistic and ρ and $\hat{\rho}$, or ρ_j and $\hat{\rho}_i$ can be made:

(2.17)
$$\begin{cases} (a) & F_{I-1;\nu} = \frac{1-\rho}{1-\hat{\rho}} \\ (b) & = \frac{[1+(J-1)\hat{\rho}_{j}][1-\rho_{j}]}{[1+(J-1)\hat{\rho}_{j}][1-\hat{\rho}_{j}]} \end{cases}.$$

Feldt (1965), Nitko and Feldt (1969), Nitko (1968), and Cleary and Linn (1968) derived the above formula, and even applied it to the sampling distribution of KR20 estimates. Kristof (1963) obtained the same results by means of maximum likelihood methods using a multinormal assumption. He obtained an estimate of intra-class correlation coefficient, which is equal to $\hat{\rho}_j$, and gave the estimate of the reliability of the total $\hat{\rho}$, called a step-up reliability, by using the general Spearman-Brown formula. However, this result is not new for mathematical statisticians. For example Scheffé gave similar results (1959, pp. 226-229).

Because (2.17) gives the relationship between the sample statistic $\hat{\rho}_j$, or $\hat{\rho}$ and the population parameter ρ_j or ρ in terms of the well-known F-statistic, the sampling distribution of reliability estimates can be determined; thus, it is possible to make inferences about the reliability, and to calculate confidence intervals. Within the essentially parallel assumptions, the sampling distribution of the reliability would not raise any questions provided the



assumptions (2.7) and (2.14) are all met and the model as given by equation (2.6) is adequate.

As a special case of the model, let all of the fixed effects $\{\beta_j^*\}$ be equal to zero, then the model (2.6) reduces to

(2.18)
$$y_{ij} = \mu + a_i + e_{ij}$$
, $i = 1,2,...,l$; $j = 1,2,...,J$.

This model is identical to the one way random effect model ANOVA (Scheffé, 1959, pp. 221-235), and it can be shown that all the formulas given above are valid with SS_e and v replaced by $(SS_B + SS_e)$ and I(J-1), and MS_e modified accordingly. Model (2.18) is equivalent to the classical parallelism assumptions (e.g., Gulliksen, 1950, p. 11) except for the distributional assumptions which are not required under the classical test theory. Kristof's case 2 and Maguire and Hazlett's case C (1969) correspond to this model

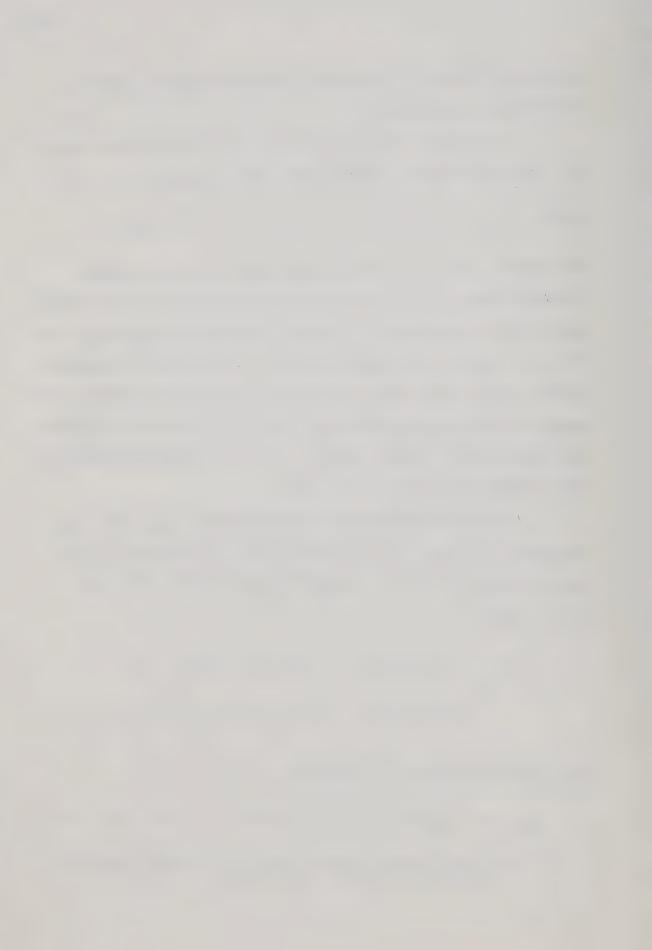
Because the variance of random variables $\{a_i\}$ and $\{e_{ij}\}$ are equal to σ_A^2 and σ_e^2 respectively under the ANOVA model, they may be rewritten in terms of standard random variables $\{f_i\}$ and $\{\epsilon_{ij}\}$, namely,

$$a_i = \sigma_A f_i$$
, $i = 1,2,...,I$, and $e_{ij} = \sigma_e \epsilon_{ij}$, $i = 1,2,...,I$; $j = 1,2,...,J$.

Then the model equation (2.6) becomes

$$y_{ij} = \mu + \sigma_A f_i + \beta_j + \sigma_e \epsilon_{ij}, \quad i = 1, 2, ..., I; \quad j = 1, 2, ..., J$$
.

The above equations can be rewritten in a matrix equation



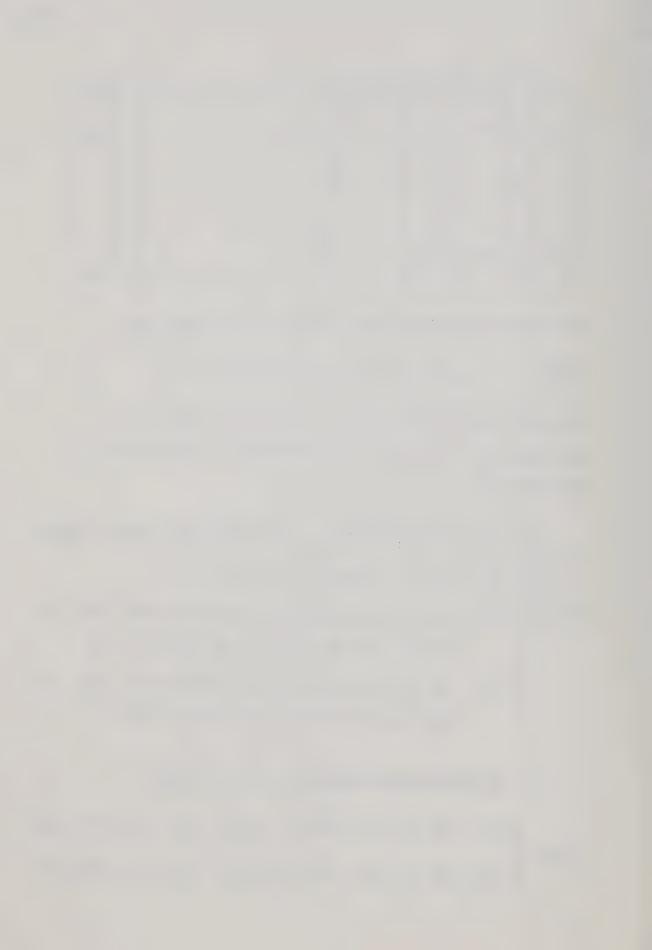
$$\begin{bmatrix} y_{i1} \\ y_{i2} \\ \vdots \\ \mu+\beta_2 \\ \vdots \\ \mu+\beta_J \end{bmatrix} \begin{bmatrix} \sigma_A \\ \sigma_A \\ \vdots \\ \sigma_e \end{bmatrix} \begin{bmatrix} \sigma_e & 0 & 0 & . & . & 0 \\ 0 & \sigma_e & 0 & . & . & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & \ddots & \ddots & \ddots & \vdots \\ 0 & \ddots & \ddots & \ddots & \ddots \\ 0 & \ddots & \ddots & \ddots & \ddots \\ 0 & \ddots & \ddots & \ddots & \ddots \\ 0 & 0 & . & . & \sigma_e \end{bmatrix} \begin{bmatrix} \epsilon_{i1} \\ \epsilon_{i2} \\ \vdots \\ \epsilon_{iJ} \end{bmatrix} ,$$

or, using the notations given in Section 1.3 of Chapter One,

(2.6')
$$\underline{y}_{i} = \underline{\mu} + \underline{\lambda} f_{i} + \underline{\Psi} \underline{\varepsilon}_{i}, \quad i = 1, 2, ..., 1,$$

with the limitations $\lambda_1=\lambda_2=\ldots=\lambda_J=\sigma_A$, and $\Psi_{11}=\Psi_{22}=\ldots=\Psi_{JJ}=\sigma_e$. The assumptions of (2.7) may be rewritten as,

The distributional assumption of (2.14) becomes



2.2 Essentially T Equivalent Measurements Model

Under the ANOVA model, $\tau_{ij} = \mu + a_i + \beta_j$, hence with $j \neq j'$, $\tau_{ij} - \tau_{ij'} = \beta_j - \beta_{j'} = c$ where c is a constant which depends only on j and j'. Therefore, the part tests satisfy the conditons of the so-called essentially τ equivalent measurements (Lord and Novick, 1968, p. 50) which will be denoted as ETEM henceforth. Because the assumption of homogeneity of error variances is not required for the definition of ETEM, the error variance σ_{ej}^2 may depend on a specific j. Thus, assumption (d) of (2.7) may be modified to become,

(2.19) (d)
$$\{e_{ij}\}$$
 are distributed with $E(e_{ij}) = 0$; $Var(e_{ij}) = \sigma_{ej}^2$.

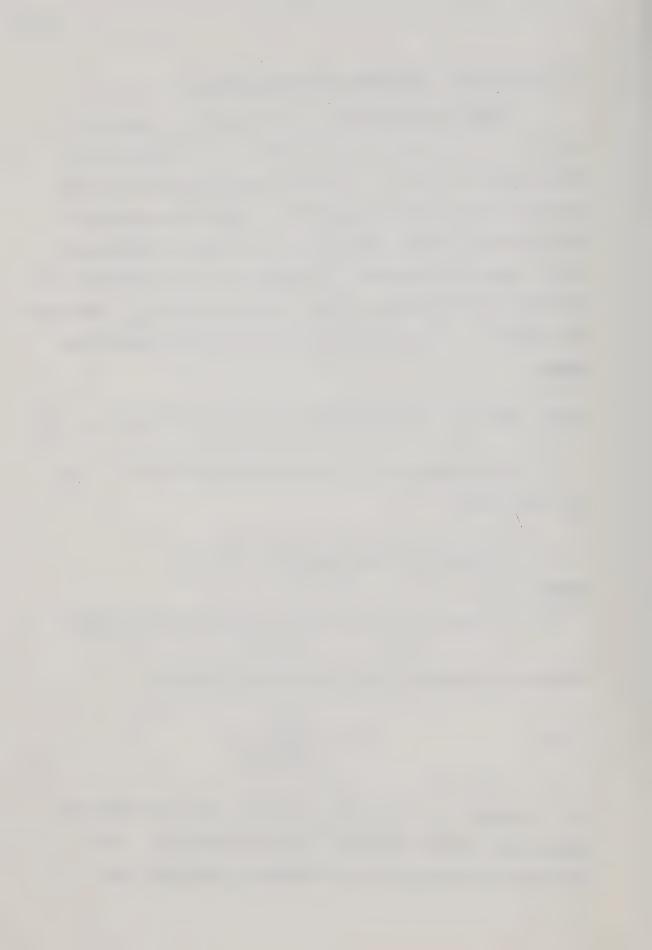
The variance of y_{ij} and the covariance between y_{ij} and y_{ij} are given by

Therefore, the reliability of jth part test is given by

$$\rho_{j} = \frac{\sigma_{A}^{2}}{\sigma_{A}^{2} + \sigma_{ej}^{2}},$$

i.e., it depends on j, and hence, in general, under the ETEM model, there is not a common correlation coefficient among the J parts.

Therefore the reliability of a part cannot be interpreted as an



intra-class correlation coefficient. The correlation coefficient between
j and j' depends on j and j', because,

$$\text{Cor} \ (y_{ij},y_{ij'}) = \frac{\text{Cov} \ (y_{ij},y_{ij'})}{\left[\text{Var} \ (y_{ij})\text{Var} (y_{ij'})\right]^{\frac{1}{2}}} = \frac{\sigma_A^2}{\left[\left(\sigma_A^2 + \sigma_{ej}^2\right)\left(\sigma_A^2 + \sigma_{ej'}^2\right)\right]^{\frac{1}{2}}} \ .$$

The reliability of the total test is given by,

(2.22)
$$\rho = \frac{\text{Var}(J a_i)}{\text{Var}(y_i)} = \frac{J^2 \sigma_A^2}{J^2 \sigma_A^2 + \sum_{e_i}^2 \sigma_{e_i}^2} = \frac{\sigma_A^2}{\sigma_A^2 + \sigma_{e_i}^2/J} ,$$

where σ_{e}^{2} is average of σ_{ej}^{2} , i.e., $\sigma_{e}^{2} = (\sum_{ej} \sigma_{ej}^{2})/J$.

If σ_j^2 denotes the total variance of jth part test given by (2.20), the total test variance denoted by σ_y^2 is

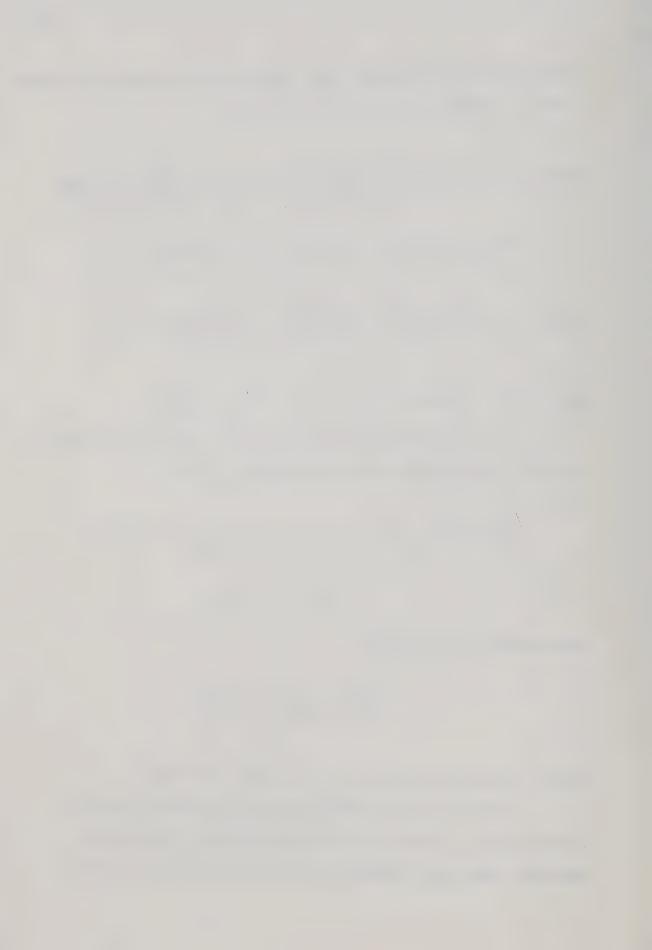
$$\sigma_{y}^{2} = \text{Var} \left(\sum_{j} y_{ij}\right) = \sum_{j} \text{Var} \left(y_{ij}\right) + \sum_{j \neq j} \sum_{i} \text{Cov} \left(y_{ij}, y_{ij}\right)$$
$$= \sum_{j} \sigma_{j}^{2} + J(J-1) \sigma_{A}^{2}.$$

Substituting this into (2.22)

$$\rho = \frac{J^2 \sigma_A^2}{\sigma_y^2} = \frac{J}{J-1} \left[1 - \frac{\sum \sigma_j^2}{\sigma_y^2}\right].$$

which is the well-known formula for the Alpha coefficient.

Novick and Lewis (1967) have shown that Alpha is equal to reliability ρ if and only if the ETEM assumption is satisfied. Otherwise, Alpha is, in general, lower than the reliability, namely



(2.23) Alpha
$$< \rho$$
.

The equality holds only if the ETEM assumption is true.

Alpha is usually estimated by

(2.24) Alpha =
$$\frac{J}{J-1} \left[1 - \frac{\sum s_{j}^{2}}{s_{y}^{2}}\right]$$
,

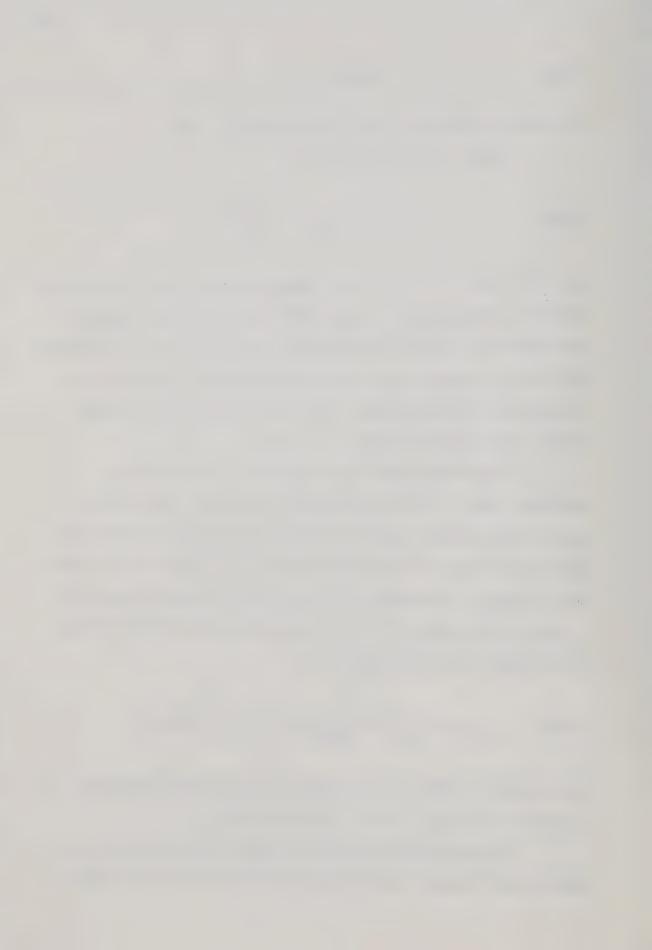
where s_j^2 and s_y^2 are the usual sample variance of part test and the total test respectively. Kristof (1970) investigated the sampling distribution of the Alpha estimate for the case of J=2, and showed that the distribution can be reduced to a Student's t-statistic by the maximum likelihood method. The sampling distribution for the general case is not yet known.

Classically, Alpha as a reliability is derived (e.g., Gulliksen, 1950, p. 223) by considering two J-parts tests that are parallel part by part, and then introducing the assumption that the covariance of a part in one test with the parallel part of the second test is equal in the average to the covariance between any two of the J parts within a test. If y_{ij}^* denotes the score of the jth part of the second test the assumption is,

(2.25)
$$\sum_{j} \text{Cov} (y_{ij}, y_{ij}^{*}) = \left[\sum_{j \neq j} \text{Cov} (y_{ij}, y_{ij})\right] / (J-1) .$$

Lord and Novick (1968, p. 92) have shown that the above assumption is satisfied if and only if the j parts are ETEM.

Under the ETEM assumption, the matrix model equation is the same as (2.6') except that the diagonal elements of $\underline{\Psi}$ may differ,



namely,

$$\underline{y}_{i} = \underline{\mu} + \underline{\lambda} f_{i} + \underline{\Psi} \underline{\varepsilon}_{i} ,$$

$$\Psi_{11} = \sigma_{e1}, \quad \Psi_{22} = \sigma_{e2}, \dots, \Psi_{JJ} = \sigma_{eJ} .$$

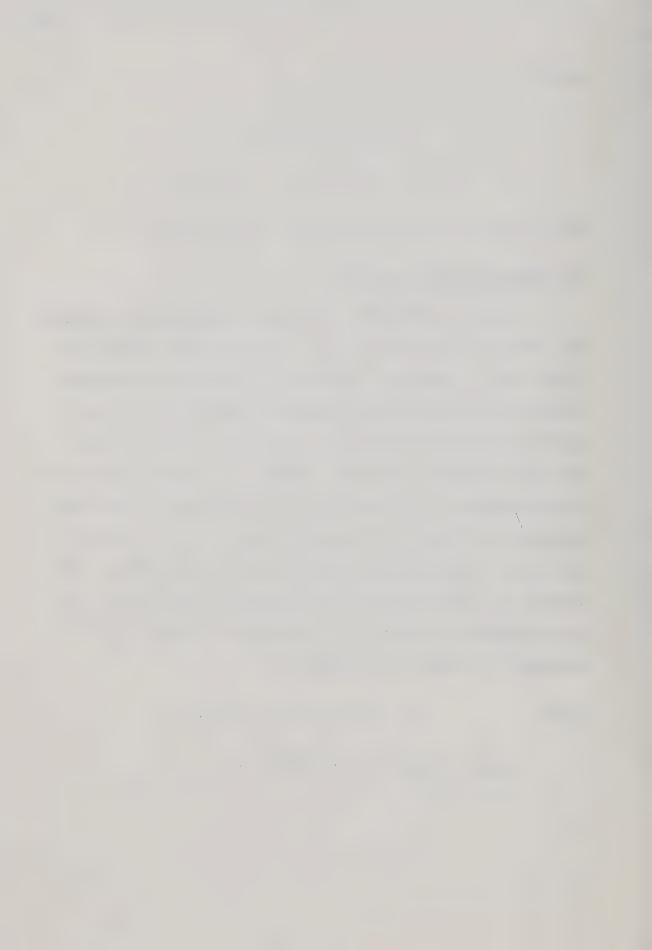
All the assumptions of (2.7') and (2.14') may be applied.

2.3 Congeneric True Score Model

Under the ETEM model, including the ANOVA model as a special case, the true score variance, σ_A^2 , is assumed to be common to all J part tests. However, for some tests, it might be more reasonable to expect that the true score variance would depend on j, i.e., some of the part tests might discriminate better and have greater true score variances. Under this situation, the classical parallelism or ETEM assumption is no longer valid. Nevertheless, the model given by equation (2.6') may still be used by removing the restriction of equal $\{\lambda_j\}$, namely the elements of the vector $\underline{\lambda}$ may differ. The constant λ_j may be interpreted as a regression coefficient of y_{ij} on the standard true score f_i , or standard deviation of the jth true score. In scalar form the equation is

(2.26)
$$y_{ij} = \mu + \lambda_{j} f_{i} + \beta_{j} + \sigma_{ej} \epsilon_{ij}.$$

Under this model, the reliability is



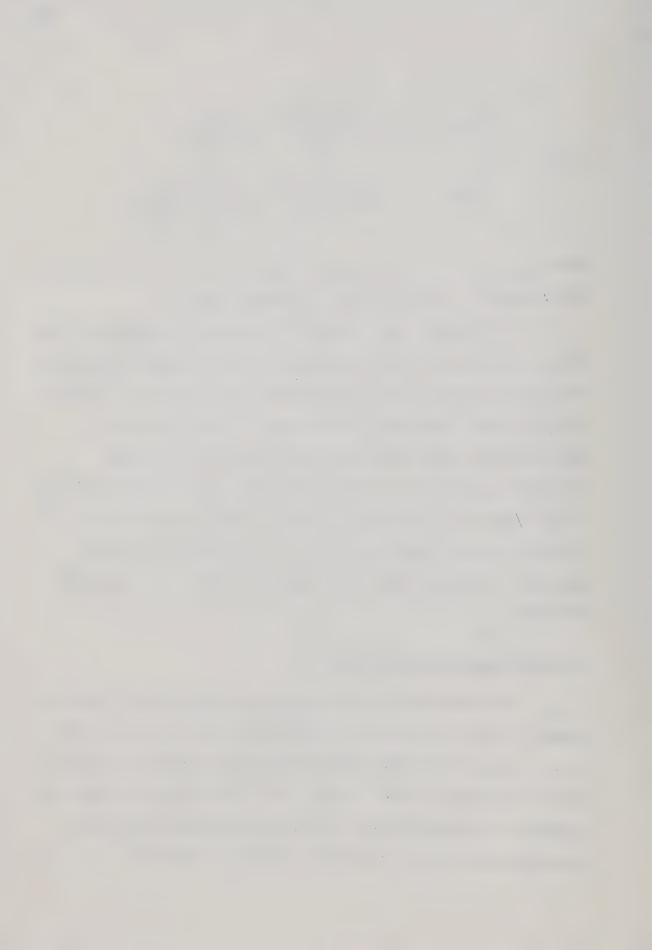
(2.27)
$$\begin{cases} (a) & \rho_{j} = \frac{\operatorname{Var}(\lambda_{j}f_{i})}{\operatorname{Var}(y_{ij})} = \frac{\lambda_{j}^{2}}{\lambda_{j}^{2} + \sigma_{ej}^{2}} \\ (b) & \rho_{j} = \frac{\operatorname{Var}(\underline{1}' \underline{\lambda}_{j} f_{i})}{\operatorname{Var}(\underline{1}' \underline{\lambda}_{i})} = \frac{\underline{1}' \underline{\lambda}_{j} \underline{\lambda}' \underline{1}}{\underline{1}' (\underline{\lambda}_{j} \underline{\lambda}' + \underline{\psi}^{2})\underline{1}} \end{cases},$$

where $\underline{1}$ is a J \times l vector whose elements are all l's. Since the ETEM assumption is not satisfied, in general, Alpha < ρ .

No formula is yet available for the direct estimation of the reliability under this model, hence the estimate of Alpha is generally used as an estimate of the lower bound for the reliability. Cronbach, lkeda and Avner (1964) used a similar model in their effort to approximate the generalizability coefficient by an intra-class correlation coefficient. However their model, which involves sampling of part tests (Type 2 sampling), assumes a uniform distribution of λ^2 , unlike the present model where the $\{\lambda_j\}$ are assumed to be fixed constants. Jöreskog (1968, 1970) named this model as the congeneric test model.

2.4 Multi-Factor True Score Model

The three models reviewed in the previous sections implicitly assumed that the test measures only one ability or trait, represented by f_i , i.e., it is assumed that the factorial structure of the true score is a uni-factor model. However, for certain types of tests, the assumption is too restrictive, and a more general model which would accommodate more than one true score structure is desirable.



If $\underline{\lambda}$ and f_i are replaced by a J × r, $(1 \le r < J)$ constant factor loading matrix $\underline{\Lambda}$ and a r × 1 standard random factor score vector \underline{f}_i respectively, the model of equation (2.61), becomes the well-known multi-factor model, (e.g., Browne, 1969; Jöreskog, 1970), namely,

(2.28)
$$\underline{y}_{i} = \underline{\mu} + \underline{\Lambda} \underline{f}_{i} + \underline{\Psi} \underline{\varepsilon}_{i} ,$$

with,

$$E(\underline{y}_i) = \underline{\mu}_i$$
; $D(\underline{y}_i) = \underline{\Lambda}_i + \underline{\Psi}^2$.

Therefore, the reliability of the total test, ρ , is given by,

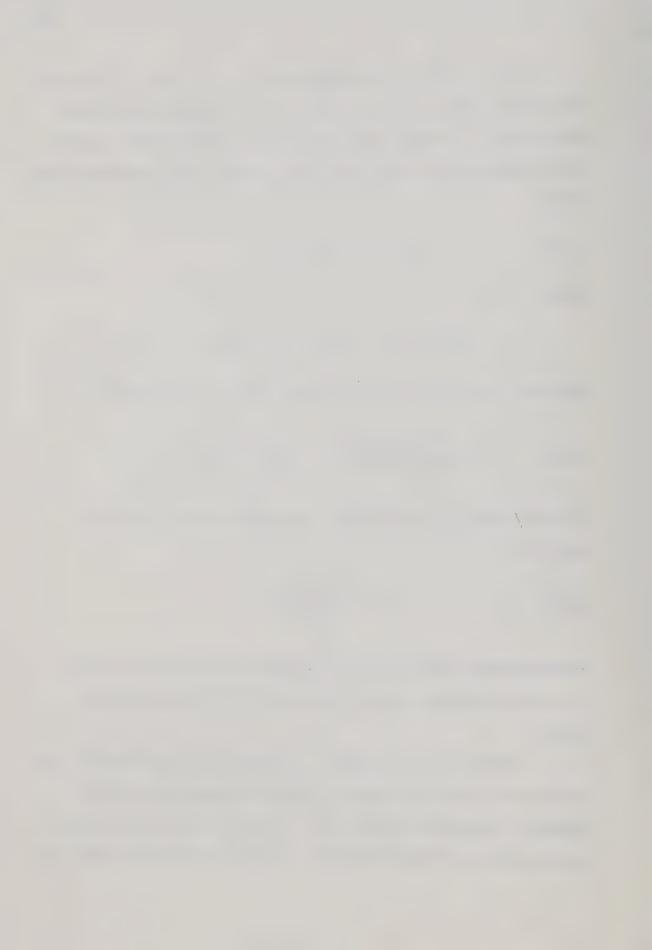
(2.29)
$$\rho = \frac{\operatorname{Var} \left(\underline{1}' \ \underline{\Lambda} \ \underline{f_i}\right)}{\operatorname{Var} \left(\underline{1}' \ \underline{Y_i}\right)} = \frac{\underline{1}' \ \underline{\Lambda} \ \underline{\Lambda}' \ \underline{1}}{\underline{1}' \left(\underline{\Lambda} \ \underline{\Lambda}' + \underline{\Psi}^2\right)\underline{1}}$$

If the estimate $\hat{\underline{\Lambda}}$ is available, an estimate of the reliability would be,

$$\hat{\rho} = \frac{\underline{1}' \hat{\Lambda} \hat{\Lambda}' \underline{1}}{s_y^2}.$$

The statistical properties of this statistic are unknown, and there is no agreed upon mean to obtain estimates of the factor loading matrix.

Under this model Alpha is in general the lower bound for the reliability as with the congeneric model. The equality is true if and only if the parts are ETEM, i.e., r=1. For this case the factor loading matrix Λ becomes the vector λ with all elements equal, and



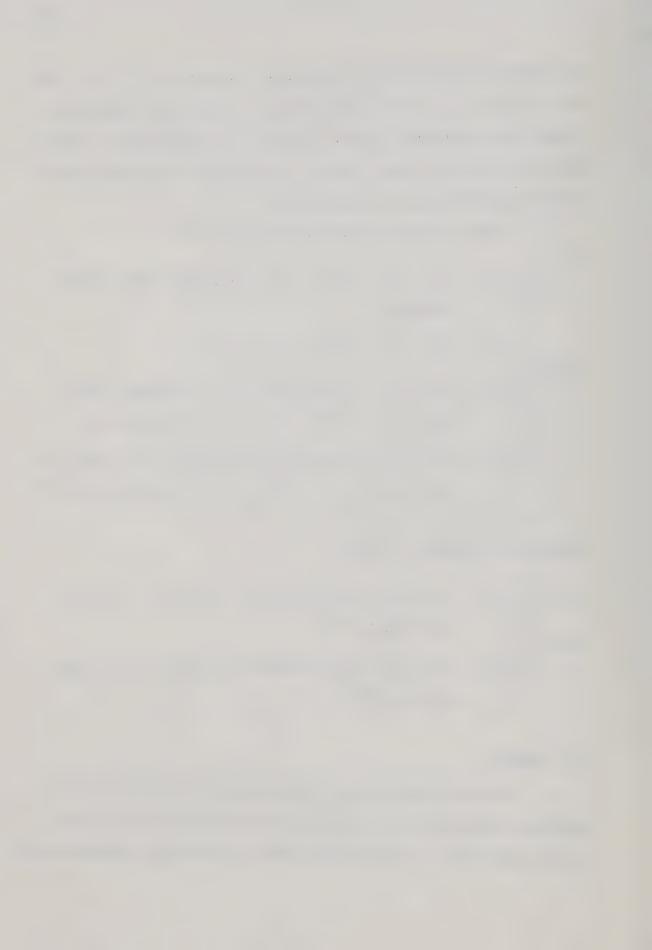
the standard deviations of the true scores are equal, as $\lambda_j = \sigma_A$ for all $j=1,2,\ldots,J$. If the error variances are all equal among the J part tests, the model becomes identical to the ANOVA model. Therefore the multi-factor model equation (2.28) includes the ANOVA, ETEM and the congeneric model as special cases.

Under this general model the assumptions are

The normality assumption becomes

2.5 Summary

Four basic models which might be used for simulation of test scores are examined in this chapter under the assumption that a test has been split into J parts whose scores are continuous random variables.



The most general model is found to be the multi-factor model. The other three models are special cases of this model with additional assumptions or restrictions on the parameters.

With uni-factor assumptions, i.e., r=1, the congeneric model is the most general one, which includes the other two models as special cases. However, the Alpha coefficient is identical to the reliability of the total test score if and only if the ETEM assumption is satisfied. Hence under the multi-factor or congeneric model, in general, the Alpha coefficient is a lower bound for the reliability.

With the homogeneity of error variance assumption the ETEM model becomes identical to the ANOVA model, the most restrictive one, and the distribution of reliability estimate is related to an F-statistic. Under more general models, the distribution is in general unknown.

If equal means are assumed among the J parts, the ANOVA model becomes identical with the classical parallelism model except for the distributional assumptions.



CHAPTER THREE

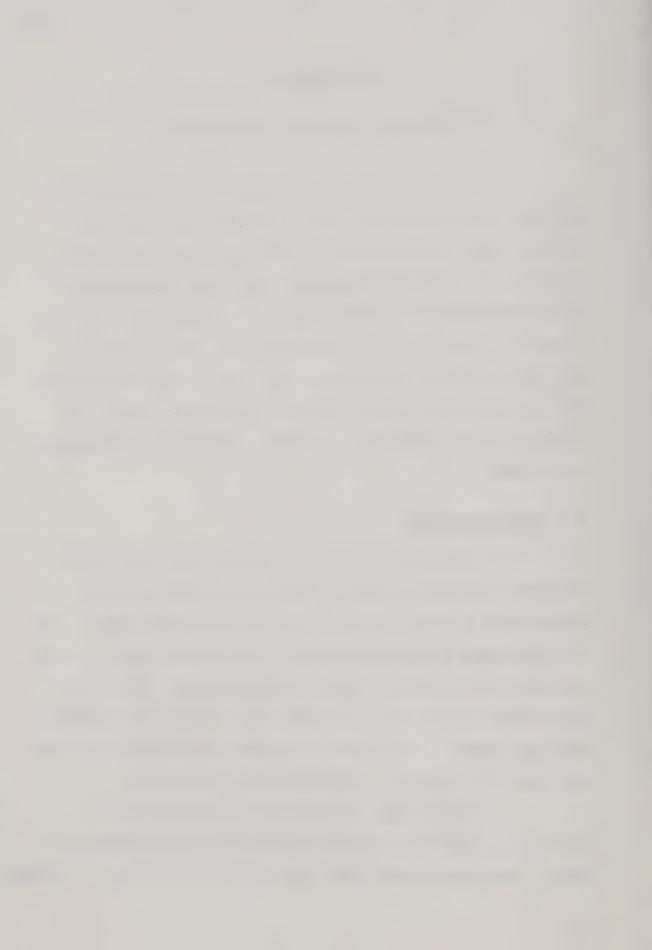
TEST MODEL FOR THE BINARY ITEM SCORE CASE

For a test consisting of J binary items as the parts of the test, the Kuder-Richardson formula 20 (KR20) has been widely used as a special case of the Alpha coefficient with little investigation of its statistical properties. Feldt (1965), and Cleary and Linn (1968) treated the discrete case as a continuous part score case. However, the imposition of the zero-one scoring scheme violates not only the assumption of continuity of part scores, but also homogeneity of error variances and independence of true and error scores. The violation of the assumptions of the ANOVA model was fully discussed by Feldt (1965).

3.1 Normal Ogive Model

To investigate the statistical properties of test scores of binary item tests, a number of mathematical models have been proposed such as the normal ogive, logistic, and binomial models. The first two assume existence of a latent trait or factor score f, which can account for the subjects behavior or performance. The binomial model relies on the 'strong true score' theory (Lord, 1965; Birnbaum, 1968, pp. 508-529). In this model the conditional distribution of the test score for a given true score is assumed to be binomial.

In the following, the discussion is restricted to the statistical properties of reliability and KR20 under the normal ogive model. Extensions to other models may be done in a similar way. Although



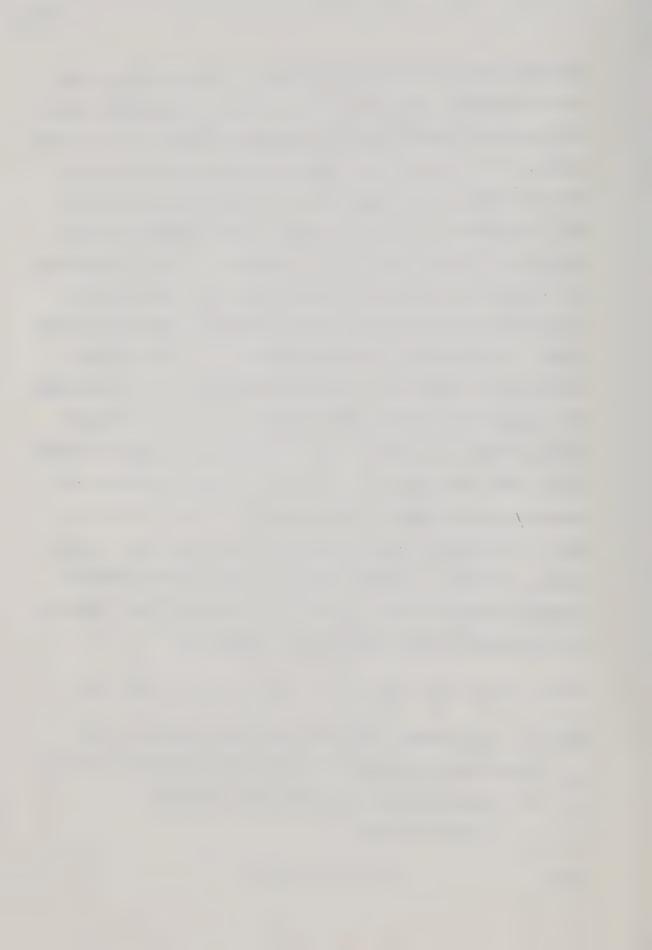
the multi-factor model for the binary test is also possible, for the sake of simplicity, only the uni-factor case will be examined. Under this model, the random variable representing the latent trait or factor scores, f, is assumed to be independently distributed as N(0,1), for all subjects in the population \mathcal{P}_{i} , as under the continuous part test score models. It is also assumed that the response of the ith subject, with latent trait f = f; to each of J items, is determined by a hypothetical intervening random variable y which shall be called the 'response strength variable' according to Bock and Liberman (1970). Since only the relative strength of y_{ij} is of interest, without loss of generality, it may be assumed that y is distributed with expected value zero and unit variance, i.e., it is a standard random variable. In addition y; is assumed to be subject to random error, and if the value of y_{ii} for the ith subject on the jth item exceeds a certain threshold constant specific to the item, denoted by β_i , the observed score of the subject, denoted by x_{ij} is equal to one, otherwise it is equal to zero. In this case the continuous response strength variable y may be written as a linear congeneric true score model noted in Section 2.3 of Chapter Two.

(3.1)
$$y_{ij} = \lambda_j f_i + \sigma_{ej} \epsilon_{ij}, \quad i = 1, 2, ..., I; \quad j = 1, 2, ..., J,$$

where λ_j is a constant regression coefficient specific to item j, σ_{ej} is the standard deviation of the error scores for jth item, while ϵ_{ij} is a standard random variable for errors as before.

In vector notation,

$$(3.2) \underline{y}_{i} = \underline{\lambda} f_{i} + \underline{\Psi} \underline{\varepsilon}_{i} ,$$



where $\underline{\lambda}$, $\underline{\Psi}$, and $\underline{\varepsilon}_i$ are as defined for the congeneric model, except that the continuous part tests are replaced by dichotomous items. Also $D(\underline{\gamma}_i) = \underline{\lambda} \underline{\lambda}^{\dagger} + \underline{\Psi}^2$ as before, and the diagonal elements of $D(\underline{\gamma}_i)$ are the variances of y_{ij} , and are assumed to be unity, i.e., $1 = \lambda_j^2 + \sigma_{ej}^2$ for all $j = 1, \ldots, J$.

Thus model equation (3.1) may be rewritten,

(3.3)
$$y_{ij} = \lambda_j f_i + (1-\lambda_j^2)^{\frac{1}{2}} \epsilon_{ij}, \quad i = 1, 2, ..., I; \quad j = 1, 2, ..., J,$$

where the standard random variables $\{\epsilon_{ij}\}$ are assumed to be distributed independently as N(0,1).

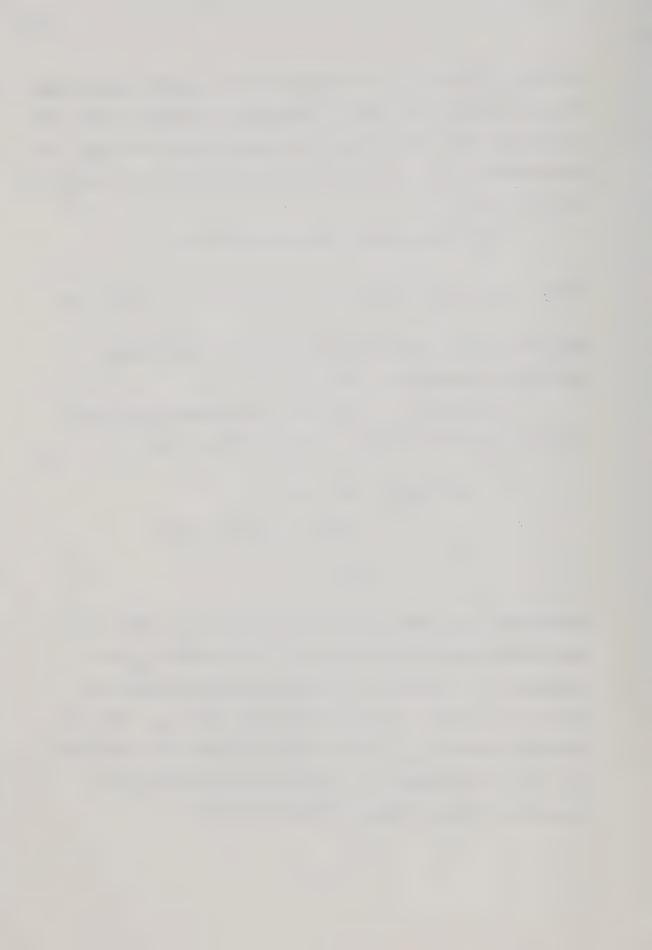
The constant λ_j may also be interpreted as the index of reliability of the jth response strength variable, since

Cor
$$(y_{ij}, f_i) = Cov (y_{ij}, f_i)$$

$$= E\{[\lambda_j f_i + (1 - \lambda_j^2)^{\frac{1}{2}} \epsilon_{ij}]f_i\}$$

$$= \lambda_j.$$

By definition the correlation coefficient between y_{ij} and f_i is equal to the biserial correlation coefficient between x_{ij} and f_i , therefore, λ_j is actually the biserial correlation between the latent trait variable f and observable item score x_{ij} . Since the correlation between y_{ij} and the individual effect or the true score $\lambda_j f_i$ is λ_j , the square of λ_j may also be interpreted as the reliability of the jth response strength variable.



3.2 Item Parameters

The jth item characteristic function $P_j(f)$ is defined to be the expected value of x_{ij} given f for subject i, (e.g., Lord and Novick, 1968, p. 360), namely,

(3.4)
$$P_{j}(f) = E(x_{ij} | f = f_{i}) = Probability (x_{ij} = 1 | f = f_{i})$$
.

Lord (1952, 1953), Lord and Novick (1968, pp. 358-394),
Samejima (1969), Bock and Liberman (1970) and many others have investigated the item characteristic function under the normal ogive model.

The expected value and variance of response strength variable y_i given a fixed subject with $f = f_i$, are given as,

(3.5)
$$E(y_{ij} | f = f_i) = \lambda_j f_i; \quad Var(y_{ij} | f = f_i) = 1 - \lambda_j^2.$$

The distribution of y_{ij} for fixed $f=f_i$ is normal with expected value $\lambda_j f_i$ and variance $1-\lambda_j^2$, or $N[\lambda_j f_i, (1-\lambda_j^2)]$. Thus the probability that subject i with the latent trait $f=f_i$ will respond correctly to item j, as indicated by observed value $x_{ij}=1$, is

$$\begin{split} P_{j}(f) &= \text{Probability } (x_{ij} = 1 \mid f = f_{i}) \\ &= \frac{1}{\left[2\pi(1-\lambda_{i}^{2})\right]^{\frac{1}{2}}} \int_{\beta_{j}}^{\infty} \text{Exp } \frac{-(y_{ij}-\lambda_{j}f)^{2}}{2(1-\lambda_{j}^{2})} \ dy_{ij} \ . \end{split}$$

Applying the transformation $z = (y_{ij} - \lambda_j f)/(1 - \lambda_j^2)^{\frac{1}{2}}$, $P_j(f)$ becomes

(3.6)
$$P_{j}(f) = \int_{g_{j}}^{\infty} \phi(z)dz = \Phi(-g_{j}),$$



where $\phi(z)$ and $\Phi(-g)$ are the respective standard normal density and distribution functions. The value $\mathbf{g}_{\dot{1}}(f)$ is given by,

(3.7)
$$g_{j}(f) = -(\lambda_{j}f - \beta_{j})/(1 - \lambda_{j}^{2})^{\frac{1}{2}}.$$

Using generally accepted notation (e.g., Lord and Novick, 1968), $g_{j}(f)$ may be rewritten as,

(3.8)
$$g_{j}(f) = -a_{j}(f - b_{j})$$
,

hence

$$\alpha_{j} = \lambda_{j}/(1 - \lambda_{j}^{2})^{\frac{1}{2}} ,$$

and

(3.9)
$$\begin{cases} b_{j} = \beta_{j}/\lambda_{j} \\ \beta_{j} = \alpha_{j} b_{j}/(1 + \alpha_{j}^{2})^{\frac{1}{2}} \end{cases}$$

The item parameters a_j and b_j have been referred to as item 'discrimination power' and 'difficulty index' by Lord and Novick (1968. pp. 368-368).

The difficulty of item $\, \mathbf{j} \,$ is defined as expected value of $\, \mathbf{x}_{\mathbf{i}\,\mathbf{j}} \,$, $\, \mathbf{n}_{\mathbf{a}\mathbf{m}=\mathbf{l}\,\mathbf{y}} \,$,

(3.10)
$$\pi_{j} = \text{Probability } (x_{ij} = 1) = E(x_{ij}) = \int_{-\infty}^{\infty} P_{j}(f) \phi(f) df$$
.

After some algebraic manipulation, it can be shown (Lord and Novick, 1968, p. 337) that, $\pi_j = \Phi(-\beta_j)$.



Since $E(x_{ij}^2) = E(x_{ij})$, the variance of jth item is given by,

(3.11)
$$\sigma_j^2 = Var(x_{ij}) = E(x_{ij}^2) - [E(x_{ij})]^2 = \pi_j - \pi_j^2 = \pi_j (1 - \pi_j)$$
.

3.3 Reliability of Binary Item Test

Since direct decomposition of the response score \mathbf{x}_{ij} into independent true and error scores is impossible for the binary item scores, there is no direct way of obtaining the variance ratio of true score variance to total test score variance which has been defined as the reliability of a test. Nevertheless the population reliability may be obtained by resorting to the correlation method, namely, by calculating the correlation coefficient between

$$x_i = \sum_j x_{ij}$$
 and $x_i^* = \sum_j x_{ij}^*$,

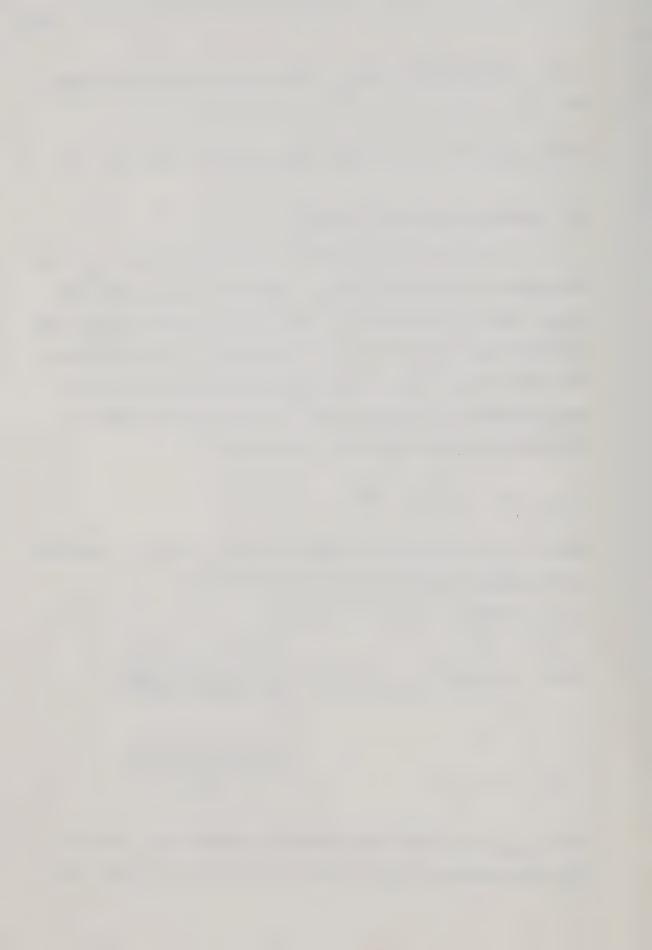
where x_{ij}^* is the score of a hypothetical test item which is parallel in the classical sense to the jth item of the test.

Then,

(3.12)
$$\rho = \text{Cor} \left(\sum_{j} x_{ij}, \sum_{j} x_{ij}^{*} \right) = \frac{\text{Cov} \left(\sum_{j} x_{ij}, \sum_{j} x_{ij}^{*} \right)}{\left[\text{Var} \left(x_{i} \right) \text{Var} \left(x_{i}^{*} \right) \right]^{\frac{1}{2}}}$$

$$= \frac{\sum_{j} \sum_{j*} \sigma_{j} \sigma_{j} \sigma_{j} \sigma_{j}^{*} \rho_{jj*}}{\sigma_{x}^{2}} ,$$

where ρ_{jj*} is the inter-item correlation between item j and j^* , σ_j^2 is the variance of the jth item, and σ_x^2 is the variance of the



total test score x_i . The test variance σ_x^2 may be given in terms of inter-item correlation and item variance, namely,

(3.13)
$$\text{Var} (x_i) = \text{Var} (\sum_{j} x_{ij}) = \sum_{j} \text{Var} (x_{ij}) + \sum_{j \neq j} \sum_{i} \text{Cov} (x_{ij}, x_{ij})$$

$$= \sum_{j} \sigma_j^2 + \sum_{j \neq j} \sum_{i} \sigma_j \sigma_{ji} \rho_{jji} .$$

To obtain ρ and $\sigma_{\mathbf{x}}^2$, the inter-item covariance $\sigma_{\mathbf{j}} \sigma_{\mathbf{j}'} \rho_{\mathbf{j}\mathbf{j}'}$ must be evaluated in terms of the item parameters $\lambda_{\mathbf{j}}$ and $\lambda_{\mathbf{j}'}$. Lord and Novick (1968, p. 379) showed that for any two items \mathbf{j} and \mathbf{j}' , the tetrachoric correlation between $\mathbf{x}_{\mathbf{i}\mathbf{j}}$ and $\mathbf{x}_{\mathbf{i}\mathbf{j}'}$, denoted by $\gamma_{\mathbf{j}\mathbf{j}'}$, can be expressed as the product of the two biserial correlations $\lambda_{\mathbf{j}}$ and $\lambda_{\mathbf{j}'}$ by performing integration of the tri-variable distribution $\mathbf{x}_{\mathbf{i}\mathbf{j}'}$, and \mathbf{f} , namely

$$\gamma_{jj'} = \lambda_j \lambda_{j'}.$$

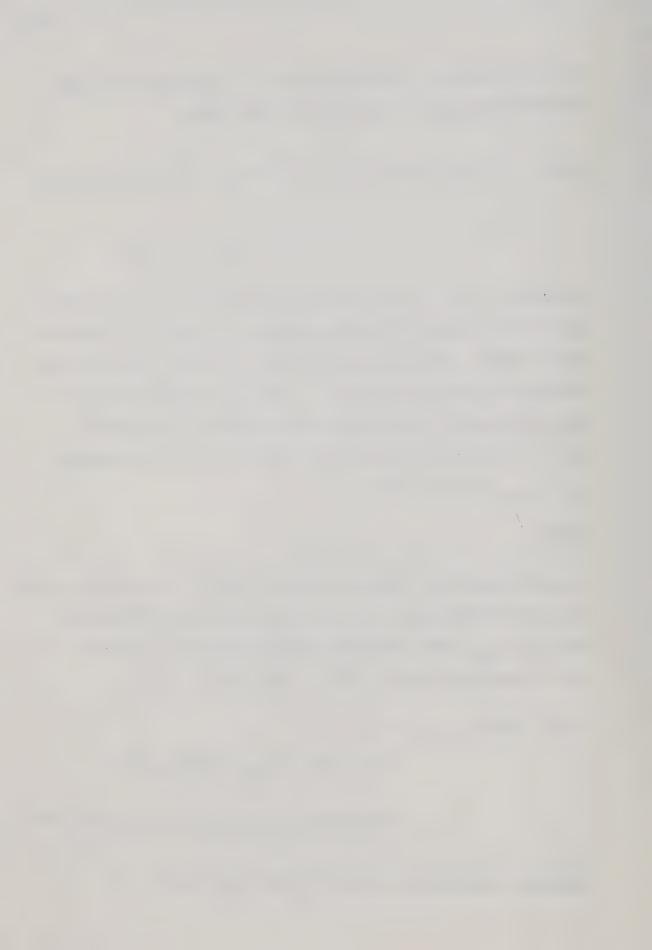
It can be shown (e.g., Kendall and Stuart, 1963, p. 161 and 1967, p. 306) that the inter-item covariance may be expressed as an infinite power series of γ_{jj} , using Tchebycheff-Hermite polynomials, denoted by $H_n(\beta)$ (Kendall and Stuart, 1963, p. 155). Then,

(3.15) Cov
$$(x_{ij}, x_{ij'}) = \sigma_j \sigma_{j'} \rho_{jj'}$$

$$= [\phi(\beta_j)\phi(\beta_{j'})][\gamma_{jj'} + 0.5 \beta_j \beta_{j'} \gamma_{jj'}^2 \dots]$$

$$= [\phi(\beta_j)\phi(\beta_{j'})] \sum_{n=1}^{\infty} [H_{n-1}(\beta_j) H_{n-1}(\beta_{j'}) \gamma_{jj'}^n]/n! .$$

Therefore, the covariance may be calculated numerically.



By the results of equations (3.11), (3.13), (3.14), and (3.15), the reliability ρ , given by equation (3.12) may be evaluated numerically if the item parameters $\{\beta_i\}$ and $\{\lambda_i\}$ are specified.

3.4 KR20 Coefficient and Its Estimate

The Alpha coefficient for the binary item test, KR20, is defined as,

(3.16) KR20 =
$$\frac{J}{J-1} \left[1 - \frac{\sum_{j=1}^{3} \sigma_{j}^{2}}{\sigma_{x}^{2}}\right] = \frac{J}{J-1} \left[1 - \frac{\sum_{j=1}^{3} (1 - \pi_{j})}{\sigma_{x}^{2}}\right]$$

which is equal to the reliability ρ if and only if the ETEM condition of (2.25) is satisfied. In general the condition is not satisfied, hence,

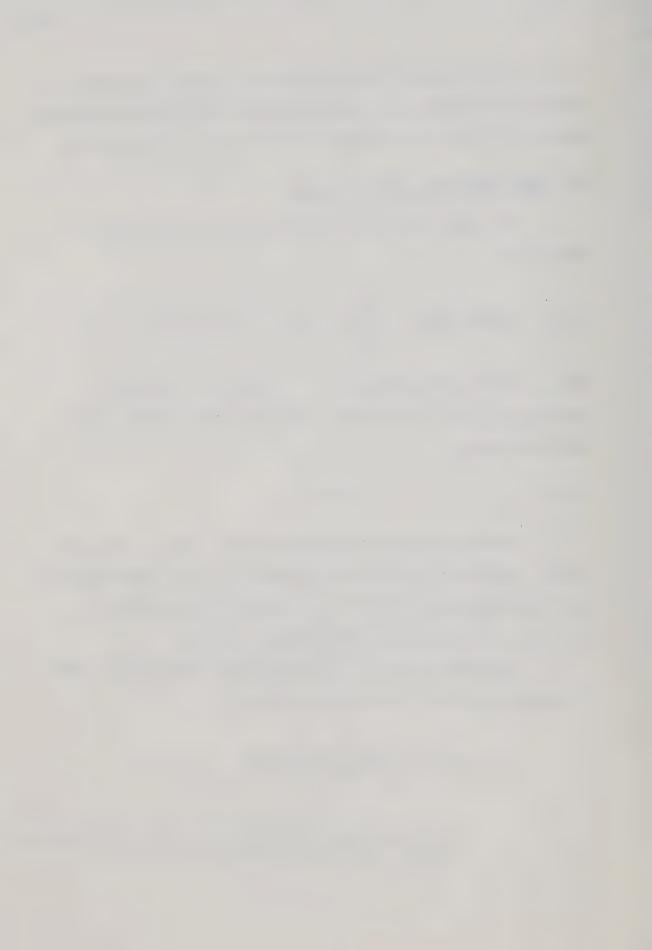
(3.17)
$$KR20 \le \rho$$
.

Using the results of equations (3.10), (3.13), (3.15), and (3.16), KR20 may also be evaluated numerically if the item difficulty $\{\pi_j\}$ and biserial correlation $\{\lambda_j\}$ are specified, provided f_j and $\{\epsilon_{ij}\}$ are distributed independently as N(0,1).

The ETEM condition of (2.25) for binary item cases in terms of the powe series of (3.15) may be written as,

$$\sum_{j} [\phi(\beta_{j})^{2} [\sum_{n=1}^{\infty} (H_{n-1}^{2}(\beta_{j})\lambda_{j}^{2n})/n!]$$

$$= \{ \sum_{i \neq j} \sum_{j=1}^{n} \phi(\beta_{j}) \phi(\beta_{j}) \sum_{n=1}^{\infty} [H_{n-1}(\beta_{j}) H_{n-1}(\beta_{j}) \gamma_{jj}^{n}] / n! \} / (J-1) ,$$



which is true if $\beta_1 = \beta_2 = \dots = \beta_J$ and $\lambda_1 = \lambda_2 = \dots = \lambda_J$. This means that all the item parameters are equal.

An estimate of KR20 is obtained by substitutiing the sample estimates of $\{\pi_i^{}\}$ and σ_x^2 , namely,

(3.18)
$$\widehat{KR20} = \frac{J}{J-1} \times \left[1 - \frac{\sum \hat{\pi}_{j} (1 - \hat{\pi}_{j})}{s_{x}^{2}}\right],$$

where $\hat{\pi}_j$ is the sample difficulty of the jth item, and s_x^2 is the sample variance of the test score x_i , given by,

(3.19)
$$\begin{cases} \hat{\pi}_{j} = (\sum_{i} x_{ij})/I, \\ s_{x}^{2} = [\sum_{i} (x_{i} - x_{i})^{2}]/I. \end{cases}$$

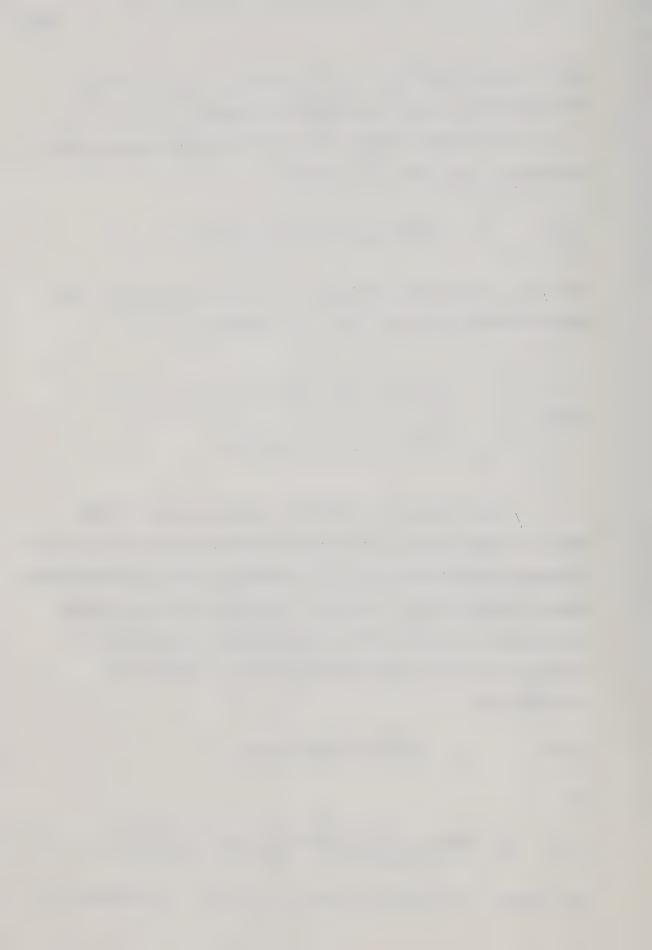
Unlike the case of reliability estimates under the ANOVA model, the exact sampling distribution of KR20 estimates given by (3.18) is unknown even with the restrictive mathematical models and assumptions. Aoyama's formulas (1957), provided an approximation for the expected value and the variance of KR20 estimates without any distributional assumptions. He gave approximate formulas for $E(\widehat{KR20})$ and $Var(\widehat{KR20})$ as,

(3.20)
$$E(\overline{KR20}) = KR20 + O(1/J)$$
,

and

(3.21)
$$\text{Var } (\widehat{KR20}) \leq \frac{1}{|(J-1)|^2} (\frac{1}{|-1|})^2 (\delta_2 + 15 + \frac{14}{J} + \frac{18}{J^2} x_m^2) ,$$

where O(1/J) is a term of the order of 1/J, δ_2 is the kurtosis of



the distribution of \mathbf{x}_i and \mathbf{x}_m is the minimum score. Formula (3.20) indicates the estimate is biased, while (3.21) suggests a bound for the standard error of KR20 estimates, but is of little use since it involves the unknown parameter δ_2 , which would be very difficult if not impossible to evaluate.

3.5 Summary

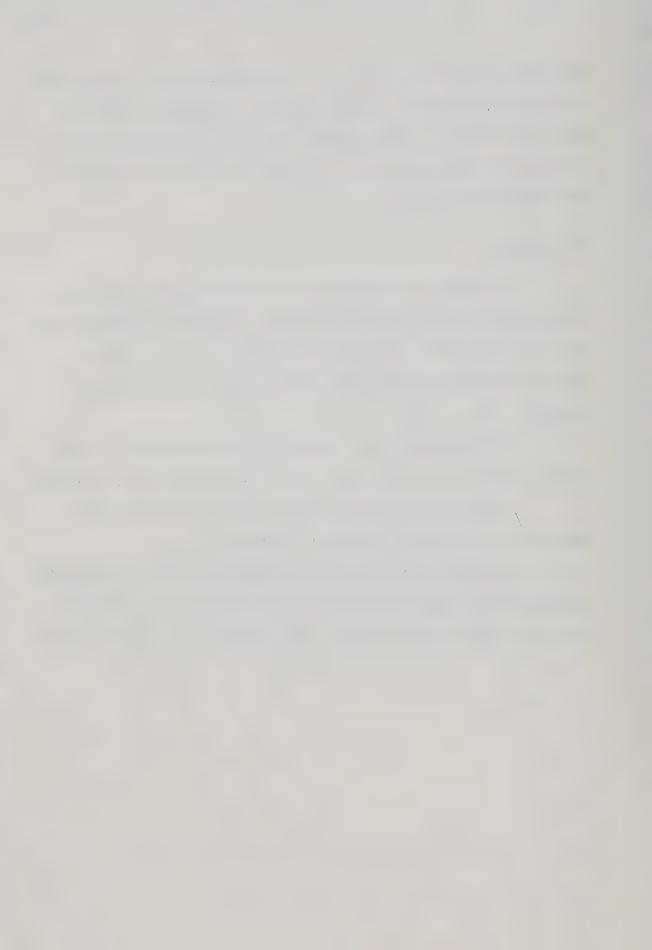
To examine the feasibility of simulating binary item test scores, the well-known normal ogive model is reviewed in terms of two basic item parameters, namely the item difficulty $\{\pi_j\}$, and the biserial correlation between items and the latent trait or factor score f_i , i.e., $\{\lambda_i\}$.

With the help of the 'response strength variable', a model equation similar to (2.26) used in the previous chapter was introduced.

Item characteristic functions and item indices are also examined in terms of the two sets of parameters.

The population reliability and KR20 were found to be amenable to calculation through numerical means in terms of these parameters.

The exact sampling distribution of KR20 estimates is in general unknown.



CHAPTER FOUR

RATIONALE FOR SIMULATION, COMPUTER PROGRAMS, AND METHOD OF INVESTIGATION

4.1 Violation of ANOVA Model and Assumptions

The review in the previous three chapters indicated that the exact sampling distribution of the reliability estimates is largely unknown except for the special case of the ANOVA model under rather restrictive assumptions. The distributional thoery and inferences based on this model are valid, if and only if all of the underlying assumptions of (2.7') and (2.14') are valid. A workable formula for the standard error of the reliability estimates may be obtained under this model only by employing the well-known characteristic of an F-statistic (Cleary and Linn, 1968). However, if any one or more of the assumptions are not valid the true sample reliability distribution will not be the same as that given by (2.17).

If the ANOVA model equation (2.6') is taken as the basic model, the more general models and the normal ogive model for the binary item test may be considered as being assumption-violating cases of the basic model. It has been shown that the latter more general models are obtained by successively relaxing some of the assumptions of (2.7'), and the normal ogive model has been shown to be the congeneric model if the hypothetical 'response strength' variable is used in the model equation. Thus the problem of investigating the distribution of reliability estimates using models other than the ANOVA model



becomes the problem of investigating the effects of the violation of the assumptions of the ANOVA model upon the distribution of the reliability estimates.

It is also suspected that, under certain circumstances for real data, cases arise in which the distributional assumptions of (2.14') are substantially violated, that is the distribution of the true scores and the error scores may be skewed, and/or platykurtic or leptokurtic (Lord, 1960, 1969).

However, regardless of which model the real data may satisfy, in practice the reliability estimates are usually obtained using the Alpha or KR20 formulas; hence the distributional theory of the estimates based on these formulas becomes a central concern for the test users as well as the theorist. Thus, it seems justifiable to investigate the distributional problem using models other than the ANOVA model, e.g., those in which a systematically distorted distribution arises for (2.17) by violating (2.7') and/or (2.14'). The assumptions underlying such models are summarized in the following table.

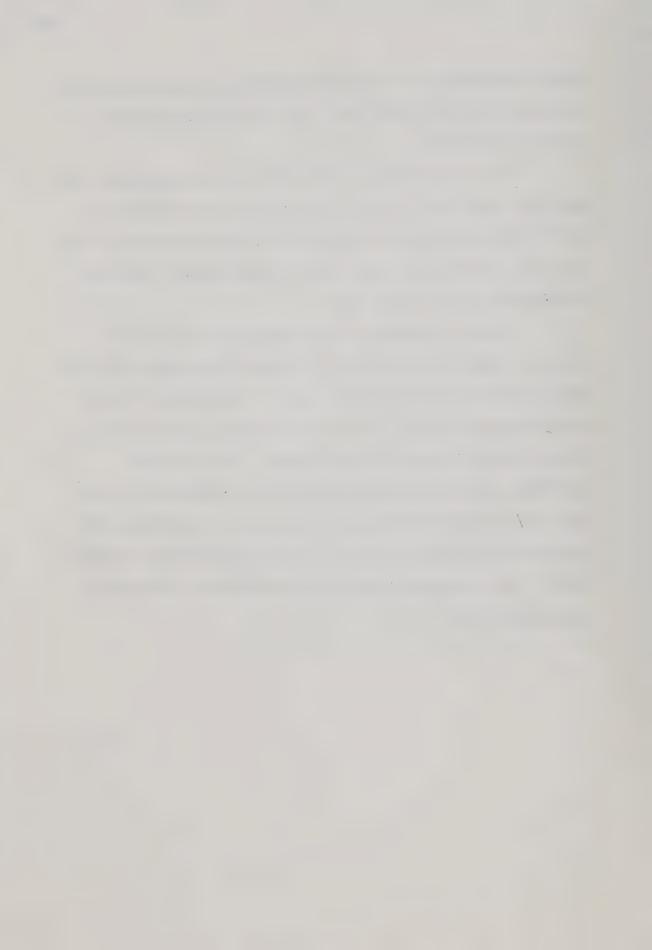


TABLE 4.1
Summary of the Assumptions Under Various Models

Assumptions	ANOVA	ETEM	CONG.	M.F.	N.O.1
independence of true and error scores	yes	yes	yes	yes	yes
uni-factor true scores	yes	yes	yes	no	yes
ETEM assumptions	yes	yes	no	no	no
homogeneity of error score variances	yes	no	no	no	no
normality of true scores	yes	yes	yes	yes	yes
normality of error scores	yes	yes	yes	yes	yes

(Cong. - congeneric; M.F. - multi-factor; N.O. - normal ogive)

4.2 Robustness Under Violation of Assumptions

It has been known that, under certain conditions, the F-test of the one way fixed effects analysis of variance model is quite robust against the violation of the underlying assumptions. It may then be asked whether or not the same robustness exists for inferences about the reliability based on (2.17), which relies on an F-statistic. That is, can the findings for the one way fixed

Applicable only to the response strength variable.



effects model ANOVA be generalized to the two way mixed effects model ANOVA case with one observation per cell. If the sampling distribution of the reliability estimates is stable with the violation of assumptions, statistical inference based on (2.17) would be very powerful. If the sampling distribution of the most often used Alpha or KR20 estimates are found to be quite robust against the violation of the assumption users may freely employ the Alpha and KR20 estimate formulas and perform statistical inferences based on (2.17) without investigating the adequacy of the models or the assumptions. If the distribution is robust only under certain conditions, the researcher should keep this in mind whenever making an inference about the reliability or interpreting an estimate based on (2.17). Therefore, the basic question to be answered is: under what conditions, if any, do the Alpha or KR20 estimates have a stable distribution against the violation of assumptions.

4.3 An Empirical Approach Toward the Problem

Since a mathematical answer to the above problem is not available at the moment, and it seems impossible to give one in the near future, one alternative approach to be considered is the performance of an actual experiment, i.e., an empirical examination of the sampling distribution under various models and assumptions that violate the ANOVA model and its assumptions. The empirical distribution of the Alpha and KR20 estimates can then be found and compared with the theoretical one under the ideal ANOVA model.

An experiment with real data is almost impossible since the population parameters are seldom known. Even if this were possible



the data would not fit the specific model and assumptions except for rather limited cases (e.g., Baker, 1962). One available method is to use computer simulated data, under various assumptions, to obtain empirical distributions of the Alpha and KR20 estimates and compare them with the distribution for the ideal ANOVA model.

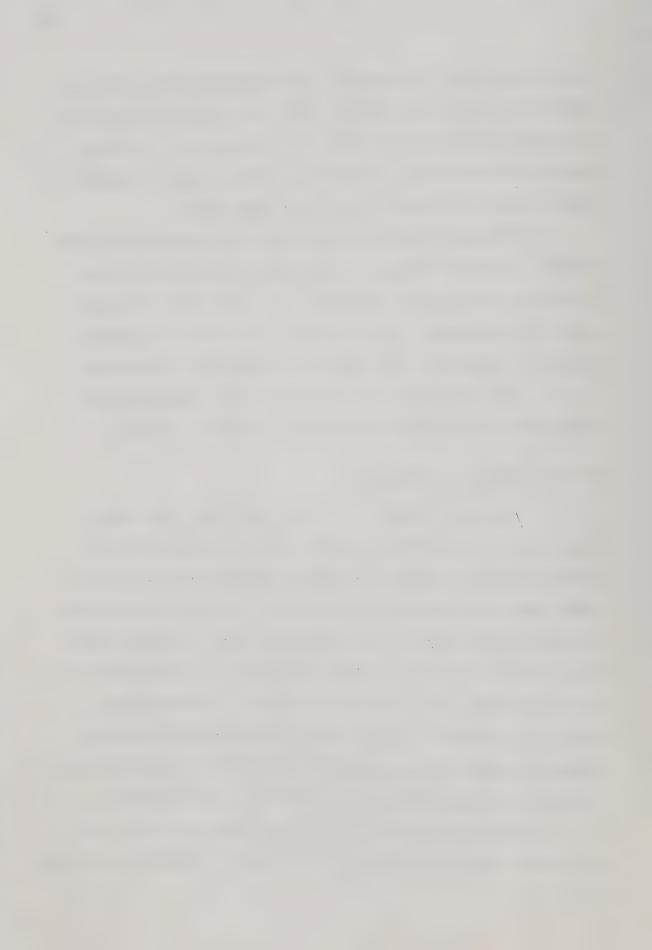
The author has already investigated the feasibility of such computer simulation techniques in the study of the effects of the violation of assumptions on the F-test for linear models requiring statistical inferences, and has provided a comprehensive computer program for educational and psychological researchers (Bay, 1970).

The present study uses essentially the same techniques to investigate the sampling distribution of reliability estimates.

4.4 The Concept of Simulation

The term 'simulation' has been used rather uncritically in a wide range of scientific or economic fields, especially for the purpose of building models. Von Neuman and Ulam's work in the late 1940's, when they attempted to solve certain nuclear physics problems by a Monte Carlo analysis, may be considered the first modern use of the simulation techniques. A Monte Carlo analysis involves the solution of a problem, that is either too expensive for experimental solution or too complicated for analytical methods, by simulating a stochastic process that has probability distributions satisfying the mathematical or probabilistic relations underlying the problems.

With the development of high speed computers in the last two decades, not only physicists and other natural scientists, but also



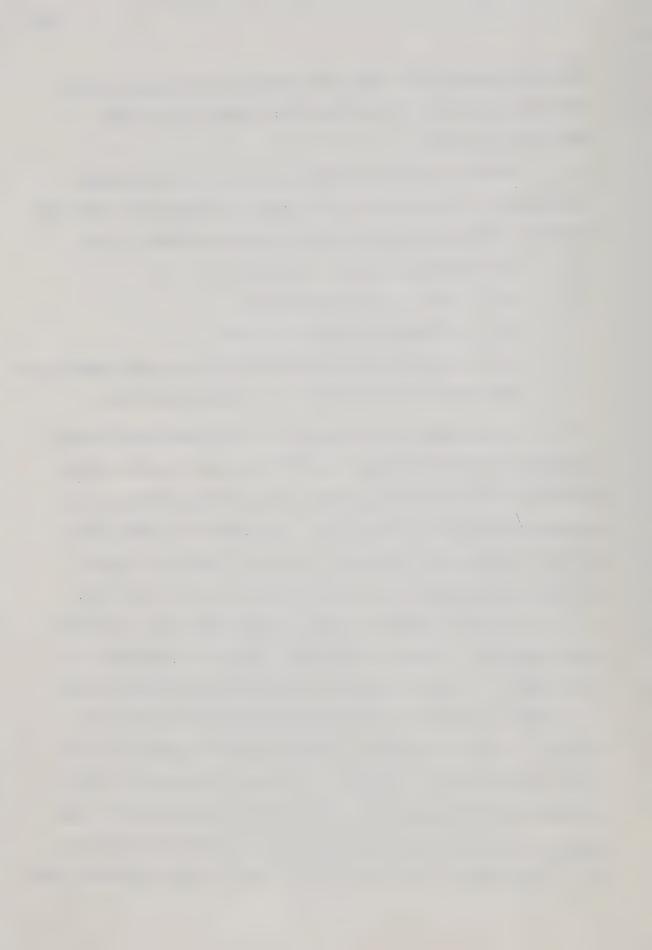
economists, psychologists, and other social scientists can perform controlled laboratory-like experiments on a computer with much efficiency and economy.

Although there is no agreed upon definition of the term 'simulation', for the purpose of this paper it was considered sufficient to use the following definition given by Churchman (1963, p. 12).

'x simulates y' is true if and only if:

- (a) x and y are formal systems,
- (b) y is taken to be the real system,
 - (c) x is taken to be an approximation to the real system, and
 - (d) the rules of validity in x are non-error free.

In the context of this paper, y is a system which produces a number of real test score sets by performing actual random sampling of subjects and administering the test, thus giving a number of real estimates of reliability of the test. The number of estimates under the real situation is limited since the actual sampling of subjects and the administration of the test are involved. On the other hand, x is a system which produces a number of test score sets, via computer, under a model and a number of assumptions which will approximate the real system y. Since the number of test score sets obtainable under x is almost unlimited, the sampling distribution of the relaibility estimates is easily obtainable by calculating the frequency distribution of the estimates. Furthermore, since the test parameters and the distributions of true and error scores can be manipulated easily under computer simulation, almost any combination of models and assumptions can be investigated. The researcher can input the most appropriate model



and assumptions which will best approximate the real system y for a given test and population of subjects.

This approach toward statistical inference is somewhat different from the conventional procedure since the user can choose the model and assumptions of interest to him, while in the conventional case the model and assumptions are predetermined by the mathematical statisticians and the user can only choose whether or not to accept the conditions and the model, look for alternatives, or give up. In this sense computer simulation techniques permit the study of sampling distributions under almost unlimited combinations of models and assumptions. Thus, the user may obtain the sampling distribution of a statistic under his own model and assumptions in the experimental situation, make statistical inferences, and use the knowledge so gained in practice. Because of the fourth property of the simulation, the method may not provide exact answers, but it would provide approximate answers to distribution problems.

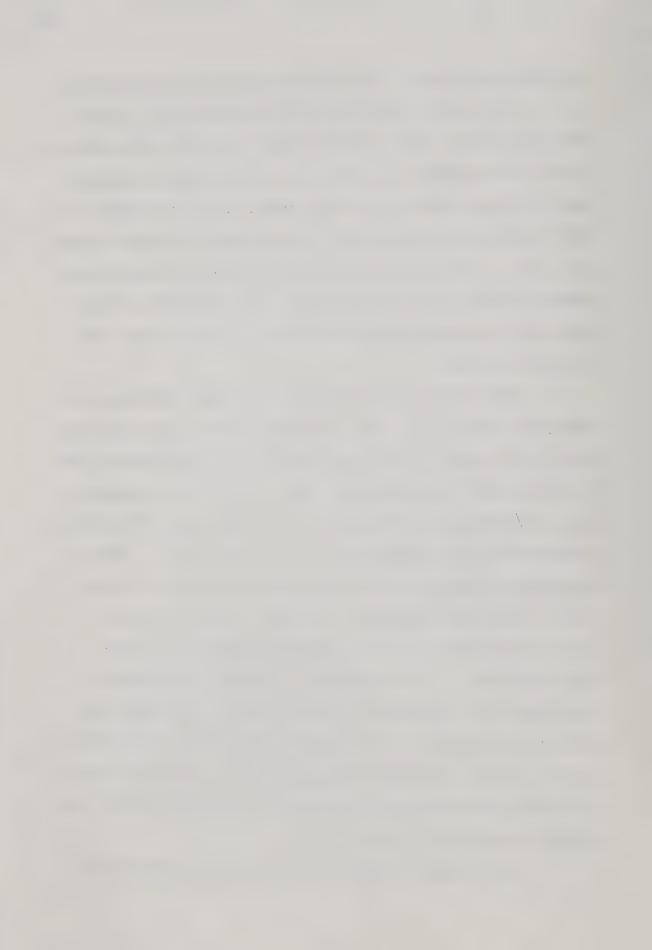
4.5 Computer Programs

Two computer programs named RELO1 and RELO2 have been developed in FORTRAN IV on the IBM 360/67 computer of the University of Alberta computer system for continuous part test and binary item test cases respectively. The programs are in sufficient general form so that they can be used for other problems related to sampling distribution of reliability estimates not considered part of the study. The programs automatically simulate the test score matrix $\underline{Y} = \{y_{ij}\}$ for the continuous case, or $\underline{X} = \{x_{ij}\}$ for the binary case based on input models, parameters, and specified distributions of true or latent



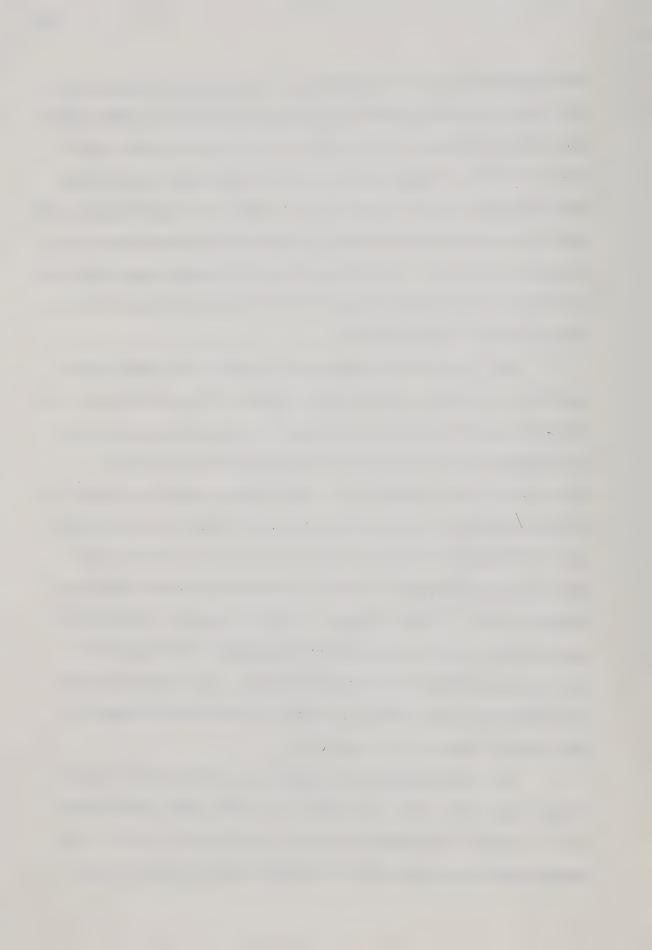
scores and error scores. The programs have the following features:

- (a) For the continuous case, the program RELO1 uses the most general model, namely the multi-factor true score model given by (2.18), and accommodates all other less general models as special cases. Users are able to specify the sample size I, the number of parts J, and the parameter vector and matrices for the model, namely $\underline{\mu}$, $\underline{\Lambda}$, and $\underline{\Psi}$, i.e., mean vector, factor loading matrix, and error standard deviation matrix respectively. The program will evaluate population test parameters such as reliability, Alpha, mean, true and error variances.
- (b) For the binary item case, the program RELO2 uses the normal ogive model (3.1), under a uni-factor latent scores assumption, and allows the user to specify the sample size I, the number of items J, and the basic item parameters, namely the difficulty parameters $\{\pi_j^2\}$ and the biserial correlations $\{\lambda_j^2\}$. The program will evaluate the population test parameters such as ρ , KR20, and σ_X^2 based on the Tchebycheff-Hermite polynomials discussed in Chapter Three and other formulas under the normal ogive model. However, these calculations are valid only for the normal distributions of latent scores and errors. If the normality is violated, the parameters calculated are no longer valid, unlike the case of continuous parts where the test parameters are independent of distributions of true and error scores. To evaluate test parameters for non-normal cases, an empirical method based on a parallel form method described in the following Section 4.6 is used.
 - (c) For both programs the user may decide shapes of the



distributions of true or latent scores $\{f_i\}$ and error scores $\{\epsilon_{ij}\}$. The programs generate specific distributions by means of random number generating subroutines. The distributions of true or latent scores and error scores are specified by user supplied subroutines DIST and DISE respectively for non-normal cases. These two subroutines may call the uniform random number generating subroutine VECRAN described in the following Section 4.7. For the normal case, the program generates the distribution automatically by employing the Box-Muller method which is also described in the Section 4.7.

- (d) The programs automatically perform N simulations, as specified by the user, and calculate a number of test statistics. The reliability coefficients are estimated for each simulated test score matrix based on the formula (2.13), regardless of the model and distributions used to generate the score matrix, since the formula is, as was noted before, the one most often used by the test theorists or users. Alternatively or concurrently, as an option, the user may adopt an unbiased estimation formula developed by Kristoff (1963) and discussed in the following chapter. The distributions of reliability thus estimated are then compared with those obtainable from (2.17), i.e., the ideal ANOVA model and normal theory. For non-normal binary item test cases, the reliability parameter obtained by the parallel form method is used for the value of ρ .
- (e) The programs also summarize the empirical distributions of MS $_A$, MS $_B$, MS $_e$, and $\hat{\rho}$ by calculating their means and variances over N samples, and compares them with the theortical values of the expected mean and variance under the ANOVA model and normal theory



assumptions. For the binary item case, the variance parameter σ_A^2 and σ_e^2 in terms of the test score \mathbf{x}_i are not defined or calculable directly. However, from the definition of reliability given by (2.12) and the variance given by (2.10), a generalization of the relationships between reliability and variances to binary item cases may be made such that the formulas in Chapter Two may be used without modification, namely,

(4.1)
$$\sigma_{A}^{2} = \frac{\rho \sigma_{X}^{2}}{J^{2}}; \qquad \sigma_{e}^{2} = \frac{(1-\rho) \sigma_{X}^{2}}{J}, \text{ or }$$

(4.1')
$$\sigma_A^2 = \frac{\rho^* \sigma_X^{*2}}{J^2}, \quad \sigma_e^2 = \frac{(1-\rho^*)\sigma_X^{*2}}{J},$$

for non-normal cases, where the star (*) notation referes to parameters evaluated by the parallel form method.

(f) Comparisons between the empirical distributions of reliability estimates based on either or both (2.13) or Kristof's unbiased formula, with those theoretical ones based on (2.17) or modified form of it for the unbiased formula, can also be made as an option by plotting both distributional curves together in a graph.

Computer program listings together with example outputs of the programs are given in Appendix A.1 and A.2 respectively.

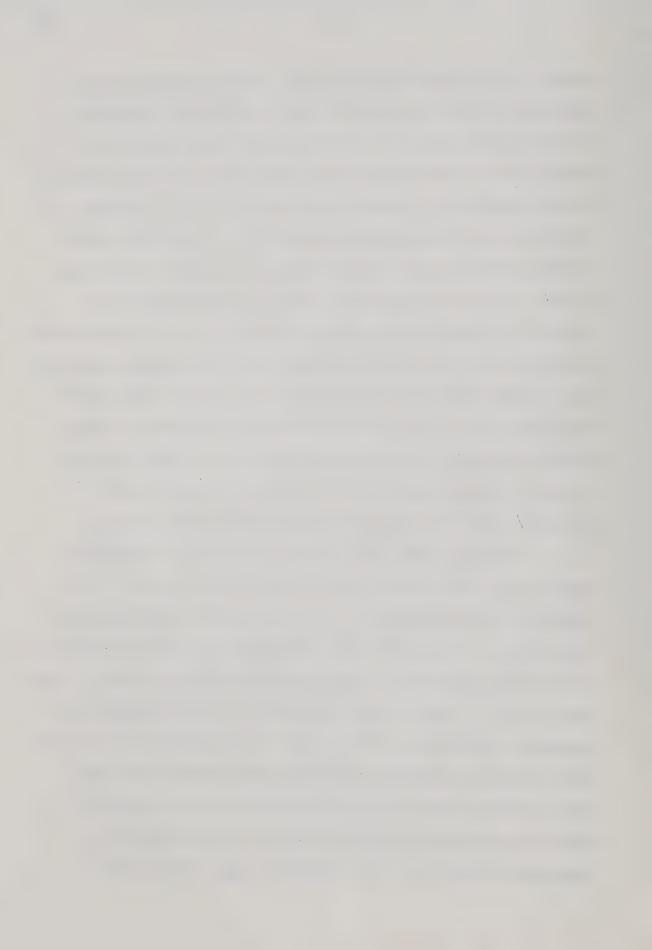
4.6 Parallel Forms Method for Test Parameters of Binary Item Test

For the continuous part test cases, test parameters such as $\sigma_{\gamma}^{2}, \quad \rho, \quad \text{and} \quad \text{Alpha depend only on the input of part test parameters}$ and are independent of the distributions of the true and error scores.



However, for the binary item test cases, the basic test parameters depend not only on item parameters such as difficulty or biserial correlations but, also on the distributions of latent scores and errors, since the normal ogive model connects the continuous response strength variable y_{ij} to the binary item score x_{ij} . Therefore the formulas for test parameters such as σ_{x}^{2} , ρ , and KR20 given in Chapter Three are valid only for the case of normal distributions, In order to be able to investigate the sampling distributions of reliability estimates under non-normal cases, i.e., under the assumption violating cases of the normal ogive model, the test parameters must be known by means other than these formulas. Although for some simpler distributions such as the uniform distribution, evaluation of these parameters by analytical means might be possible, a general solution to cover all types of possible distributions is impossible, and alternative empirical methods are employed in the RELO2 program.

Since the number (N) of test score matrices simulated is usually large, say at least 1000, the number of test scores (N \times I) simulated in each experiment is a very large number compared with the sample size I. On the other hand, the sample reliability and variance are consistent estimators of the corresponding population values. Therefore, if N \times I test score sets are used at a time to estimate these parameters, the estimates will be close to the population values. However, to obtain a population reliability coefficient by this large sample method and the correlation formula give by (3.12), parallel form test scores must also be simulated which have identical f_i terms but different ϵ_{ij} terms denoted by ϵ_{ij}^* due to random



fluctuation of responses. Therefore, two sets of model equations may be considered for the response strength variables y_{ij} , namely,

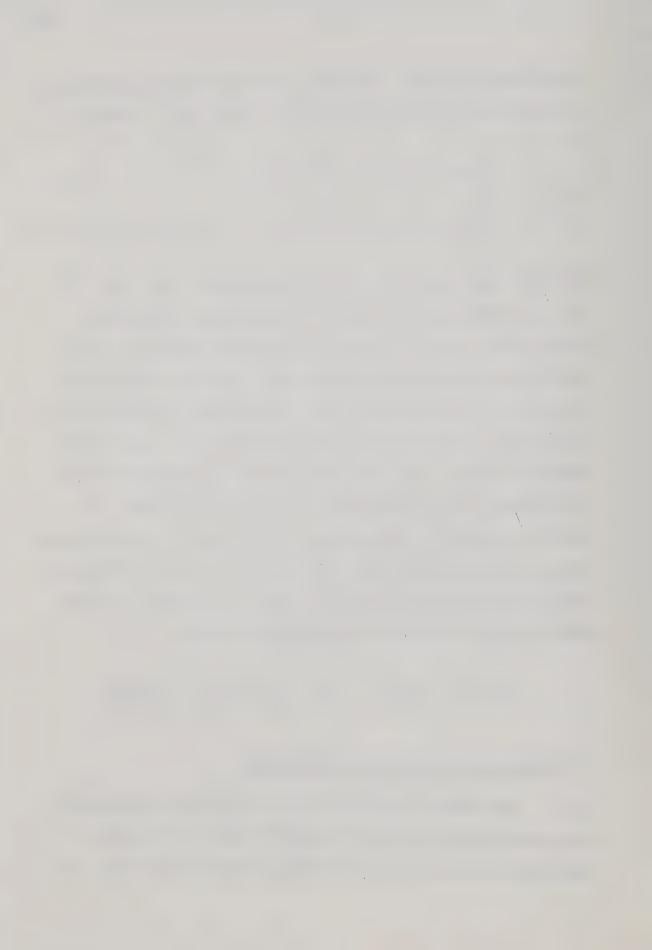
(4.2)
$$\begin{cases} y_{ij} = \lambda_{j} f_{i} + (1 - \lambda_{j}^{2})^{\frac{1}{2}} \epsilon_{ij}, \\ y_{ij}^{*} = \lambda_{j} f_{i} + (1 - \lambda_{j}^{2})^{\frac{1}{2}} \epsilon_{ij}^{*}; \quad i = 1, ..., NI; \quad j = 1, ..., J. \end{cases}$$

Form these model equations, two sets of test scores $\{x_i^*\}$ and $\{x_i^*\}$ may be generated, and by calculating the correlation coefficient between these two sets of scores, the population reliability may be obtained regardless of which distribution is used for simulating the test scores. For ideal normal cases, the parameters obtained by this method should agree closely with the calculated values based on the formulas of Chapter Three, providing one way of checking the formulas in the chapter and the computing procedures adopted by RELO2. The population parameters thus estimated will be denoted by the corresponding population parameter symbols with a star (*) sign to distinguish them from those obtained by analytical means. For example, the test mean and variance obtained by this method are given by,

$$\mu^* = (\sum_{i} x_{i})/NI$$
, and $\sigma_{x}^{*2} = \{\sum_{i} (x_{i} - \mu^*)^{2}\}/NI$.

4.7 Procedures for Generating Random Numbers

The method of generating a set of independent random numbers with a specific distribution by a computer program is of extreme importance to the success of a stochastic simulation experiment. The



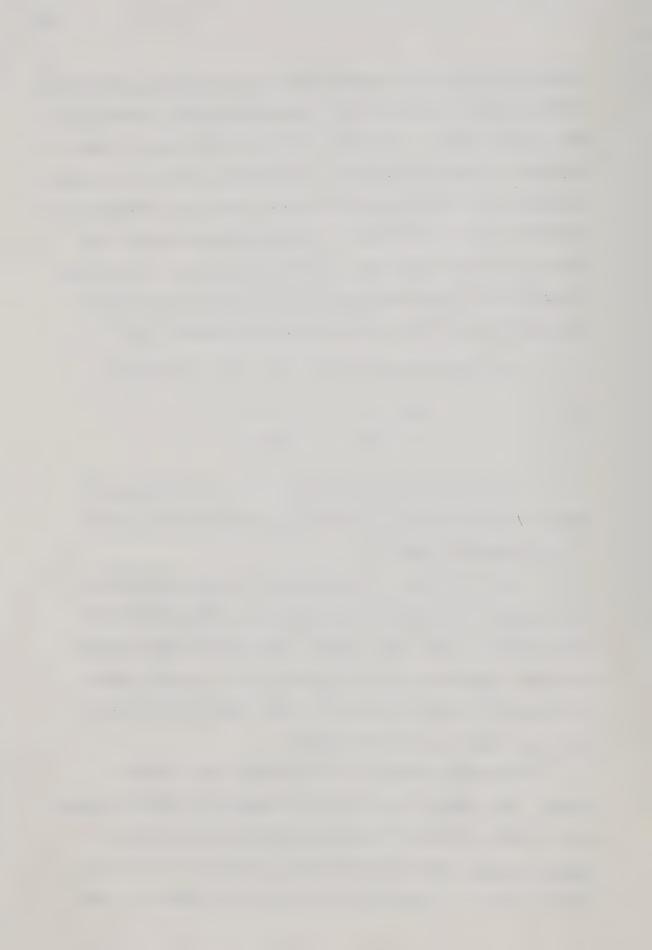
simplest and basic set of random numbers with a continuous probability density function is the one that is constant over the interval (0,1) and is zero otherwise. The density function defines what is known as a uniform or square distribution. The principal value of the uniform distribution for the simulation techniques lies in its simplicity and in the fact that it can be used to simulate random variables from almost any kind of probability, distribution since the inverse transformation of the cummulative distribution function of any random variables results in the uniform distribution between (0,1).

The uniform density function on (0,1) is defined by f(z) = 1.0 0 < z < 1 = 0.0 otherwise.

Due to its simple density function, it is very easy to evaluate moments for such a uniformly distributed random variable by using elementary calculus.

For this study, the method used for generating uniform random number is the same as that used by the IBM Scientific Subroutine Package RANDU (IBM, 1968). The subroutine named VECRAN can however generate a specified number of uniform random numbers at a time and provides the output in vector form, while only one number at a time is generated by RANDU.

The method employed is the so-called 'power residue method', (IBM, 1959) or 'multiplicative congruential method' (Nayler et al., 1968, p. 51-52). The method generates successive non-negative integer random number which are less than 2^C for binary computers where c denotes the word size of the computer by means



of a congruence relation, namely,

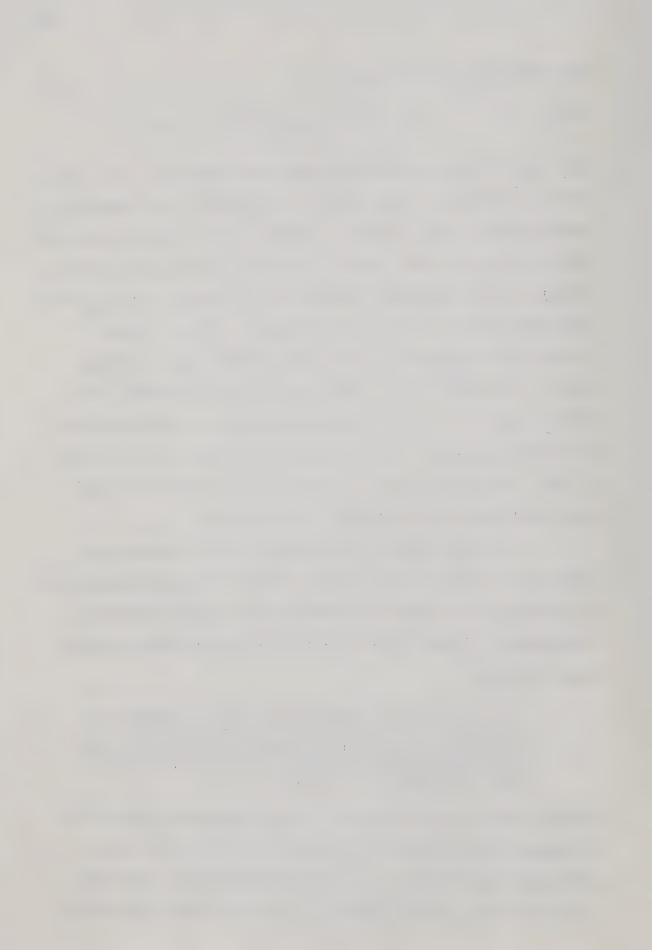
$$n_{i+1} = a n_i \pmod{2^c}, i = 0,1,...$$

where n_0 is the so-called seed random number denoted by IX in the program. Meanings of 'power residue', 'congruential' or 'modulo' are given by Nayler et al., (1968, pp. 63-66), or can be found in any text-book of elementary number theory. The formula (4.4) is the so-called formula for generating power residuals, and results in $u = n_{i+1}/(2^c-1)$ being approximately a uniform random number in (0,1). For the IBM 360 series computers, c = 31, and VECRAN uses a = 65539, and $2^{-c} = 0.4656613 \times 10^{-9}$ which are the same as for RANDU. The user must specify $n_0 = IX$ as an input parameter at the beginning of the program execution, and it must be an odd integer with nine digits or less. The last value of n_i generated may be used as an input seed random number IX for the next step generation.

The random numbers thus generated are often referred as pseudo-random numbers, and the method involves the generating procedure by 'indefinitely continued transformation of a group of arbitrarily chosen numbers' (Tocher, 1954, p. 41). The term has been defined by Lehmer (1951) as,

... a vague notion embodying the idea of a sequence in which each term is unpredictable to the uninitiated and whose digits pass a certain number of tests, traditional with statisticians and depending somewhat on the use to which the sequence is to be put.

Although there are some objections on the philosophical grounds that the sequence is generated by a deterministic rule of (4.4), use of such pseudo-random numbers can be defended by pragmatic reason that a sequence may be regarded random if it satisfies some predetermined



statistical tests of randomness, and the uniform number generated by RANDU has been known to satisfy these requirements (IBM, 1968).

Based on the uniform random numbers thus generated by VECRAN, denoted by U1, five other kinds of random numbers are generated for this study. For the selection of these specific types of a random number the following factors were taken into account:

- (a) Ease of generation and computer time required for computation.
- (b) Ease of evaluating the moments of random numbers by calculus to ensure that the program generates random numbers with the required distribution.
- (c) Some practical usefulness. For example, normal, uniform, and exponential distributions are included because the approximation of the normal distribution to real data is so often assumed, the uniform distribution is closely associated with ranked data, and the exponential distribution can arise with the truncated data of normal distribution due to a selection process.

The six kinds of random numbers, including U1, are summarized in the following table.



TABLE 4.2
Summary of the Random Numbers

Description	Notation	Transformation Formula		
Uniform, (0,1)	Ul	z = u ₁		
Sum of 2 indep. Ul	U2	$z = \{(u_1 + u_2) - 1.0\} \times (6)^{\frac{1}{2}}$		
Sum of 3 indep. Ul	U3	$z = \{(u_1 + u_2 + u_3) - 1.5\} \times 2$		
Sum of 6 indep. Ul	U6	$z = \{(u_1 + u_2 + + u_6) - 3.0\} \times (2)^{\frac{1}{2}}$		
Normal	NO	$z_1 = (-2 \text{ Ln } u_1)^{\frac{1}{2}} \text{ Cos } (2\pi u_2)$		
		$z_2 = (-2 \text{ Ln } u_1)^{\frac{1}{2}} \text{ Sin } (2\pi u_2)$		
Exponential	EX	$z = -Ln (u_1) - 1.0$		

Note: u₁,...,u₆ denote the uniform random numbers generated by VECRAN.

The method used for the generation of standard normal random variables is the same as given by Box and Muller (1959). Since the distribution is exact, it has an advantage over the so-called central limit approach which uses the sum of a number of independent uniform random variables. All random variables in this study were used in standard form, namely with an expected value of zero and unit variance, except U1 which was standardized by subtracting 0.5 and multiplying by the square root of 12.0. Therefore the random numbers thus generated can easily be used as $\{f_{\vec{i}}\}$ or $\{\epsilon_{\vec{i}\vec{j}}\}$ of the model equations (2.28), (3.3), and (4.2).



A number of preliminary sampling experiments were performed to ensure that this method generates the random numbers with desired distributions. To see whether the means, variances and other statistics for large samples closely approximated the population values of the distribution simulated by the random numbers, five samples of size 6000 each were generated for each distribution, and the obtained statistics were compared with the population values obtained from the knowledge of the probability density functions and the application of elementary calculus. The results are summarized in Table 4.3. With some exceptions for the calculated kurtosis of the distribution noted with (*) sign, the sample statistics approximate reasonably well the population values. The exceptional cases are probably due to the imperfections of the random number generating procedures and sensitivity of kurtosis to the shapes of the distribution. The calculated auto-correlations are almost zero indicating no serial correlations for adjacent random numbers in the sequences and the degree of independence of random numbers thus generated.

4.8 Methodological Limitations

Because the computer simulated experiments cannot be exhaustive and cover all possible combinations of models, parameter sets, and distributional assumptions, and due to the very nature of computer simulation techniques and limited funds available for the computing charges, the following methodological limitations are imposed on this study.

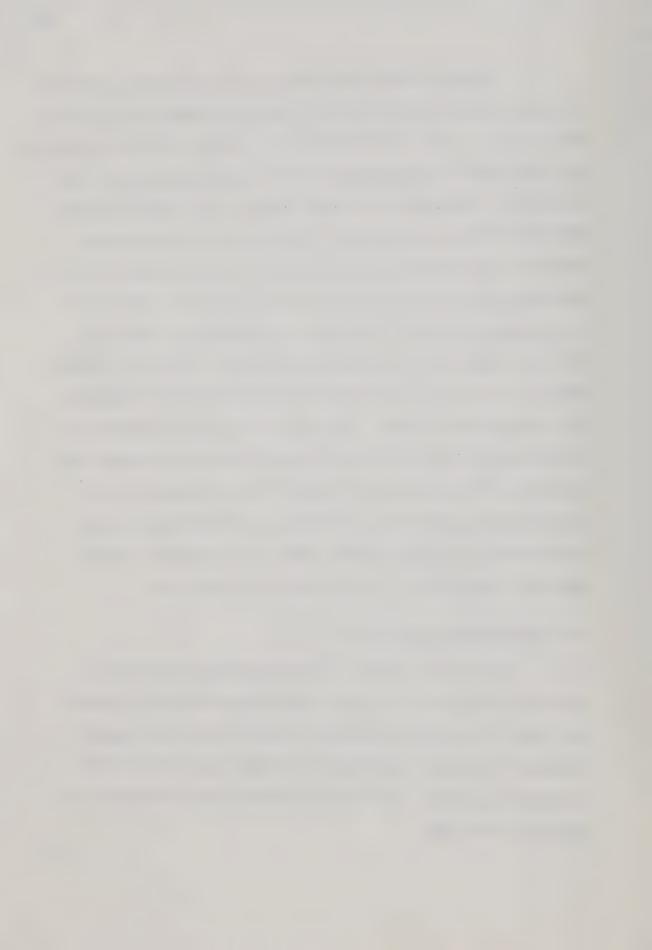
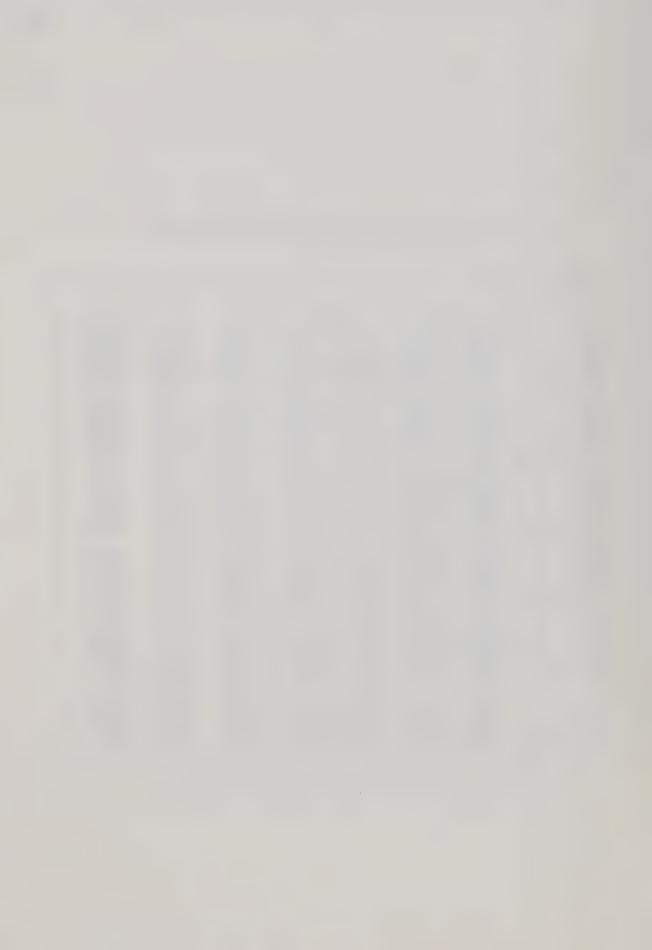


TABLE 4.3

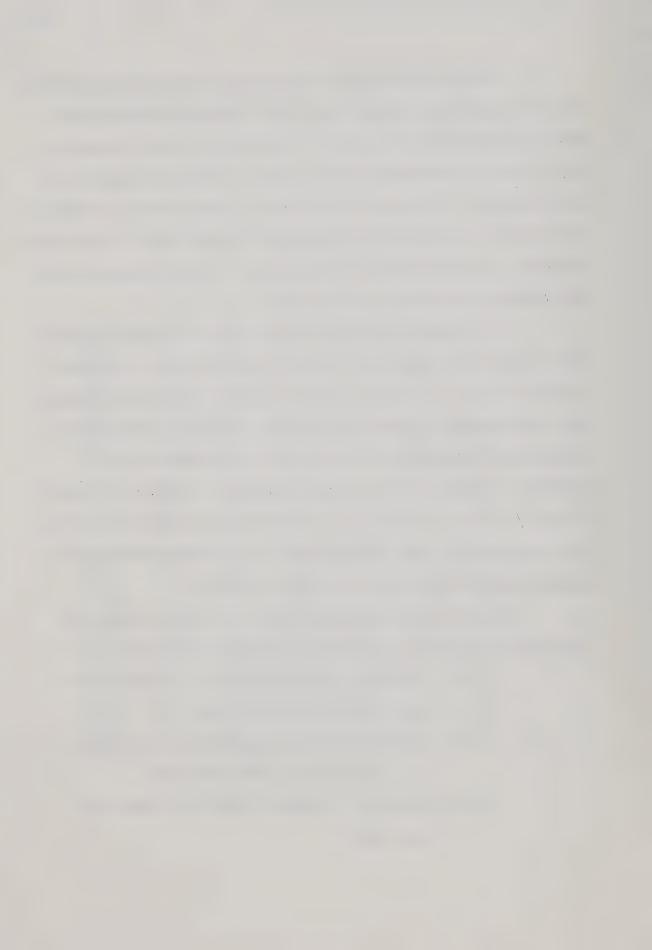
Descriptive Summary of Random Numbers Generated by Pseudo-Random Number Generating Subroutines, Sample Size = 6000 for Each Trial

Dis	Trial	Mean	Var.	Skewness	Kurtosis	Auto-Correlations		
						Lag 1	Lag 2	Lag 3
U1	1	0.50347	0.08417	-0.01615	-1.21110	0.00153	-0.00182	0.00152
Ul	2	0.50027	0.08500	-0.00620	-1.23131	0.00029	0.00054	-0.00206
Ul	3	0.50080	0.08367	-0.02638	-1.20730	-0.00070	0.00045	-0.00049
U1	4	0.49840	0.08320	-0.01426	-1.19213	0.00036	0.00174	0.00073
Ul	5	0.50682	0.08226	-0.02995	-1.18213	0.00118	0.00052	0.00005
U1	Expected	0.50000	0.08333	0.00000	-1.20000	0.00000	0.00000	0.00000
U2	1	0.03035	0.99873	-0.00577	-0.58865	0.02595	-0.22086	-0.00478
U2	2	0.01817	0.98648	-0.02644	-0.59803	0.01458	-0.00631	0.00929
U2	3	-0.00268	1.01429	0.00608	-0.63365	0.00781	0.02034	-0.00341
U2	4	0.01204	0.98045	-0.02414	-0.58109	-0.01133	0.01728	0.00093
U2	5	0.02277	1.01143	-0.00802	-0.65140	0.02078	0.02055	0.00163
U2	Expected	0.00000	1.00000	0.00000	-0.60000	0.00000	0.00000	0.00000
U3	1	0.02933	1.00741	0.00310	-0.42060	0.02305	-0.01435	0.01603
U3	2	0.01852	0.95938	0.00809	-0.30457	0.01778	-0.01994	0.00278
U3	3	-0.00475	1.00159	-0.01646	-0.37746	0.00498	0.01504	-0.00118
U3	4	0.00062	0.99190	-0.02163	-0.37966	-0.00196	0.00308	-0.00630
U3	5	0.01843	1.02359	-0.01513	-0.40427	0.00996	0.00901	-0.00601
U3	Expected	0.00000	1.00000	0.00000	-0.40000	0.00000	0.00000	0.00000
υ6	1	0.01903	0.98999	-0.01882	-0.23413	-0.01181	-0.01000	0.02742
U6	2	0.00843	0.97866	0.00333	-0.20790	-0.00566	-0.02743	0.02315
U6	3	-0.00411	1.00637	-0.00300	-0.22061	-0.01835	-0.01835	0.02315
U6	4	0.00294	0.99037	-0.01588	-0.24665	-0.00398	0.00064	-0.01555
U6	5	0.01480	1.03165	-0.00895	-0.16114	0.00049	0.01274	0.00500
U6	Expected	0.00000	1.00000	0.00000	-0.20000	0.00000	0.00000	0.00000
NO	1	0.00587	1.01532	-0.00714	0.11501*	0.01517	0.01176	-0.00349
NO	2	0.00214	0.99160	-0.05184	0.05017	-0.00904	0.02503	-0.01246
NO	3	-0.00856	0.99918	-0.00635	0.03248	0.02173	-0.02119	0.03329
NO	4	-0.00069	0.99955	0.02294	-0.04551	0.01060	-0.02274	-0.00699
NO	5	-0.01763	0.97289	0.01456	-0.05775	-0.01532	-0.00687	0.00793
NO	Expected	0.00000	1.00000	0.00000	0.00000	0.00000	0.00000	0.00000
EX	1	-0.00475	1.01587	2.00600	5.70110	0.00894	-0.01838	0.01769
EX	2	0.00565	1.01611	1.93136	5.31563	0.00892	0.01781	-0.01341
EX	3	0.00586	1.05517	2.19383	8.02954*	-0.00005	-0.00905	-0.01218
ξX	4	0.00866	1.01780	1.91303	4.91614*	0.00727	0.01803	-0.00044
EX	5	-0.02518	0.96299	2.03853	6.10958	0.00473	-0.00114	0.00189
EX	Expected	0.00000	1.00000	2.00000	6.00000	0.00000	0.00000	0.00000

Note: All random numbers are standardized by population mean and variance except U1.



- (a) The investigation is restricted to the sampling distributions of reliability estimates under Type I sampling situation only, namely only sampling of subjects is involved; the test is assumed to be given and all parameters for part-tests or items are assumed to be fixed constants. The distributions under the Type 2 or Type 12 sampling situation, such as the distributions of generalizability coefficient estimates, are not considered in this study, although this may be done very easily as an extension to this study.
- (b) Because the computer time required for each experiment must be kept within reasonable limits, the sample size I, the number of parts or items J, and the number of samples to be simulated must be kept within moderate bounds for this study. Therefore, although the programs are dimensioned such that they can accommodate up to N = 5000, I = 100, J = 30, investigations are limited to N = 2000 or 1000, I = 30, J = 6, 8, or 9 to restrict each experiment within 5 to 7 minutes of C.P.U. time which costs approximately \$20-30 at the present charging rate of the University of Alberta.
- (c) To conserve computer time for the overall study, the experiments have focused only on the following key problems:
 - (i) The effect of non-normal true or latent scores and error scores distributions.
 - (ii) The effects of non-homogeneous error variances,i.e., distributions under ETEM model.
 - (iii) The effect of congeneric and multi-factor true score model.



- (iv) The effect of binary item scores, non-homogeneous difficulty parameters and biserial correlations, and non-normal distributions.
- (d) The non-normal distributions used in this study are limited to a minimal number of well known distributions outlined in Section 4.7.

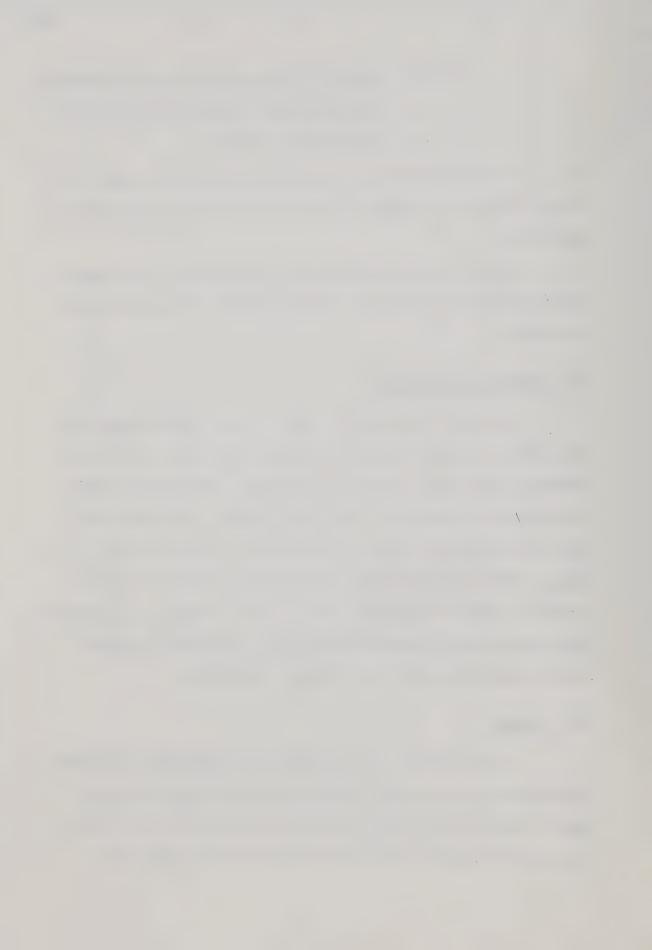
Because of these limitations, the findings of this study will be limited to some extent in their generalization to all 'real' situations.

4.9 Accuracy of Calculation

Like any other numerical analysis, the results reported in this study are subject to certain computational errors. The figures reported in this study retain, in most cases, three decimal places, but they may be inaccurate in the right most one significant digit due to the cummulative effects of errors when the sample size N is large. This is especially true for the case when the variance of a variable is small in comparison with the mean. However, it is expected that the errors are confined only within 3 to 4% level at maximum, and they would not affect the findings of this study.

4.10 Summary

In this chapter, the rationale for investigating the sampling distributions of reliability estimates as assumption violating cases of the well known ANOVA model and normal distributional theory, and using the computer simulation technique to investigate such



problems were discussed. The computer programs developed for this study were outlined, and the parallel form method, the random number generating procedures, and the methodological limitations due to the very nature of computer simulation techniques were also discussed.



CHAPTER FIVE

RESULTS FOR CONTINUOUS PART TEST SCORE CASES

This chapter presents the results of the computer simulated experiments for the continuous part test score cases. Section 5.1.0 deals with the effects of non-normality under the ANOVA model; and some analytical methods are also used to investigate the standard error of reliability estimates. The distributions of reliability estimates under the ETEM model are dealt with in Section 5.2.0, and in Section 5.3.0 for the congeneric and multi-factor true score cases, i.e., non-ETEM cases.

5.1.0 Effects of Non-Normality Under the ANOVA Model

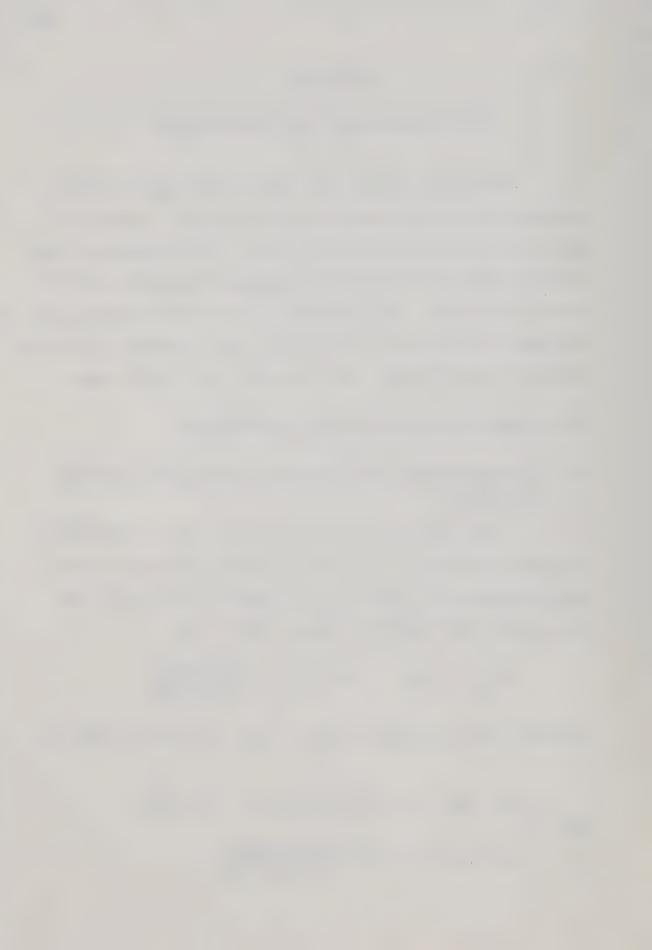
5.1.1 <u>Distribution Under ANOVA and Normal Distribution of True and</u> Error Scores

It has been shown in Chapter Two that, under the ANOVA model and normal distribution, the reliability estimate given by (2.13)-(b) can be related to an F-statistic by the equation (2.17), and it can also be shown that (Kendall and Stuart, 1963, p. 393),

$$E(F_{m;n}) = \frac{n}{n-2}$$
, $Var(F_{m;n}) = \frac{2 n^2 (n+m-2)}{m(n-2)^2 (n-4)}$.

Therefore, using the relation $1/F_{m;n} = F_{n;m}$, it is easy to show that,

(5.1)
$$\begin{cases} (a) & E(\hat{\rho}) = 1 - (1-\rho) \ E(F_{\nu; 1-1}) = 1 - (1-\rho) \frac{1-1}{1-3} \\ (b) & Var(\hat{\rho}) = (1-\rho)^2 \frac{2(1-1)(\nu+1-3)}{(J-1)(1-3)^2(1-5)} \end{cases}.$$



Hence $\hat{\rho}$ is in general a biased, but consistent estimator and does not have the minimum variance property. Kristof (1963) modified formula (2.13) to obtain the unbiased estimator $\hat{\hat{\rho}}$ and has shown that it has a smaller variance than $\hat{\rho}$, namely

(5.2)
$$\begin{cases} (a) & \hat{\rho} = \frac{2}{1-1} + \frac{1-3}{1-1} & \hat{\rho} = \frac{2}{1-1} + \frac{1-3}{1-1} & (1 - MS_e/MS_A), \text{ or} \\ \\ (b) & F_{1-1}; v = \frac{(1-3)(1-\rho)}{(1-1)(1-\frac{\pi}{\rho})} \end{cases}.$$

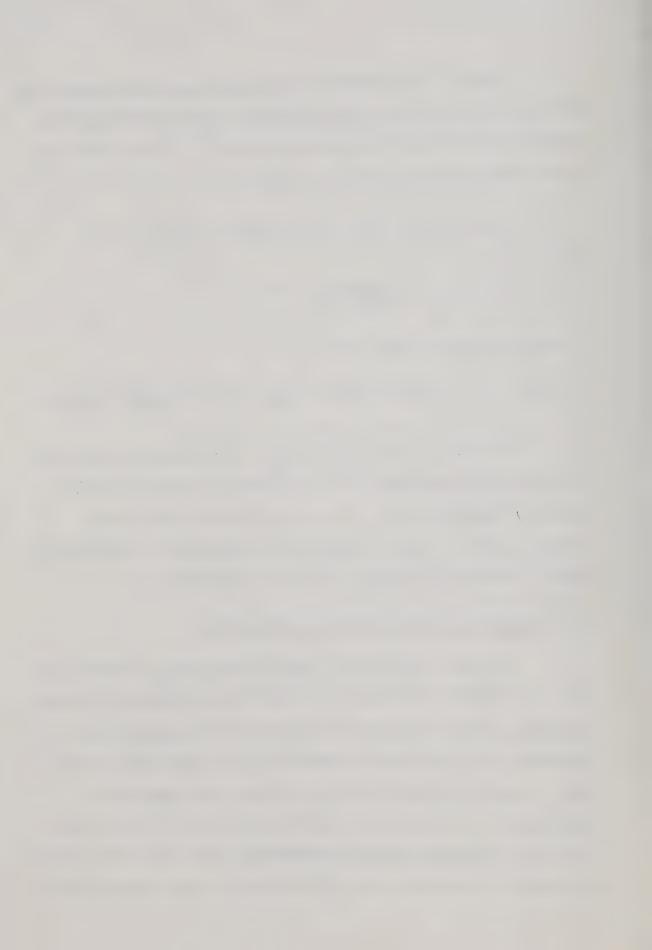
It can then be easily shown that

$$E(\hat{\rho}) = \rho;$$
 $Var(\hat{\rho}) = \left[\frac{1-3}{1-1}\right]^2 Var(\hat{\rho}) = (1-\rho)^2 \frac{2(\nu+1-3)}{\nu(1-5)} \le Var(\hat{\rho}).$

Therefore, if the equation (2.6) is the appropriate model for the data and the assumptions (2.7) and (2.14) are all satisfied, the results of equations (2.17), (5.1), or (5.2) can be used to make inferences about ρ and to calculate the standard error of estimation which is defined as the square root of the variance of $\hat{\rho}$.

5.1.2 Known Effects of Non-Normality Under ANOVA

As it has been seen, the sampling theory and the formula for the standard error of estimation rely heavily on the normal distribution assumptions, despite the fact that real data seldom satisfy these assumptions, and at best may be expected to only approximately satisfy them. It does not logically follow, of course, that approximate satisfaction of the normal distribution assumptions by true and error scores will guarantee automatic approximation of the actual distribution of reliability estimates to the distribution given under normal theory.



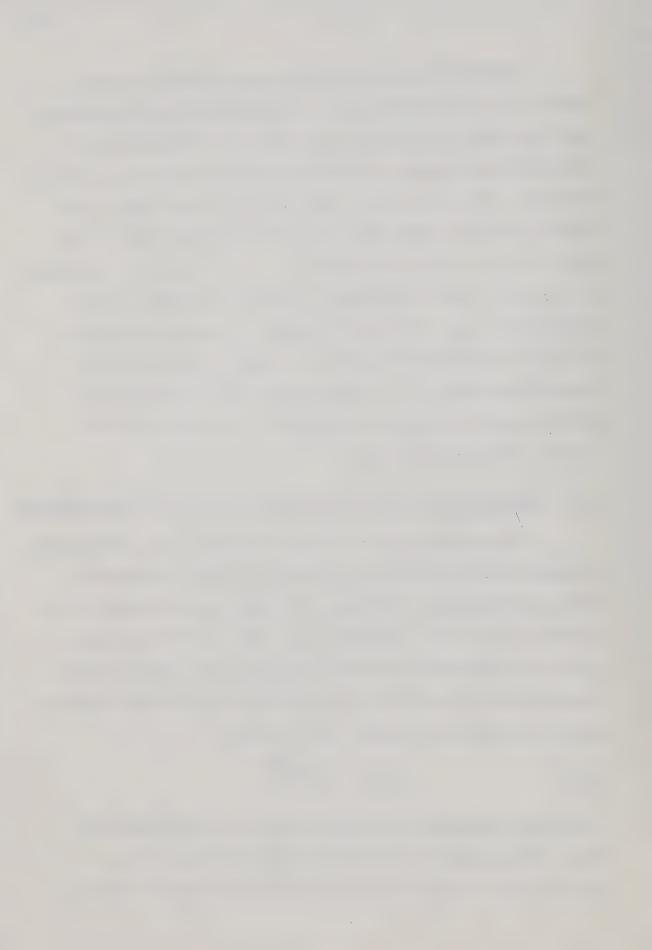
Scheffé (1959, p. 345) investigated the effect of non-normality from an analytical point of view and concluded 'Non-normality has little effect on inferences about means but serious effects on inferences about variances of random effects whose kurtosis γ_2 differs from zero'. He also noted that 'The direction of the effect is such that for confidence coefficients $1-\alpha$ and significance level α the true α will be less than the nominal α if the $\gamma_{2,A} < 0$, and greater if $\gamma_{2,A} > 0$, and the magnitude of the effect increases with the magnitude of $\gamma_{2,A}$.' Although his argument is based on the inference of the so-called signal-noise ratio $\theta = \sigma_A^2/\sigma_e^2$, under the one way random effects model, it is suggestive for reliability theory, and provides a guideline for the investigation of the effects of non-normality under the ANOVA model.

5.1.3 Standard Error of Reliability Estimates Corrected for Non-Normality

The standard error of reliability estimates is a useful measure of the precision of the estimates, although, as noted in Chapter One, without any knowledge of the shape of the sampling distributions of the estimates it has little inferential use. Since reliability has been historically identified as a correlation coefficient, the well-known standard error of correlation coefficient estimates has been frequently used (e.g., Jackson and Ferguson, 1941), namely,

(5.3)
$$\operatorname{Var}(\beta) = \frac{(1-\rho^2)^2}{1}$$

in which the assumption of bivariate normality is made (Kendall and Stuart, 1963, p. 236). However, this formula or those given by equations (5.1) and (5.2) would be misleading if normality cannot be



assumed. General distributional theory under non-normal true and error scores is not yet known, but the Var (β) or its square root, denoted by S.E. (β), may be evaluated approximately if the kurtosis of the true and error scores, denoted by γ_A and γ_e respectively, are known or can be estimated. In this case

(5.4)
$$\begin{cases} (a) & \gamma_{A} = [E(a_{i}^{4})/\sigma_{A}^{4}] - 3, \\ \\ (b) & \gamma_{e} = [E(e_{ij}^{4})/\sigma_{e}^{4}] - 3. \end{cases}$$

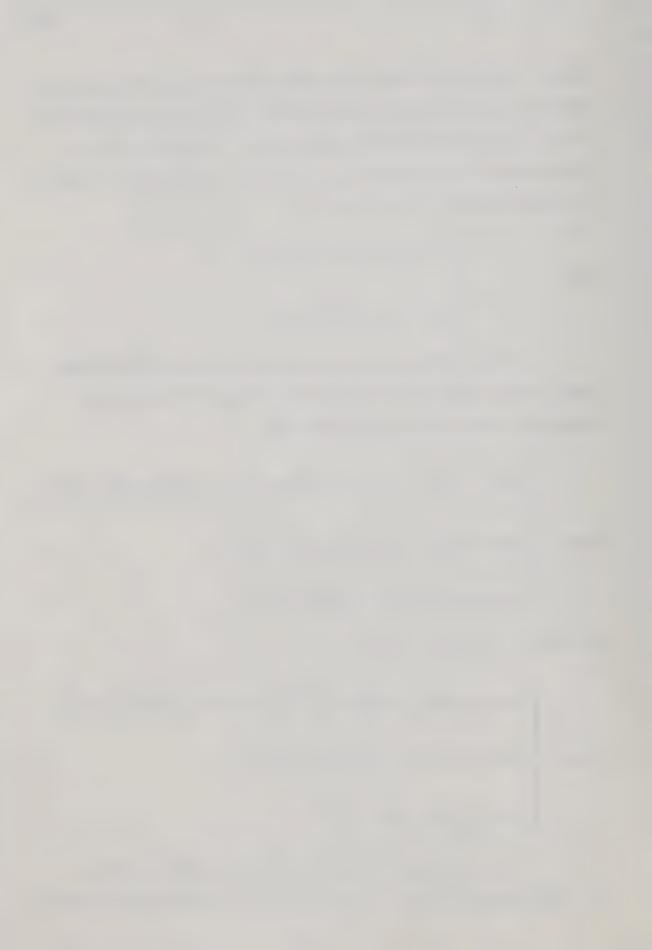
Tukey (1956) obtained the variance of the variance estimates under various ANOVA models by employing 'polykays'. For the model considered in this paper, he has shown that

(5.5)
$$\begin{cases} (a) & \text{Var } (\hat{\sigma}_{A}^{2}) = \frac{2}{I-1} \sigma_{A}^{4} + \frac{4}{J(I-1)} \sigma_{A}^{2} \sigma_{e}^{2} + \frac{2}{J(J-1)(I-1)} \sigma_{e}^{4} + \frac{\gamma_{A}}{I} \sigma_{A}^{4} ,\\ (b) & \text{Var } (\hat{\sigma}_{e}^{2}) = \frac{2}{(I-1)(J-1)} \sigma_{e}^{4} + \frac{\gamma_{e}}{IJ} \sigma_{e}^{4} ,\\ (c) & \text{Cov } (\hat{\sigma}_{A}^{2}, \hat{\sigma}_{e}^{2}) = \frac{-2}{(I-1)(J-1)J} \sigma_{e}^{4} . \end{cases}$$

From (5.5) it is easy to obtain

(5.6)
$$\begin{cases} (a) & \text{Var } (MS_A) = \left[\frac{2}{I-1} + \frac{1}{I} \left\{ \rho^2 \gamma_A + (1-\rho)^2 \gamma_e / J \right\} \right] (J \sigma_A^2 + \sigma_e^2)^2 \\ (b) & \text{Var } (MS_e) = \left[\frac{2}{(I-1)(J-1)} + \frac{\gamma_e}{IJ} \right] \sigma_e^4 \\ (c) & \text{Cov } (MS_A, MS_e) = \frac{\gamma_e}{IJ} \sigma_e^4 \end{cases}.$$

It is noted that if the true and error scores are normal, i.e., the kurtosis is equal to zero, the results are the same as expected



under normal theory obtainable from equation (2.15) and the resulting independence of ${\rm MS}_{\Delta}$ and ${\rm MS}_{\Delta}$.

Letting $x_1 = MS_A$, and $x_2 = MS_e$, and $W(x_1, x_2)$ a function of x_1 and x_2 , an approximation formula (e.g., Scheffé, 1959, p. 230) may be applied to approximate $Var(\beta)$ from (2.13)-(b) namely,

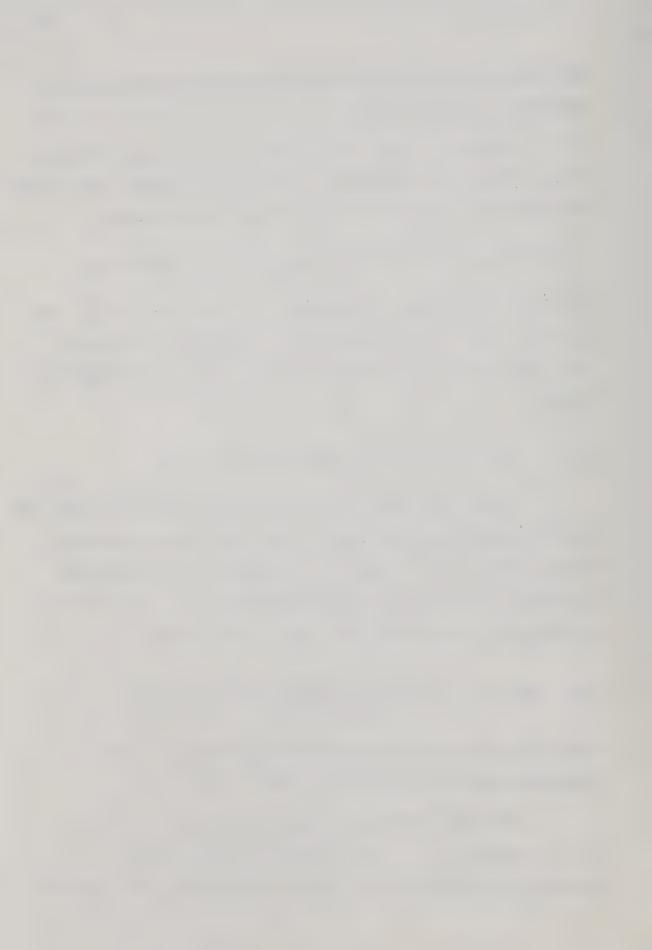
(5.7)
$$\text{Var } (\beta) \simeq (1-\rho)^2 \left[\frac{2J}{(1-1)(J-1)} + \frac{\rho^2}{I} (\gamma_A + \gamma_e/J) \right] .$$

Formula (5.7) does not agree exactly with formula (5.1)-(b) when the distributions are normal since an approximation has been employed. However, formula (5.7) is suggestive for correction terms to be added to formula (5.1)-(b) for non-normal distributions, i.e., $Var(\beta)$ may be obtained by a new formula combining (5.1) and (5.7) as

(5.8)
$$\operatorname{Var}(\hat{\rho}) \simeq (1-\rho)^2 \left[\frac{2(1-1)(1J-J-2)}{(J-1)(1-3)^2(1-5)} + \frac{\rho^2}{I} (\gamma_A + \gamma_e/J) \right].$$

Since this formula involves two unestimable parameters γ_A and γ_e , further approximation is necessary to make it useful.

The kurtosis of the test scores $y_i = \sum_j y_{ij} = J\mu + J a_i + \sum_j e_{ij}$, denoted by γ_y , is an estimable parameter, and may be evaluated by considering it as a linear combination of J+1 independent



random variables a_i and $\{e_{ij}\}$ for j = 1,...,J, and applying a formula given by Scheffé (1959, p. 332), namely,

(5.9)
$$\gamma_{y} = \rho^{2} \gamma_{A} + (1-\rho)^{2} \gamma_{e}/J$$

Then, $\gamma_y \simeq \rho^2 \gamma_A$ for $\rho \simeq 1$, or $\gamma_e \simeq 0$, or J fairly large. Therefore, it may be shown that,

(5.10) Var
$$(\beta) \simeq (1-p)^2 \left[\frac{2(1-1)(1J-J-2)}{(J-1)(1-3)^2(1-5)} + \frac{\gamma_y}{1} \right]$$
.

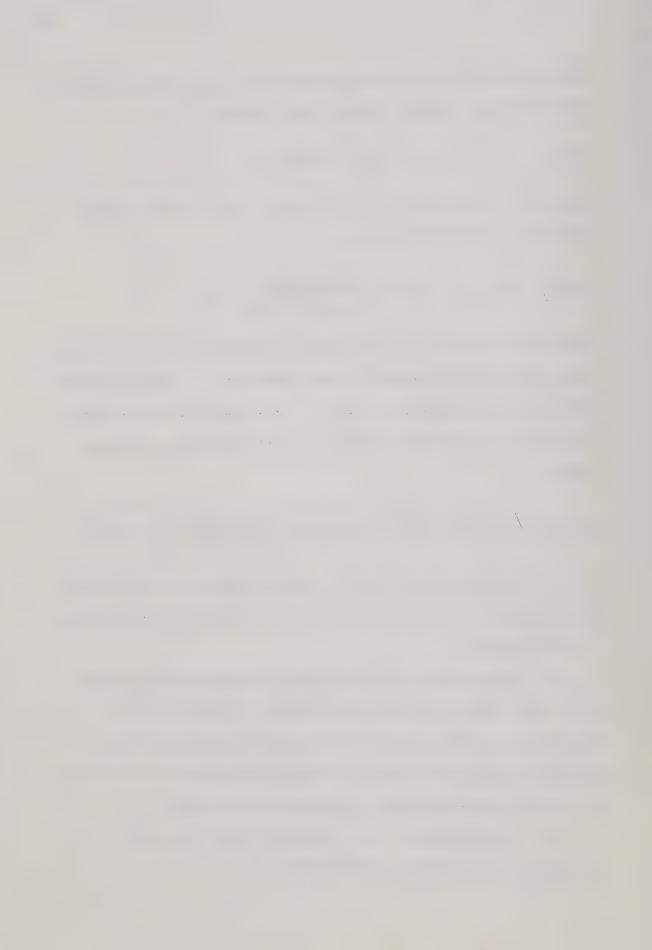
This formula (5.10) is, to the author's knowledge, a new one for test theory, which only includes the known constants. I,J and the unknown but estimable parameters ρ and γ_y . As a result it can be used to obtain an estimate of the standard error of reliability estimates, namely,

(5.11)
$$\widehat{S.E.}$$
 $\widehat{(\beta)} = [\widehat{Var} \widehat{(\beta)}]^{\frac{1}{2}} \simeq (1-\beta) \left[\frac{2(1-1)(1J-J-2)}{(J-1)(1-3)^2(1-5)} + \hat{\gamma}_y/1 \right]^{\frac{1}{2}}.$

From the formula (5.8) it may be observed that the effects of non-normality on the standard error of reliability estimates depend on the following:

- (a) The kurtosis of the true scores multiplied by the factor 1/I, and of the error scores multiplied by a factor of 1/IJ.

 Therefore, the effect of non-normality would be dominated by the kurtosis of true scores which is closely approximated by the kurtosis of the test scores divided by the square of the reliability.
- (b) The magnitude of $\,\rho\,,\,\,$ namely, the larger the value of $\,\rho\,,\,\,$ the greater is the effect of non-normality.



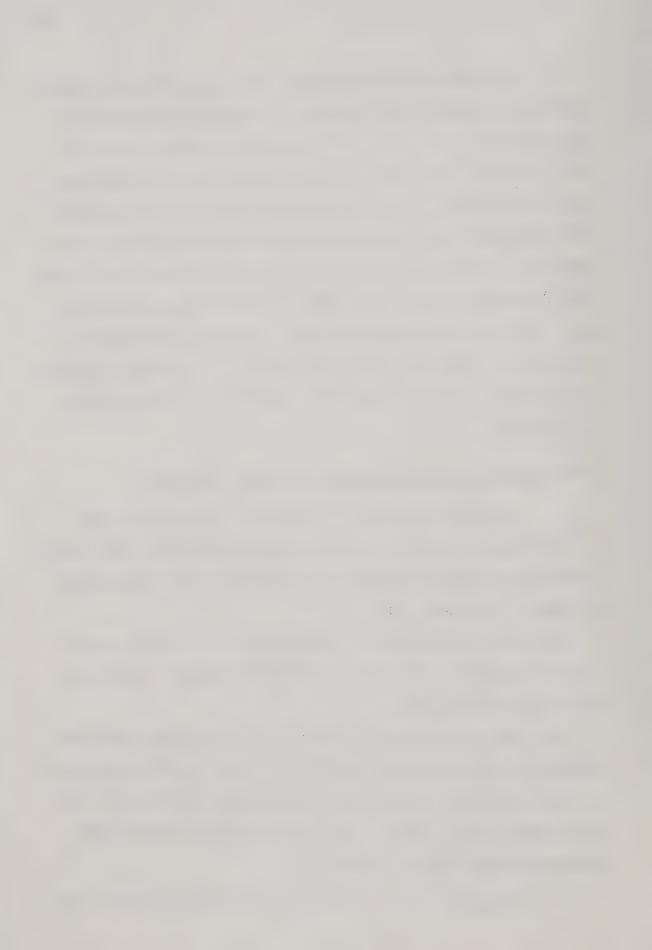
The above observations suggest that the sampling distribution would be robust against the violation of normality assumptions if (a) the sample size I is large, (b) reliability is close to zero, or (c) J is fairly large and the true score kurtosis (or the test score kurtosis) is close to zero. The condition (a) is of little practical value since statistical inference problems usually arise for the small sample case, while (b) is also of little practical value since, in most cases, reliability theory deals with ρ close to unity rather than zero. The last condition indicates that the sampling distribution of reliability estimates would be robust against the violation of normality of errors for J fairly large, and is sensitive to the distribution of true scores.

5.1.4 Results of Simulation Experiments Under ANOVA Model

In order to investigate the effect of non-normality under the ANOVA model, a number of experiments were performed by RELO1 using the following distribution-parameters combinations with the constants N = 2000, I = 30, and J = 8.

- (a) For the distribution of true scores, all of the six distributions discussed in Table 4.2 of Chapter Four, namely U1, U2, U3, U6, NO, and EX. were used.
- (b) For the error scores distributions, the uniform, normal, and exponential distributions were used, i.e., Ul, NO, and EX respectively.
- (c) Three levels of ρ were used by fixing $\sigma_e^2 = 4.0$, and using three levels of σ_A^2 , namely, 4.0, 1.0, and 0.36 to indicate high, middle and lower levels of reliability.

Altogether $6 \times 3 \times 3 = 54$ experiments were performed, each



requiring approximately six minutes of C.P.U. time. Since the parameters $\mu \quad \text{and} \quad \{\beta_{\frac{1}{2}}\} \quad \text{do not affect the distributions, they are not reported.}$

In Table 5.1, the observed means and variances of ${
m MS}_{
m A}$ and MS_{e} for N = 2000 samples are presented with the theoretical values based on formula (5.6). Because formula (5.6) does not involve any approximation, any disagreement between the observed and calculated values must be attributed to either sampling fluctuations due to the finiteness of N or deficiencies in random number generating methods. It is noted that a rather close agreement exists between the observed means of MS_{Δ} and MS_{ϵ} given in columns (1) and (3) with their theoretical expected values given in column (7). Comparisons of the observed variances of the MS's given in columns (2) and (4) with the theoretical values based on (5.6) given in columns (5) and (6)suggest that the two agree reasonably well, although the agreement is not as close as that for the means and expected values, which probably reflects the imperfectness of the random number generating procedures and/or the sensitivity of the variance to the change in the shape of population distributions.

Column (1) of Table 5.2 contains the mean of $\hat{\rho}$ over the N samples. These values can be compared with the expected values under normal distribution theory given in column (6). It is observed that, for negative γ_A , the means are in general higher than $E(\hat{\rho})$ based on formula (5.1)-(a), thus causing some moderating in the tendency to underestimate the reliability under normal thoery. If γ_A is positive, the mean of $\hat{\rho}$ is in general lower than $E(\hat{\rho})$ and exaggerates the tendency of underestimation. The effect of γ_e is

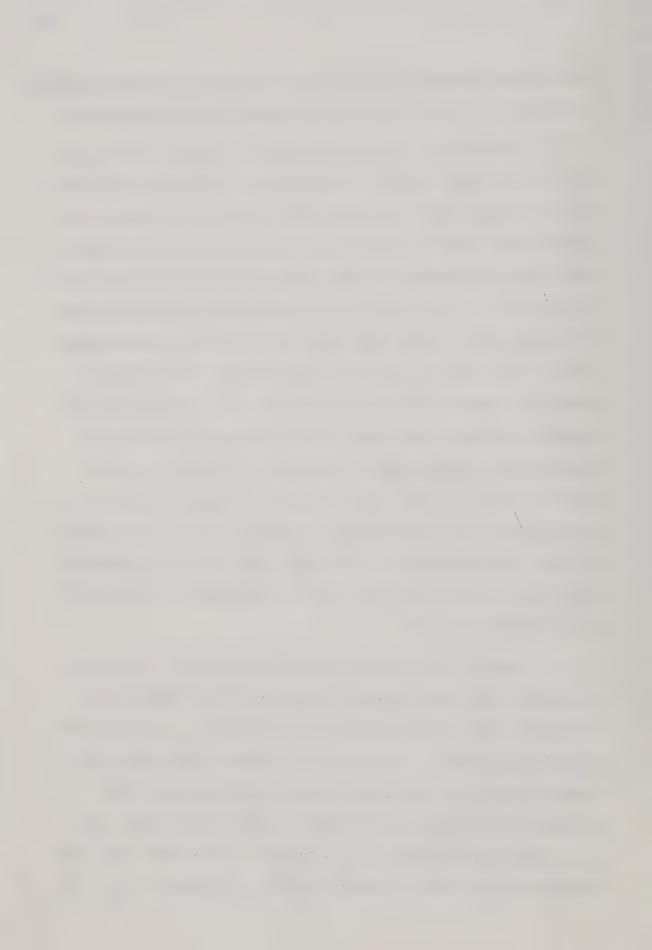


TABLE 5.1

Comparisons of Observed Means and Variances of MS's Under ANOVA Model and Various Combinations of True and Error Score Distributions With the Values Obtainable From Formula (5.6), $N=2000,\quad I=30,\quad J=8$

Ex.	Dis. Tr.	Ēr,	Observed MS _A		ed MS e Var.	Var. by	(5.6) MS	Parameters and E(MS)
			(1) (2)	(3)	(4)	(5)	(6)	(7)
01 02 03	U1 U1 U1	U I NO Ex		108 4.005 563 3.998 041 3.972	0.085 0.162 0.523	48.339 48.419 48.819	0.078 0.158 0.558	$\sigma_{A}^{2} = 4.0$
04 05 06	U2 U2 U2	U I NO EX	36.286 66. 36.283 69. 35.765 68.		0.081 0.165 0.572	68.819 68.899 69.299	0.078 0.158 0.558	$\sigma_{\rm e}^2 = 4.0$
07 08 09	U3 U3 U3	U I NO EX	36.106 74. 36.114 77. 36.033 76.	586 4.002	0.082 0.168 0.517	75.646 75.726 76.126	0.078 0.158 0.558	ρ = 0.8889
10 11 12	υ6 υ6 υ 6	U Ì NO EX	35.856 81. 36.107 84. 36.016 82.	019 4.006	0.081 0.171 0.559	82.473 82.553 82.953	0.078 0.158 0.558	E(MS _A) = 36.0
13 14 15	NO NO NO	U I NO EX	35.931 81. 36.016 85. 36.130 90.	815 3.998	0.084 0.162 0.523	89.299 89.379 89.779	0.078 0.158 0.558	E(MS _e) = 4.0
16 17 18	EX EX	U I NO EX	35.335 258. 35.358 270. 35.380 269.	874 3.998	0.085 0.162 0.523	294.099 294.179 294.579	0.078 0.158 0.558	
19 20 21	U1 U1 U1	U I NO EX	12.028 7.	3.994 147 3.992 657 3.981	0.084 0.168 0.557	7.291 7.371 7.771	0.078 0.158 0.558	$\sigma_{A}^{2} = 1.0$
22 23 24	U2 U2 U2	U1 NO EX	11.982 8.	902 3.999 550 3.991 953 4.021	0.082 0.164 0.568	8.571 8.651 9.051	0.078 0.158 0.558	$\sigma_{\rm e}^2 = 4.0$
25 26 27	U3 U3 U3	U I NO EX	11.945 9.	3.996 455 4.013 048 3.993	0.084 0.158 0.538	8.998 9.078 9.478	0.078 0.158 0.558	ρ = 0.6667
28 29 30	U6 U6 U6	U I NO EX	12.033 9.	794 4.000 430 3.993 972 3.979	0.084 0.165 0.536	9.424 9.504 9.904	0.078 0.158 0.558	E(MS _A) = 12.0
3 1 32 33	NO NO NO	U1 NO EX	12.029 9.	3.994 492 3.992 484 3.981	0.084 0.168 0.557	9.851 9.931 10.331	0.078 0.158 0.558	E(MS _e) = 4.0
34 35 36	EX EX	U1 NO EX	12.005 23. 11.883 22. 11.913 23.		0.085 0.168 0.557	22.651 22.731 23.131	0.078 0.158 0.558	
37 38 39	U1 U1 U1	U1 NO EX	6.869 2.	910 3.991 886 4.006 180 3.997	0.087 0.171 0.526	2.853 2.933 3.333	0.078 0.158 0.558	$\sigma_{A}^{2} = 0.36$
40 41 42	U2 U2 U2	U I NO EX	6.805 3.	026 3.997 162 3.987 376 4.002	0.084 0.160 0.536	3.019 3.099 3.499	0.078 0.158 0.558	$\sigma_e^2 = 4.0$
43 44 45	U3 U3 U3	U I NO EX	6.853 3.	3.980 111 3.989 522 3.982	0.087 0.162 0.550	3.074 3.154 3.554	0.078 0.158 0.558	p = 0.4186
46 47 48	U6 U6 U6	U I NO EX	6.907 3.	115 4.000 240 3.985 476 3.998	0.082 0.158 0.519	3.129 3.209 3.609	0.078 0.158 0.558	$E(MS_A) = 6.88$
49 50 51	NO NO NO	U I NO EX	6.883 3.	3.991 362 4.006 629 3.997	0.087 0.171 0.526	3.184 3.264 3.664	0.078 0.158 0.558	E(MS _e) = 4.0
52 53 54	EX EX	U1 NO EX	6.865 4.	3.991 627 4.006 995 3.997	0.087 0.171 0.526	4.843 4.923 5.323	0.078 0.158 0.558	

(a)
$$Var(MS_A) = \left[\frac{2}{1-1} + \frac{1}{1} \left\{\rho^2 \gamma_A + (1-\rho)^2 \gamma_e / J\right\}\right] \left(J\sigma_A^2 + \sigma_e^2\right)^2$$

(b) $Var(MS_e) = \left[\frac{2}{(1-1)(J-1)} + \frac{\gamma_e}{IJ}\right] \sigma_e^4$

(5.6) (b)
$$Var(MS_e) = {\frac{2}{(1-1)(J-1)}} + {\frac{\gamma_e}{IJ}}$$

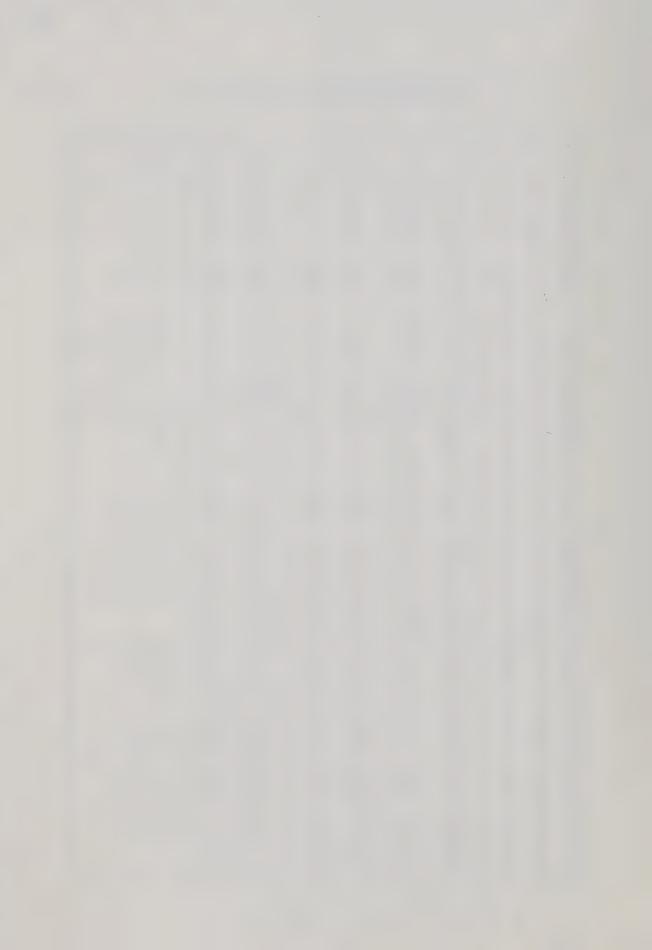


TABLE 5.2

Comparisons of Observed Means and Standard Errors of Reliability Estimates
Under ANOVA Model and Various Combinations of True and Error Score
Distributions With the Values Obtainable From Formulas (5.3),
(5.1)-(b), and (5.10), N = 2000, 1 = 30, J = 8

Ex.	Dis	Er.	Obser	ved ô	Calcu!	lated S.E. (6) by	Parameters and
No.	Tr.		Mean	S.E.	(5.3)	(5.1)-(b)	(5.10)	E(β) by (5.1)-(a)
			(1)	(2)	(3)	(4)	(5)	(6)
01	U1	UI	0.884	0.028	0.038	0.036	0.030	$\sigma_{A}^{2} = 4.0$
02	U1	NO	0.885	0.028	0.038	0.036	0.030	
03	U1	EX .	0.886	0.033	0.038	0.036	0.030	
04	U2	U1	0.884	0.031	0.038	0.036	0.033	$\sigma_{\rm e}^2$ = 4.0
05	U2	NO	0.833	0.032	0.038	0.036	0.033	
06	U2	EX	0.882	0.038	0.038	0.036	0.033	
07	U3	U1	0.882	0.033	0.038	0.036	0.034	ρ ≈ 0.8889
08	U3	NO	0.882	0.038	0.038	0.036	0.034	
09	U3	EX	0.883	0.038	0.038	0.036	0.034	
10	U6	U1	0.881	0.036	0.038	0.036	0.035	E(β) = 0.8807
11	U6	NO	0.881	0.035	0.038	0.036	0.035	
12	U6	EX	0.882	0.040	0.038	0.026	0.035	
13	NO	U1	0.881	0.035	0.038	0.036	0.036	
14	NO	NO	0.881	0.036	0.038	0.036	0.036	
15	NO	EX	0.882	0.040	0.038	0.036	0.036	
16 17 18	EX EX	U1 NO EX	0.864 0.864 0.865	0.062 0.061 0.064	0.038 0.038 0.038	0.036 0.036 0.036	0.057 0.057 0.057	
19	บ1	U I	0.646	0.090	0.101	0.108	0.098	$\sigma_{A}^{2} = 1.0$
20	บ1	NO	0.650	0.091	0.101	0.108	0.098	
21	บ1	EX	0.653	0.098	0.101	0.108	0.100	
22	U2	U1	0.644	0.103	0.101	0.108	0.103	$\sigma_{\rm e}^2 = 4.0$
23	U2	NO	0.646	0.100	0.101	0.108	0.103	
24	U2	EX	0.647	0.107	0.101	0.108	0.105	
25	U3	U1	0.642	0.101	0.101	0.108	0.104	ρ = 0.6667
26	U3	NO	0.640	0.108	0.101	0.108	0.105	
27	U3	EX	0.645	0.107	0.101	0.108	0.106	
28	U6	U1	0.643	0.106	0.101	0.108	0.106	E(s) = 0.6420
29	U6	NO	0.645	0.103	0.101	0.108	0.106	
30	U6	EX	0.645	0.111	0.101	0.108	0.108	
31	NO	U1	0.644	0.106	0.101	0.108	0.108	
32	NO	NO	0.645	0.105	0.101	0.108	0.108	
33	NO	EX	0.647	0.114	0.101	0.108	0.109	
34 35 36	EX EX	U I NO EX	0.615 0.612 0.617	0.154 0.156 0.158	0.101 0.101 0.101	0.108 0.108 0.108	0.146 0.147 0.148	
37	U1	U1	0.380	0.175	0.151	0.188	0.180	$\sigma_{A}^{2} = 0.36$
38	U1	NO	0.380	0.172	0.151	0.188	0.182	
39	U1	EX	0.384	0.179	0.151	0.188	0.189	
40	U2	U 1	0.380	0.181	0.151	0.188	0.183	$\sigma_{\rm e}^2 \approx 4.0$
41	U2	NO	0.369	0.195	0.151	0.188	0.185	
42	U2	EX	0.379	0.185	0.151	0.188	0.192	
43	U3	U I	0.381	0.189	0.151	0.188	0.184	ρ = 0.4186
44	U3	NO	0.376	0.186	0.151	0.188	0.186	
45	U3	EX	0.376	0.189	0.151	0.188	0.193	
46	U6	U I	0.382	0.181	0.151	0.188	0.185	E(8) = 0.3755
47	U6	NO	0.381	0.184	0.151	0.188	0.187	
48	U6	EX	0.375	0.187	0.151	0.188	0.194	
49 50 51	NO NO	U I NO EX	0.379 0.374 0.379	0.185 0.188 0.185	0.151 0.151 0.151	0.188 0.188 0.188	0.186 0.188 0.195	
52 53 54	EX EX	U1 NO EX	0.360 0.357 0.362	0.213 0.219 0.217	0.151 0.151 0.151	0.188 0.188 0.188	0.216 0.217 0.224	

(5.1)
$$\begin{cases} (a) & E(\beta) = 1 - (1-\rho) \frac{1-1}{1-3} \\ (b) & Var(\beta) = (1-\rho)^2 \frac{2(1-1)(y+1-3)}{(J-1)(1-3)^2(1-5)} \end{cases}$$

(5.3)
$$yar(\beta) = \frac{(1-\rho^2)^2}{1}$$

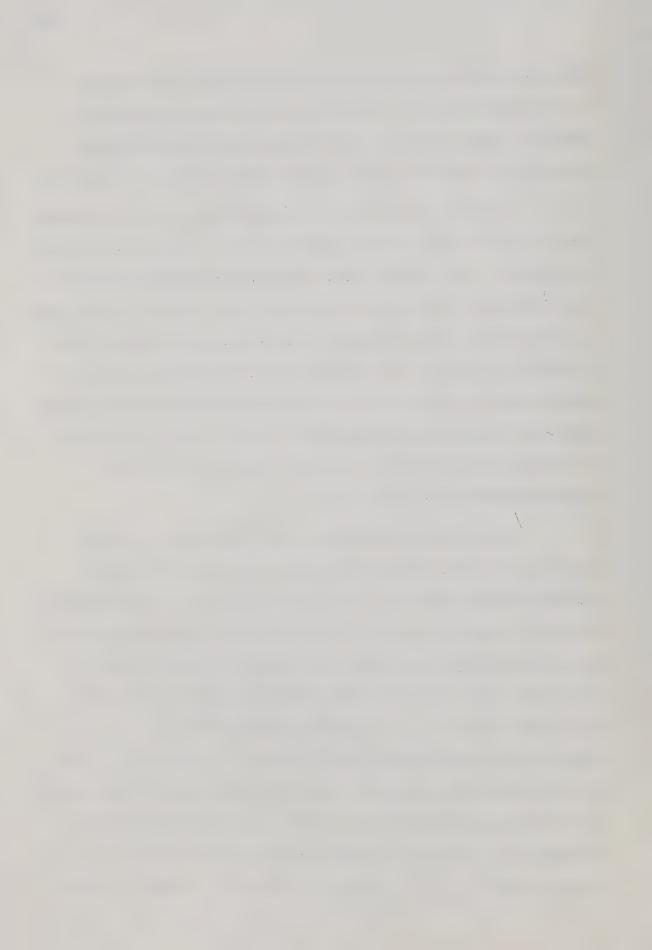
(5.10)
$$\operatorname{Var}(\beta) \simeq (1-\rho)^2 \left[\frac{2(1-1)(1J-J-2)}{(J-1)(1-3)^2(1-5)} + \frac{\gamma_y}{i} \right]$$



almost negligible, as expected from the discussion of the standard errors in Section 5.1.3. Therefore, as far as point estimation is concerned, negative kurtosis would not cause any serious problems, but positive kurtosis may cause serious underestimation of reliability.

Table 5.2 also contains the standard errors of β in columns (3), (4), and (5) under various formulas as well as the observed results in column (2). The results clearly indicate the inappropriateness of the tranditional formula (5.3) or the more recent formula (5.1)-(b) when γ_A is non-zero, and demonstrates the effectiveness of formula (5.10). To see how closely the values based on these formulas approximate the observed values, the sum of squares of the deviation from the observed values are calculated with the results 0.0416, 0.0133, and 0.0013 for formulas (5.3), (5.1)-(b) and (5.10) respectively, with the minimum deviations for formula (5.10).

To examine the robustness of the F-test based on formula (2.17), under normal distribution theory, the shapes of the upper and lower 5% tail portions of the distributions of β were investigated. Columns (1) and (2) of Table 5.3 show approximate real Type one errors when nominal significance levels are fixed at 5% level for each tail. The results clearly indicate that real Type one errors are less than the nominal value if γ_A is negative, and the smaller is γ_A , the smaller is the resulting real Type one error. For positive γ_A , the real Type one errors are greater than the nominal value. These results are in close agreement with the Scheffé's conclusion referred to in Section 5.1.2. It is also noticed that the effect of non-zero γ_A is less for small ρ , i.e., the test is robust if ρ tends to zero as



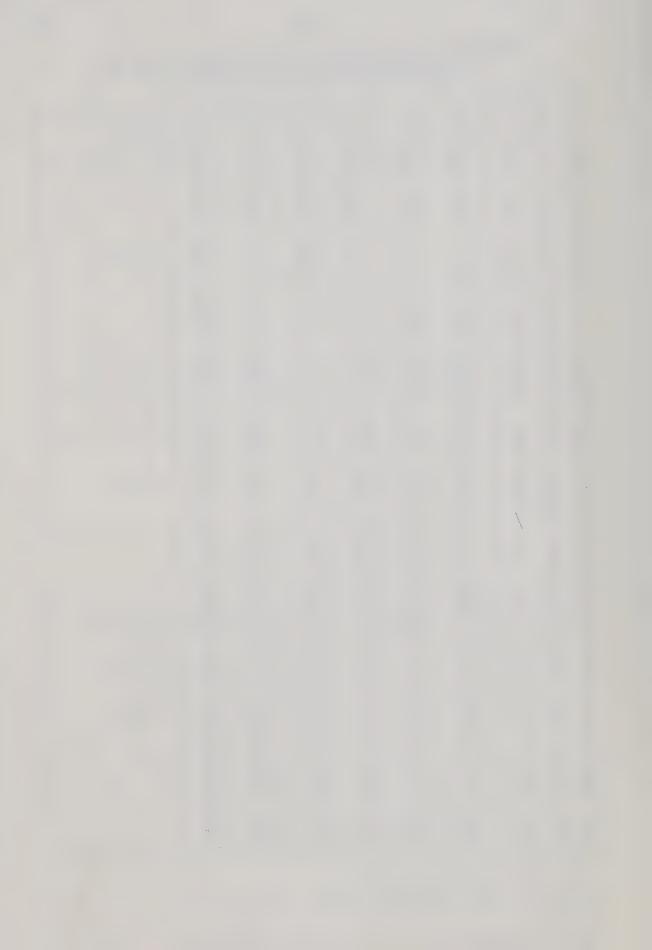
Comparisons of Observed Lower and Upper 5% Critical Points of Reliability Estimates Under the ANOVA Model Using Various Comminations of True and Error Score Distributions, and Real Type One Errors of F-lest When Nominal Value is 5% With the Values Obtainable Under the Normal Theory, N = 2000, I = 30, J = 8

Ex. Dis.			Real Si	g. (%)	Observe	ed C.P.	Theoret	ical C.P. ²	2
No.	Tr.	Er.	Lower	Upper	Lower	Upper	Lower	Upper	Parameters ³
			(1)	(2)	(3)	(4)	(5)	(6)	(7)
01	U1 U1	UI NO	1.80	1.65	0.837	0.919 0.920	0.814	0.927 0.927	$\sigma_{A}^{2} = 4.0$
03	U1 U2 U2	U1 NO	2.25 2.75 3.05	5.05 2.45 3.45	0.829 0.827 0.827	0.927 0.922 0.924	0.814 0.814 0.814	0.927 0.927 0.927	$\sigma_0^2 = 4.0$
)6)7	U2 U3	EX U1	4.85	3.05	0.815	0.929	0.814	0.927	e 4.0
18	U3 U3	NO EX	4.15 5.00	4.40 7.25	0.821	0.926 0.930	0.814	0.927	ρ = 0.8889
10	U6 U6 U6	U1 NO EX	4.30 4.65 5.60	3.60 4.70 7.20	0.816 0.816 0.812	0.924 0.926 0.930	0.814 0.814 0.814	0.927 0.927 0.927	
13 14 15	NO NO NO	U1 NO EX	4.70 4.25 5.30	3.90 4.85 8.30	0.816 0.819 0.811	0.925 0.926 0.932	0.814 0.814 0.814	0.927 0.927 0.927	
16 17 18	EX EX	U1 NO EX	17.40 17.35 17.95	10.50 11.15 12.90	0.747 0.744 0.752	0.940 0.942 0.944	0.814 0.814 0.814	0.927 0.927 0.927	
19 20 21	U1 U1 U1	U1 NO EX	3.35 3.00 3.50	3.00 3.45 5.40	0.474 0.483 0.471	0.769 0.772 0.783	0.442 0.442 0.442	0.781 0.781 0.781	σ _A = 1.0
22 23 24	U2 U2 U2	U1 NO EX	4.55 3.95 4.65	3.85 4.00 6.20	0.450 0.470 0.448	0.775 0.776 0.788	0.442 0.442 0.442	0.781 0.781 0.781	$\sigma_e^2 = 4.0$
25 26 27	U3 U3 U3	U1 NO EX	4.15 5.05 4.80	3.85 4.45 5.45	0.453 0.441 0.448	0.774 0.778 0.785	0.442 0.442 0.442	0.781 0.781 0.781	ρ = 0.6667
28 29 30	υ6 υ6 υ6	U1 NO EX	4.45 4.75 5 .35	4.45 4.30 6.65	0.446 0.445 0.440	0.777 0.778 0.788	0.442 0.442 0.442	0.781 0.781 0.781	
31 32 33	NO NO	U1 NO EX	4.55 4.55 5.95	4.80 5.05 7.25	0.448 0.449 0.427	0.780 0.782 0.792	0.442 0.442 0.442	0.781 0.781 0.781	
34 35 36	EX EX	U1 NO EX	11.55 11.95 12.80	10.55 11.45 12.10	0.327 0.331 0.321	0.814 0.813 0.822	0.442 0.442 0.442	0.781 0.781 0.781	
37 38 39	U1 U1 U1	U1 NO EX	3.80 3.75 4.65	5.05 4.50 4.75	0.056 0.070 0.040	0.619 0.612 0.616	0.027 0.027 0.027	0.618 0.618 0.618	$\sigma_{A}^{2} = 0.36$
40 41 42	U2 U2 U2	U1 NO EX	4.65 5.50 5.10	5.25 4.65 5.35	0.034 0.070 0.025	0.622 0.615 0.623	0.027 0.027 0.027	0.618 0.618 0.618	$\sigma_{\rm e}^2 = 4.0$
43 44 45	U3 U3 U3	U1 NO EX	5.05 5.05 4.85	5.65 4.55 5.55	0.026 0.026 0.033	0.626 0.615 0.618	0.027 0.027 0.027	0.618 0.618 0.618	ρ = 0.4186
46 47 48	U6 U6 U6	U1 NO EX	4.30 4.55 4.55	4.85 4.85 4.65	0.053 0.041 0.043	0.615 0.617 0.614	0.027 0.027 0.027	0.618 0.618 0.618	
49 50	NO NO NC	U1 NO EX	4.60 5.10 4.70	4.60 4.55 4.85	0.033 0.023 0.029	0.616 0.615 0.618	0.027 0.027 0.027	0.618 0.618	
52 53 54	EX EX	U1 NO EX	7.30 8.25 7.35	7.05 7.10 8.65	-0.026 -0.0/19 -0.049	0.637 0.644 0.645	0.027 0.027 0.027	0.618 0.618 0.618	

 $^{^{1}}$ Observed lower and upper 5% critical points of $\,$ $\,$ $\,$ $\,$ $\,$

 $^{^2}$ Theoretical lower and upper 5% critical points of β with normal distribution of true and error scores.

 $^{^3}$ Kurtosis of the random variables U1, U2, U3, U6, N0, and EX are given in Table 4.3.



anticipated by the earlier discussion of the standard errors of estimation in Section 5.1.3.

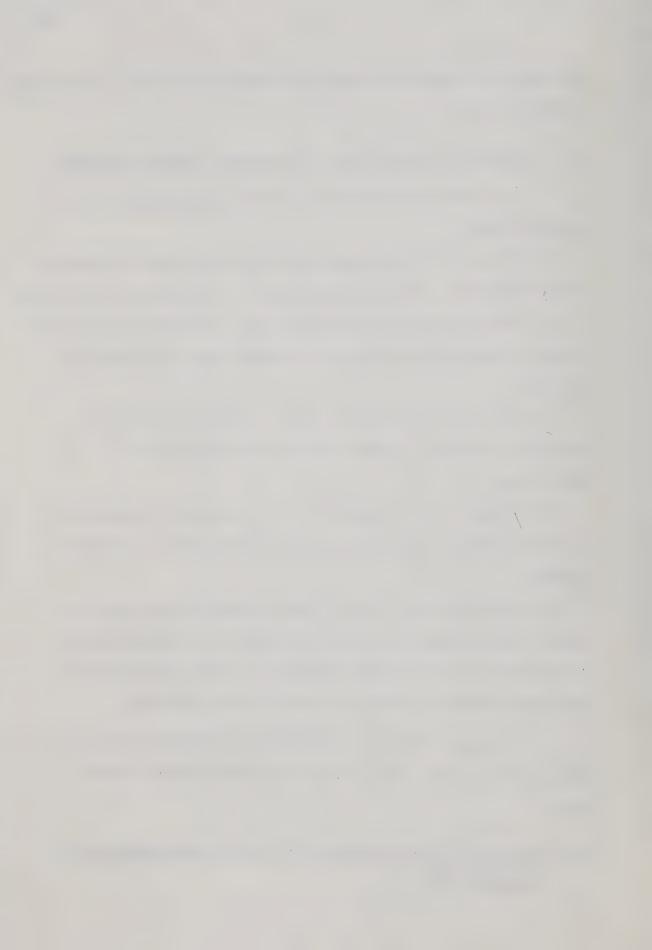
5.1.5 Conclusions on the Effects of Non-Normality Under ANOVA Model

From the above discussions the following conclusions are tentatively made:

- (a) The effect of non-normality of the error score distribution is negligible for J fairly large, where J is the number of part-tests.
- (b) Non-zero kurtosis of the true score distribution substantially effects the sampling distribution and standard error of reliability estimates.
- (c) The F-test under normal theory is robust for near zero population reliability, or near zero true score kurtosis, if J is fairly large.
- (d) Formula (5.10) is superior to the traditional formula (5.3) or (5.1)-(b) for the calculation of the standard error of reliability estimates.
- (e) For the F-test, the real Type one error is lower than the nominal value for negative kurtosis, and higher for positive kurtosis of true scores. This true score kurtosis is closely approximated by test score kurtosis divided by the square of the reliability.

The above findings are restricted to the ANOVA model, and generalization to more liberal test score models requires further study.

5.2.0 Relaxation of the Homogeneity of Error Variance Constraint in the ANOVA Model



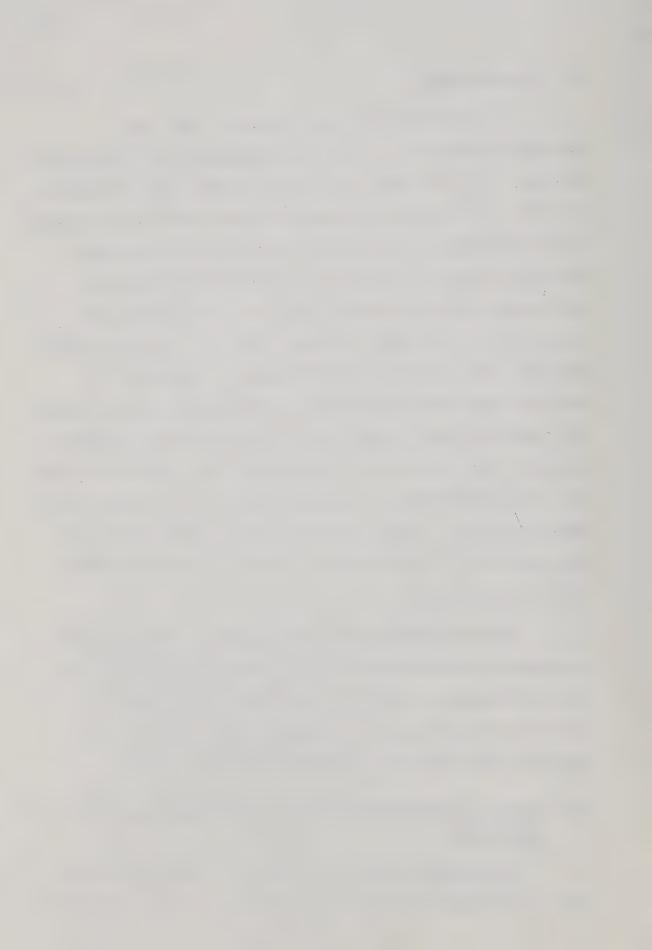
5.2.1 The ETEM Model

For the ANOVA model it was assumed variances of error scores {e; } were homogeneous, i.e., all the error variances $\{\sigma_{e}^2\}$ are equal to an unknown constant σ_{e}^2 by assumption (2.7)-(d). This assumption was made not because real data are expected to have homogeneous error variances, but to make the mathematical abstraction simpler. Therefore it is conceivable that the error variances may differ for each part test, i.e., for real data the variance of e; may depend on the part test j, as given by (2.19). Under this last assumption, the model becomes an essentially τ equivalent measurement (ETEM) which was discussed more fully in Chapter Under this model, there is not a common intra-class correlation among the J part-scores to be interpreted as the reliability of a parttest under the ANOVA model. But the reliability is still equal to the Alpha coefficient. The only difference from the ANOVA model is the replacement of σ_e^2 in the reliability formula (2.12) by the mean of $\{\sigma_{e_i}^2\}$, denoted by $\sigma_{e_i}^2$.

Because assumption (2.7)-(d) is violated, the distribution of reliability estimates given by (2.17) cannot be expected to hold for the ETEM models; at best it is hoped that the distribution is closely approximated or the distribution is robust against the violation of the assumption of homogeneity of error variances.

5.2.2 Effects of Non-Homogeneous Error Variances Assuming Normal Distribution

The general distributional theory of reliability estimates under the ETEM model with the normal assumption is not yet known except



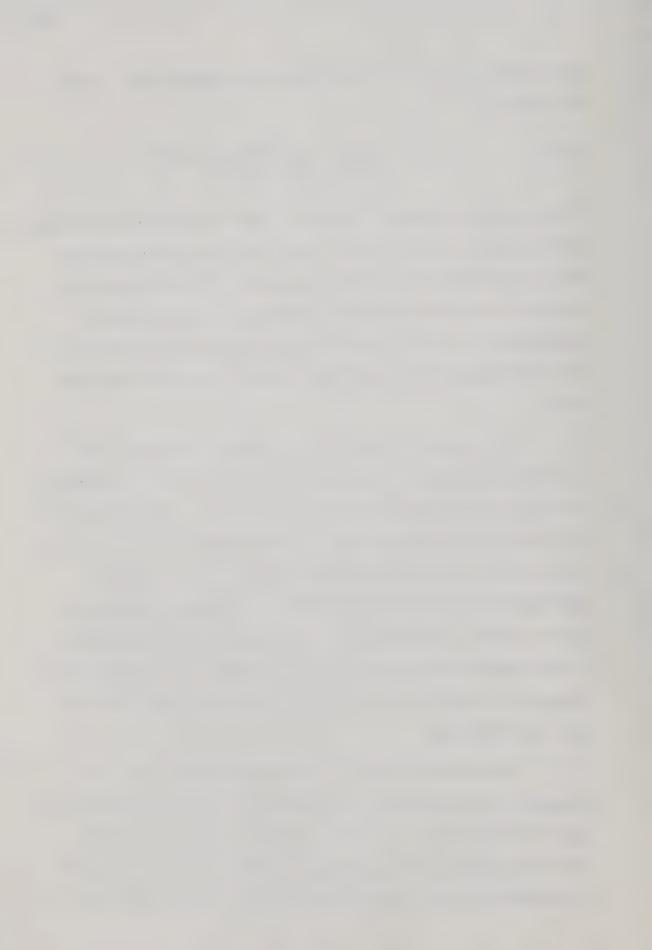
for the case of J=2. Kristof (1970) has shown that, for J=2, the statistic

(5.12)
$$t = \frac{\rho - \beta}{\beta (1-\rho)^{\frac{1}{2}}} \frac{s_{12}}{(s_1^2 s_2^2 - s_{12}^2)^{\frac{1}{2}}} (1-2)^{\frac{1}{2}}$$

is distributed as Student's t-statistic with I-2 degrees of freedom, where s_1^2 , s_2^2 , and s_{12} are the sample variances of two part-tests and the covariance between them respectively. Kristof derived this formula by the maximum likelihood method under bivariate normal assumptions for the alpha coefficient, but the formula can also be used interchangeably for the reliability coefficient under the ETEM model.

For the general case, J > 2, nothing is known yet, and at present the simulation method provides the only way to investigate the sampling distribution of reliability estimates. Because equation (2.17) does not involve the error variance parameter directly, it may be hoped that the distribution given by (2.17) is still valid or approximately true under the ETEM model if the normality assumptions are not violated. In other words, it is hoped that the distribution is robust against the violation of the homogeneity of error variances assumption to enable the test theorists to use the results obtained under the ANOVA model.

To separate the effect of non-normality from that of non-homogeneous error variances, the ETEM model is first investigated using normal distributions of true and error scores. In order to make comparisons possible, the constants and parameters used for the cases of the ANOVA model are retained except for the values of the error



variances. With 3 levels of σ_A^2 , as under the ANOVA model, 6 different sets of non-homogeneous error variances are used for the simulation experiments. The sets of error variances are given in the following table including the homogeneous case (EVI) used under the ANOVA model as a special case.

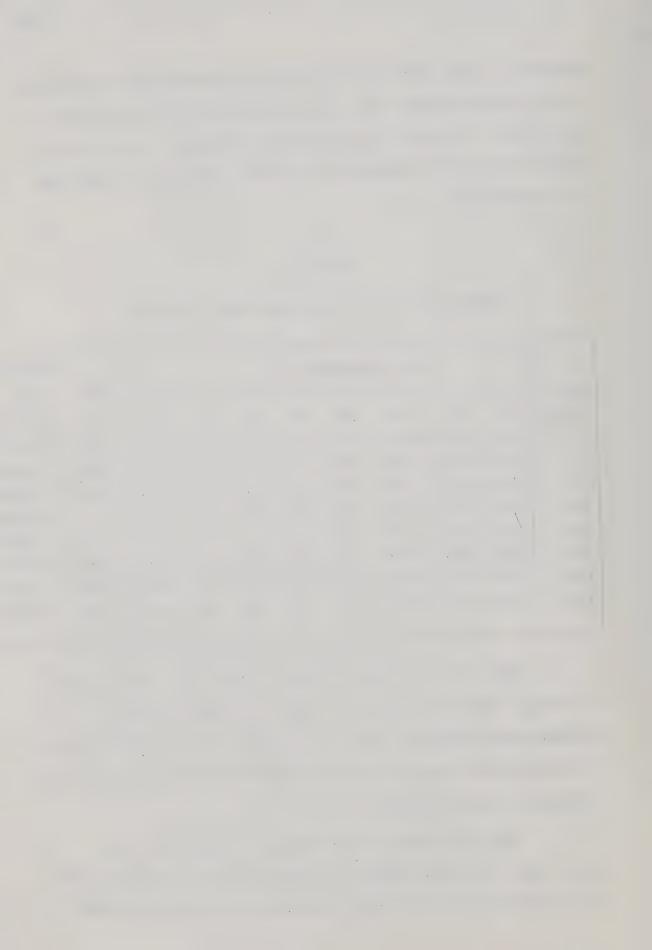
TABLE 5.4

Summary of Error Variances used Under ETEM Model

		Variance Mean (5, 2								
Nota- tion	j=1	j=2	j=3	j=4	j=5	j=6	j=7	j=8	σe.	$(\sum (\sigma_{ej}^2 - \sigma_{e}^2)^2)/J$
EV1	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.00	4.0000	0.0000
EV2	1.46	2.56	3.24	4.00	4.00	4.84	5.76	6.15	4.0018	2.1887
EV3	1.00	1.00	4.00	9.00	9.00	4.00	1.00	1.00	3.7500	10.6875
EV4	9.00	4.00	1.00	0.25	0.25	1.00	4.00	9.00	3.5625	11.8242
EV5	16.00	9.00	4.00	1.00	1.00	1.00	1.00	1.00	4.2500	26.6875
EV6	1.00	4.00	16.00	16.00	9.00	4.00	1.00	0.00	6.3750	37.7344
EV7	1.00	1.00	16.00	16.00	1.00	1.00	1.00	1.00	4.7500	42.1875

The last two columns of Table 5.4 give $\sigma_{e.}^2$, which is equal to $E(MS_e)$, and the variance of $\{\sigma_{ej}^2\}$ within each set over J=8. To make comparisons easy, these sets are ordered with increasing degree of non-homogeneity, measured by the variance within each set, which has a range of 0.0 to 42.1875.

Table 5.5 summarizes the mean and variance MS and MS , for N = 2000 samples in columns (1) to (4) inclusive, and compares the results with those obtainable from formula (5.6) with σ_e^2



Comparisons of Observed Means and Variances of MS's Under the ETEM Model and Normal Distributions With the Values Obtainable From Formula (5.6), N = 2000, 1 = 30, J = 8

TABLE 5.5

Ex. No.	Error Set	Obser Mean (1)	ved MS _A Var. (2)	Observe Mean (3)	ed MS _e Var. (4)	E (MS _A)	Var. by MSA (6)	(5.6) MS _e (7)	Parameters (8)
01	EV 1	36.016	85.815	3.998	0.162	36.000	89.379	0.158	$\sigma_{A}^{2} = 4.0$
02	EV 2	36.041	85.556	4.000	0.184	36.002	89.388	0.158	
03	EV 3	35.727	88.222	3.742	0.226	35.750	88.142	0.139	
04	EV 4	35.879	98.868	3.543	0.242	35.562	87.220	0.125	
05	EV 5	36.266	86.094	4.244	0.387	36.250	90.625	0.178	
06	EV 6	38.049	101.514	6.378	0.742	38.375	101.561	0.400	
07	EV 7	36.784	94.840	4.705	0.551	36.750	93.142	0.222	
08	EV1	12.029	9.492	3.992	0.168	12.000	9.931	0.158	$\sigma_A^2 = 1.0$
09	EV2	12.034	9.581	3.995	0.189	12.002	9.934	0.158	
10	EV3	11.898	9.537	3.740	0.236	11.750	9.522	0.139	
11	EV4	11.495	9.317	3.549	0.220	11.562	9.220	0.125	
12	EV5	12.278	10.465	4.236	0.407	12.250	10.349	0.178	
13	EV6	14.563	14.483	6.366	0.753	14.375	14.251	0.400	
14	EV7	12.838	11.499	4.780	0.603	12.750	11.211	0.222	
15	EV1	6.883	3.362	4.006	0.171	6.880	3.264	0.158	$\sigma_{A}^{2} = 0.36$
16	EV2	6.891	3.411	4.008	0.189	6.882	3.266	0.158	
17	EV3	6.700	3.203	3.762	0.221	6.630	3.032	0.139	
18	EV4	6.430	2.779	3.559	0.230	6.442	2.862	0.125	
19	EV5	7.120	3.491	4.252	0.429	7.130	3.506	0.178	
20	EV6	9.341	6.174	6.403	0.704	9.255	5.907	0.400	
21	EV7	7.629	4.035	4.750	0.619	7.630	4.015	0.222	

$$E(MS_e) = \sigma_e^2 = 4.000 (EV1)$$

 $4.002 (EV2)$
 $3.750 (EV3)$
 $3.563 (EV4)$
 $4.250 (EV5)$
 $6.375 (EV6)$
 $4.750 (EV7)$

(5.6)
$$\begin{cases} (a) & \text{Var } (MS_A) = \left[\frac{2}{I-1} + \frac{1}{I} \left\{\rho^2 \gamma_A + (1-\rho)^2 \gamma_e / J\right\}\right] (J\sigma_A^2 + \sigma_e^2)^2 \\ (b) & \text{Var } (MS_e) = \left[\frac{2}{(I-1)(J-1)} + \frac{\gamma_e}{IJ}\right] \sigma_e^4 \end{cases}$$



replaced by σ_e^2 , and $\gamma_A = \gamma_e = 0$ in columns (6) and (7). Close agreement between expected MS's and the mean of observed MS's is seen as was the case for the ANOVA model. More specifically, the expected and observed variance of MS_A, columns (2) and (6), agree closely, but the observed variance of MS_e, column (4), differs greatly from the theoretical value obtainable from (5.6) given in column (7). The greater the non-homogeneity of error variances, the greater the discrepancy noted, reaching in the extreme a factor of three for experiment 21. Therefore, it may be concluded that the formula (5.6) cannot be applied blindly in the case of the ETEM model, due to the possible effect of non-homogeneity of error variances.

Table 5.6 summarizes the observed mean and standard error for each experiment in columns (3) and (4) and compares it with the values obtainable from (5.1), (5.3), and (5.10) given in columns (2), (5), and (6). It is observed that a rather close agreement exists between the observed mean of $\hat{\rho}$ and $E(\hat{\rho})$ obtainable from (5.1)-(a) under the ANOVA model, i.e., columns (2) and (3), indicating robustness of the ETEM model as far as point estimation and biasedness are concerned. For the standard error of estimation, all two formulas predict the observed values reasonably well. Formula (5.10) seems better than (5.3), though the difference is not great. The calculated sum of squares of the deviation from the observed values are 0.00858 and 0.00097 for formulas (5.3) and (5.10) respectively, confirming the conclusion. All of these results suggest that the standard error of reliability estimate is robust against the violation of homogeneity of error variances.

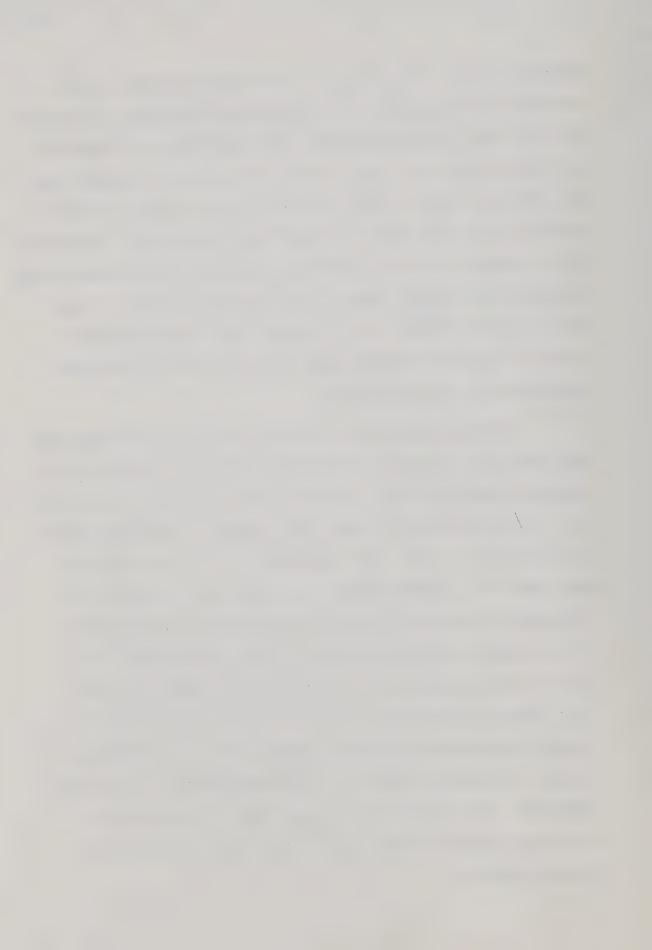


TABLE 5.6

Comparisons of Observed Means and Standard Errors of Reliability Estimates Under ETEM Model and Normal Distributions With the Values Obtainable From Formula (5.3), and (5.10), N = 2000, I = 30, J = 8

No.	Error Set	Rel.	E(ô) by (5.1)-(a)	Observ Mean	/ed β S.E.	S.E. b (5.3)	y formulas (5.10)	Parameters
		(1)	(2)	(3)	(4)	(5)	(6)	(7)
01 02 03 04 05 06	EV1 EV2 EV3 EV4 EV5	0.889 0.889 0.895 0.899 0.883 0.834	0.881 0.881 0.887 0.892 0.874 0.822	0.881 0.881 0.887 0.893 0.875 0.820	0.036 0.036 0.036 0.035 0.039	0.038 0.038 0.036 0.035 0.040 0.056	0.036 0.036 0.034 0.032 0.038 0.054	σ _A = 4.0
07 08 09	EV7 EV1 EV2	0.871 0.667 0.667	0.861 0.642 0.642	0.863 0.645 0.644	0.044 0.105 0.106	0.044	0.042 0.108 0.108	$\sigma_{A}^{2} = 1.0$
10 11 12 13	EV3 EV4 EV5 EV6	0.681 0.692 0.653 0.557	0.657 0.669 0.627 0.524	0.664 0.669 0.631 0.533	0.099 0.102 0.114 0.127	0.098 0.095 0.105 0.126	0.103 0.110 0.112 0.143	A .
14	EV7	0.628	0.600	0.603	0.119	0.111	0.121	2 000
16 17 18 19 20 21	EV2 EV3 EV4 EV5 EV6 EV7	0.419 0.434 0.447 0.404 0.311 0.378	0.375 0.393 0.406 0.360 0.260 0.331	0.375 0.398 0.410 0.365 0.267 0.338	0.187 0.180 0.173 0.184 0.201 0.197	0.151 0.148 0.146 0.153 0.165 0.157	0.188 0.183 0.179 0.193 0.223 0.201	$\sigma_{A}^{2} = 0.36$

(5.1)-(a)
$$E(\beta) = 1 - (1-\rho) \frac{1-1}{1-3}$$

(5.3)
$$\operatorname{Var}(\beta) = \frac{(1-\rho^2)^2}{1}$$

(5.10)
$$\text{Var } (\beta) \simeq (1-\rho)^2 \left[\frac{2(1-1)(1J-J-2)}{(J-1)(1-3)^2(1-5)} + \frac{\gamma_y}{I} \right] .$$

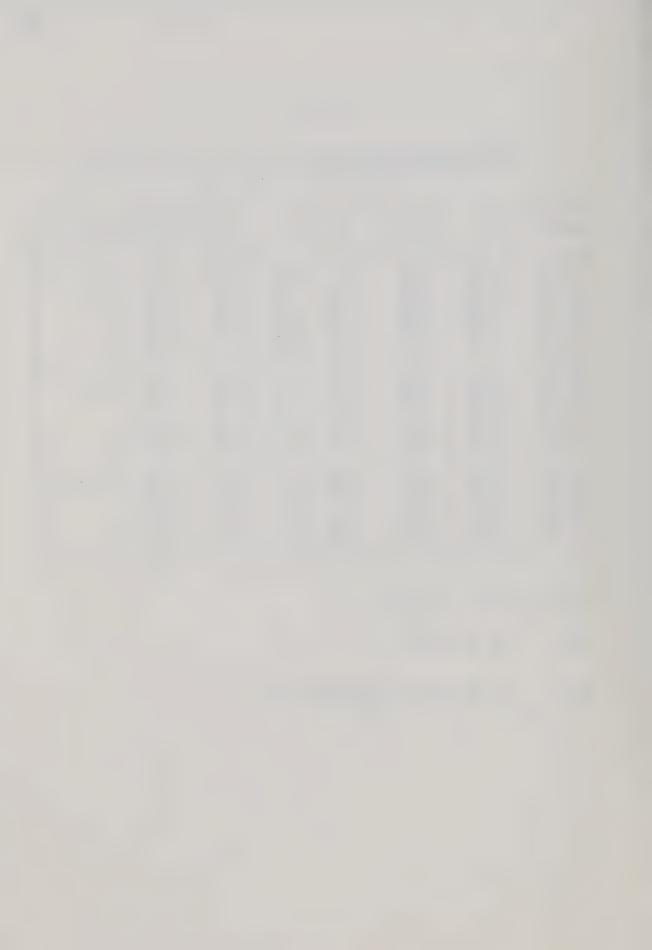


Table 5.7 summarizes the lower and upper 5% portions of the observed distribution of $\hat{\rho}$ in columns (2) and (3) and compares them with the values obtainable under the ANOVA model and normal theory given in columns (4) and (5), namely from formula (2.17). The table also gives approximate real Type one error in columns (6) and (7) when the F-test of (2.17) is used for the ETEM model with normal distributions. The results clearly indicate the robustness of the F-test against the violation of homogeneity of error variance assumptions. Although there is a case (experiment 4) which gives as much as an 8% level of Type one error, there seems to be no systematic inflation or deflation of the nominal Type one error as a whole.

5.2.3 Effects of Non-Normality on ETEM Model

In the previous section, it was seen that the effect of non-homogeneous error variances on sampling distribution of reliability estimates is minimal, and it was also seen in Section 5.1 that the sampling distribution is sensitive only to the violation of the assumption of the normality of true scores and is robust against distributional assumption of error scores. Therefore, it is logical to expect that the distribution is not robust against the distributional assumption of true scores, but the effect of non-normality of error scores must still be investigated under the ETEM model, since there is a possibility of interaction between the non-normal error score distribution and non-homogeneous error variances.

To investigate this interaction effect, further experiments were carried out using the EV2 error variances set, chosen because its $\sigma_e^2 = 4.0018$ is closest to $\sigma_e^2 = 4.0$ used for the ANOVA model

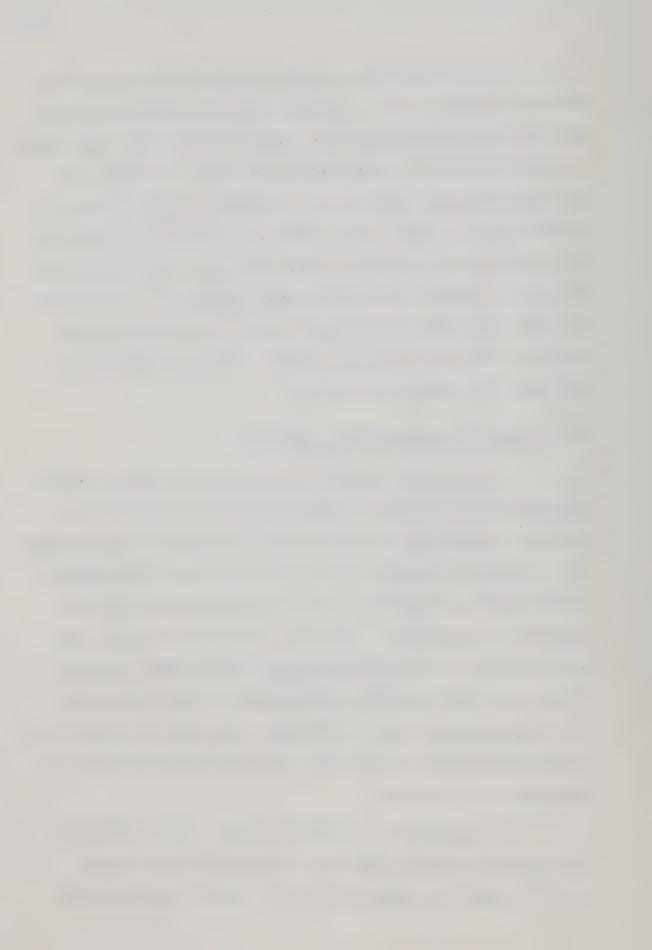


TABLE 5.7

Comparisons of Observed Lower and Upper 5% Critical Points and Real Type One Errors of F-Test When Nominal Value is Fixed at 5%, Under ETEM Model and Normal Distributions With the Values Obtainable Under ANOVA Model, $N=2000,\quad I=30,\quad J=8$

	Error		0bserve	d C.P.	Theoret	ical C.P. ²	Real Si	g. (%)	Parameters
No.	Set	Rel.	Lower	Upper	Lower	Upper	Lower	Upper	
		(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
01 02 03 04 05 06	EV1 EV2 EV3 EV4 EV5 EV6	0.889 0.889 0.895 0.900 0.883 0.834 0.871	0.819 0.818 0.821 0.831 0.802 0.719 0.787	0.926 0.927 0.932 0.940 0.925 0.892 0. 920	0.814 0.814 0.824 0.832 0.804 0.722 0.784	0.927 0.927 0.931 0.934 0.923 0.891 0.915	4.25 4.10 5.55 5.25 5.20 5.30 4.65	4.85 4.90 6.05 8.05 6.00 5.65 7.15	$\sigma_A^2 = 4.0$
08 09 10 11 12 13	EV1 EV2 EV3 EV4 EV5 EV6	0.667 0.667 0.681 0.692 0.653 0.557 0.628	0.449 0.442 0.479 0.475 0.414 0.292 0.385	0.782 0.784 0.793 0.801 0.778 0.712	0.442 0.442 0.466 0.484 0.419 0.258 0.376	0.781 0.782 0.791 0.798 0.772 0.709 0.755	4.55 5.00 3.85 5.45 5.20 3.80 4.50	5.05 5.20 5.45 6.10 6.25 5.25 5.40	σ <mark>2</mark> = 1.0
15 16 17 18 19 20 21	EV1 EV2 EV3 EV4 EV5 EV6 EV7	0.419 0.419 0.434 0.447 0.404 0.311 0.378	0.023 0.018 0.057 0.095 0.020 -0.135 -0.031	0.616 0.617 0.633 0.627 0.604 0.549 0.582	0.027 0.026 0.053 0.074 0.002 -0.153 -0.042	0.618 0.618 0.629 0.637 0.609 0.543 0.591	5.10 5.15 4.80 4.55 4.25 4.35 4.60	4.55 4.70 5.45 4.05 4.45 5.05 4.10	$\sigma_{A}^{2} = 0.36$

¹ Observed lower and upper 5% critical points of \$.

 $^{^2}$ Theoretical lower and upper 5% critical points of $\,$ $\,$ $\,$ under ANOVA model.



to make comparisons simpler, and three levels of σ_A^2 , for three types of true and error score distributions, namely uniform (U1), normal (N0), and exponential (EX). Altogether the results of 27 experiments are summarized by tabulating the MS's (Table 5.8), standard errors (Table 5.9), and lower and upper 5% critical points of the distribution of reliability estimates with approximate real Type one errors when the nominal values are fixed at 5% level (Table 5.10).

These 27 experiments may be compared with the results of the corresponding experiments under the ANOVA model, namely experiments 1-3, 13-21, 31-39, and 49-54 of Tables 5.1, 5.2, and 5.3. The expected values of MS's and variance of MS_A show close agreement with observed values, but formula (5.6) does consistently underestimate the variance of MS_e, though the difference is trivial. Table 5.9 suggests that formula (5.10) closely approximates the observed standard error as in the case of ANOVA model. Observation of Table 5.10 also suggests that the pattern of discrepancy of real Type one error from the nominal value of 5% is almost the same as for the case of the ANOVA model, thus indicating non-existence of interaction effects between the non-homogeneous variance and non-normality of error score distributions.

5.2.4 Conclusions for the Distributions Under ETEM Model

The effects of non-homogeneous error variances on the sampling distribution of reliability estimates was investigated by simulating 21 experiments using three levels of ρ and 7 sets of error variances whose variance ranged from 0.0 to 42.1876. The following conclusions are tentatively made.

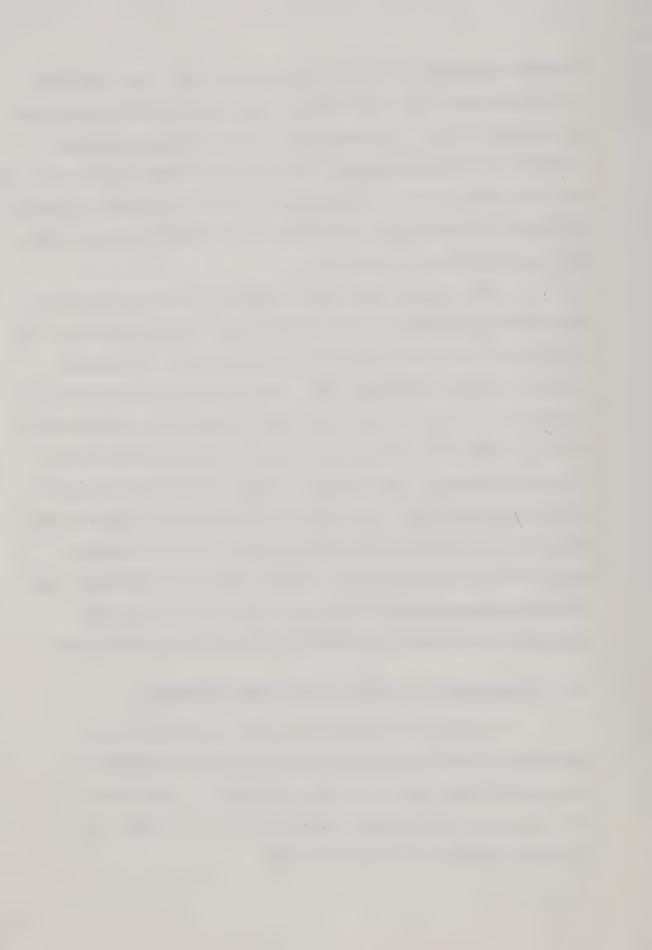


TABLE 5.8

Comparisons of Observed Means and Variances of MS's Under ETEM Model with EV2 Error Variances Set and Various Combinations of True and Error Score Distributions with the Values Obtainable from Formula (5.6), N = 2000, I = 30, J = 8

	D	is	Observ	red MS _A	Observ	ed MS _e	Var. by	(5.6)	Parameters,
No.	Tr.	Er.	Mean	Var.	Mean	Var.	MSA	MSe	Expected Values Under ANOVA
			(1)	(2)	(3)	(4)	(5)	(6)	(7)
01	Ul	Ul	36.063	46.826	4.005	0.094	48.348	0.078	$\sigma_A^2 = 4.0$
02	Ul	NO	36.119	45.750	3.996	0.184	48.428	0.158	**
03	Ul	EX	36.041	45.461	3.971	0.597	48.829	0.558	$\rho = 0.8888$
04	NO	Ul	35.946	81.623	4.005	0.094	89.308	0.078	$E(MS_A) = 36.0$
05	NO	ИО	36.041	85.556	4.000	0.184	89.388	0.158	= /un \
06	NO	EX	36.112	90.902	3.971	0.597	89.789	0.558	$E(MS_e) = 4.0018$
07	EX	U1	35.328	259.119	4.005	0.094	294.108	0.078	
08	EX	NO	35.347		3.996	0.184	294.188	0.158	
09	EX	EX	35.378	269.587	3.971	0.597	294.589	0.558	
10	Ul	U1	11.913	7.355	3.999	0.092	7.294	0.078	$\sigma_{\Lambda}^2 = 1.0$
11	U1	NO	12.019	7.240	3.995	0.189	7.374	0.158	A
12	Ul	EX	12.036	7.769	3.985	0.632	7.774	0.558	$\rho = 0.6666$
13	NO	Ul	12.049	9.579	3.999	0.092	9.854	0.078	$E(MS_A) = 12.0018$
14	NO	NO	12.034	9.581	3.995	0.189	9.934	0.158	A
15	NO	EX	12.083	10.585	3.985	0.632	10.334	0.558	
16	EX	U1	12.012	22.965	3.999	0.093	22.654	0.078	$E(MS_{e}) = 4.0018$
17	EX	NO	11.901	22.794	3.995	0.189	22.734	0.158	
18	EX	EX	11.918	23.848	3.985	0.632	23.134	0.558	
			1	2.01/	2 000	0.097	2.854	0.078	$\sigma_{A}^{2} = 0.36$
19	Ul	U1	6.877	2.916	3.990	0.189	2.934	0.078	A ~ 0.30
20	Ul	NO	6.879	2.891 3.264	4.002	0.607	3.335	0.558	$\rho = 0.4185$
21	Ul	EX	6.886	3.184	3.990	0.007	3.186	0.078	p = 0.470)
22	NO NO	U I NO	6.912	3.411	4.008	0.189	3.266	0.158	$E(MS_A) = 6.8818$
23 24	NO	EX	6.870	3.718	4.002	0.607	3.667	0.558	1 "
25	EX	Ul	6.870	4.620	3.990	0.097	4.845	0.078	$E(MS_e) = 4.0018$
26	EX	NO	6.873	4.662	4.008	0.189	4.925	0.158	e e
27	EX	EX	6.858	5.080	4.002	0.607	5.325	0.558	
2/	LA	-/	0.000						

(5.6)
$$\begin{cases} (a) & \text{Var } (MS_A) = \left[\frac{2}{I-1} + \frac{1}{I} \left\{\rho^2 \gamma_A + (1-\rho)^2 \gamma_e / J\right\}\right] \left(J \sigma_A^2 + \sigma_e^2\right)^2 \\ (b) & \text{Var } (MS_e) = \left[\frac{2}{(I-1)(J-1)} + \frac{\gamma_e}{IJ}\right] \sigma_e^4 \end{cases}$$

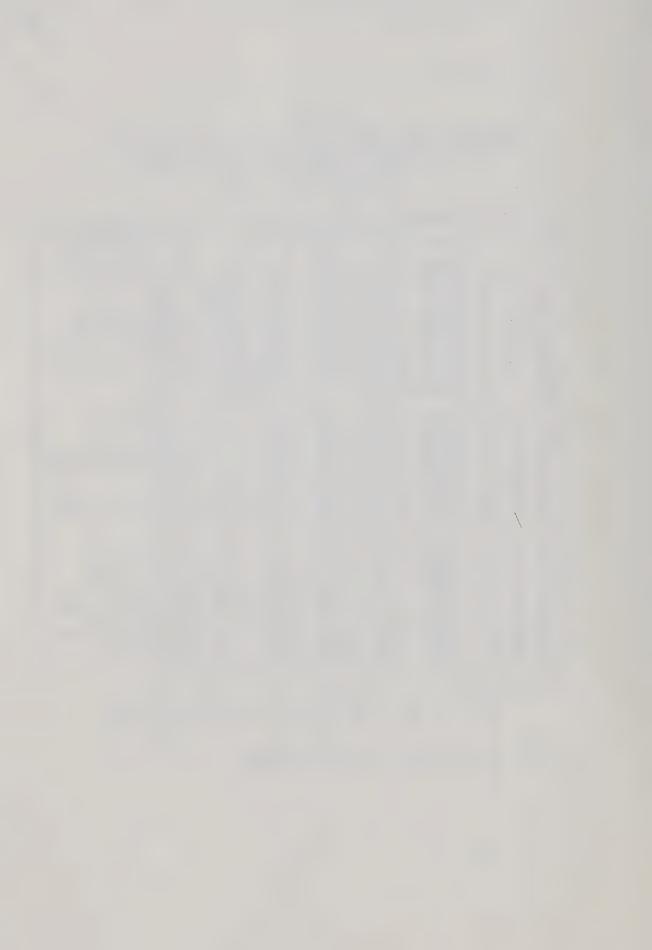


TABLE 5.9

Comparisons of Observed Means and Standard Errors of Reliability Estimates Under ETEM Model With EV2 Error Variances Set and Various Combinations of True and Error Score Distributions With the Values Obtainable From Formulas (5.3), (5.1), and (5.10), N = 2000, I = 30, J = 8

No.		s. Er.	Observ Mean	ved β S.E.	(5.3)	lated from (5.1)	formulas (5.10)	Parameters
			(1)	(2)	(3)	(4)	(5)	(6) -
01 02 03 04 05 06 07 08 09 10 11 12 13 14 15 16	UI UI NO NO EX EX EX EX EX EX	U1 NO EX EX U1 NO EX EX U1 EX EX EX EX EX EX EX EX EX EX EX EX EX	0.884 0.885 0.886 0.881 0.882 0.863 0.864 0.865 0.650 0.653 0.644 0.648 0.648	0.028 0.028 0.033 0.036 0.036 0.041 0.063 0.062 0.064 0.091 0.092 0.101 0.105 0.114 0.114	0.038 0.038 0.038 0.038 0.038 0.038 0.038 0.038 0.038 0.101 0.101 0.101 0.101 0.101 0.101	0.036 0.036 0.036 0.036 0.036 0.036 0.036 0.036 0.036 0.108 0.108 0.108 0.108 0.108 0.108	0.030 0.030 0.030 0.036 0.036 0.036 0.057 0.057 0.057 0.057 0.098 0.109 0.108 0.109 0.109 0.146 0.147	$\sigma_{A}^{2} = 4.0$ $\rho = 0.8888$ $E(\beta) = 0.8806$ $\sigma_{A}^{2} = 1.0$ $\rho = 0.6666$ $E(\beta) = 0.6419$
18 19 20 21 22 23 24 25 26 27	EX UI UI NO NO NO EX EX EX	EX U1 NO EX U1 NO EX U1 NO EX U1 NO EX	0.617 0.380 0.381 0.386 0.380 0.375 0.380 0.360 0.358 0.362	0.158 0.175 0.170 0.179 0.184 0.187 0.187 0.212 0.218	0.101 0.151 0.151 0.151 0.151 0.151 0.151 0.151	0.108 0.188 0.188 0.188 0.188 0.188 0.188 0.188 0.188	0.148 0.180 0.182 0.189 0.187 0.188 0.195 0.216 0.217 0.224	$\sigma_{A}^{2} = 0.36$ $\rho = 0.4185$ $E(\beta) = 0.3754$

(5.1)
$$\begin{cases} (a) & E(\beta) = 1 - (1-\rho) \frac{1-1}{1-3} \\ (b) & Var(\beta) = (1-\rho)^2 \frac{2(1-1)(\nu+1-3)}{(J-1)(1-3)^2(1-5)} \end{cases}$$

(5.3)
$$\operatorname{Var}(\beta) = \frac{(1-\rho^2)^2}{1}$$

(5.10) Var
$$(\beta) \simeq (1-\rho)^2 \left[\frac{2(1-1)(1J-J-2)}{(J-1)(1-3)^2(1-5)} + \frac{\gamma_y}{I}\right]$$



TABLE 5.10

Comparisons of Observed Lower and Upper Critical Points of Reliability Estimates and Real Type One Errors of F-Test When Nominal Value is 5%, Under ETEM Model With EV2 Error Variances Set and Various Combinations of True and Error Score Distributions With the Values Obtainable Under the ANOVA Model and Normal Theory, N = 2000, I = 30, J = 8

	Dis.		Real S	ig. %	Observe	ed C.P.	Theoretic	cal C.P. ²	
No.	Tr.	Er.	Lower	Upper	Lower	Upper	Lower	Upper	Parameters
			(1)	(2)	(3)	(4)	(5)	(6)	(7)
01 02 03 04 05 06	U1 U1 U1 NO NO NO	U1 NO EX U1 NO EX U1	1.50 1.80 3.25 4.60 4.10 5.40	1.45 1.85 5.85 3.95 4.90 8.65	0.838 0.839 0.826 0.817 0.818 0.810 0.746	0.920 0.921 0.928 0.925 0.927 0.934 0.940	0.814 0.814 0.814 0.814 0.814 0.814	0.927 0.927 0.927 0.927 0.927 0.927 0.927	$\sigma_{A}^{2} = 4.0$ $\rho = 0.8888$
08	EX	NO EX	17.15 18.40	11.50	0.745	0.927	0.814	0.927 0.927	
10 11 12 13	U1 U1 U1 NO	U1 NO EX U1	3.20 2.80 3.15 4.70	3.15 3.70 5.25 5.05	0.478 0.481 0.470 0.445	0.768 0.774 0.783 0.781	0.442 0.442 0.442 0.442	0.781 0.781 0.781 0.781	$\sigma_A^2 = 1.0$
14 15 16 17 18	NO NO EX EX EX	NO EX U1 NO EX	5.00 5.90 11.65 11.45 12.85	5.20 7.35 9.90 11.60 11.95	0.442 0.422 0.337 0.326 0.323	0.784 0.794 0.813 0.814 0.823	0.442 0.442 0.442 0.442 0.442	0.781 0.781 0.781 0.781 0.781	ρ = 0.6666
19 20 21 22	U1 U1 U1 N0	U1 NO EX U1	4.20 3.25 4.45 4.60	4.75 4.20 5.10 5.30	0.050 0.072 0.049 0.039	0.616 0.610 0.621 0.620	0.026 0.026 0.026 0.026	0.618 0.618 0.618 0.618	$\sigma_{A}^{2} = 0.36$
23 24 25 26 27	NO NO EX EX EX	NO EX U1 NO EX	5.15 4.80 6.85 7.60 7.20	4.70 5.25 7.10 7.10 8.50	0.018 0.033 -0.090 -0.051 -0.037	0.617 0.620 0.634 0.647 0.618	0.026 0.026 0.026 0.026 0.026	0.618 0.618 0.618 0.618 0.618	ρ = 0.4185

Observed lower and upper 5% critical points.

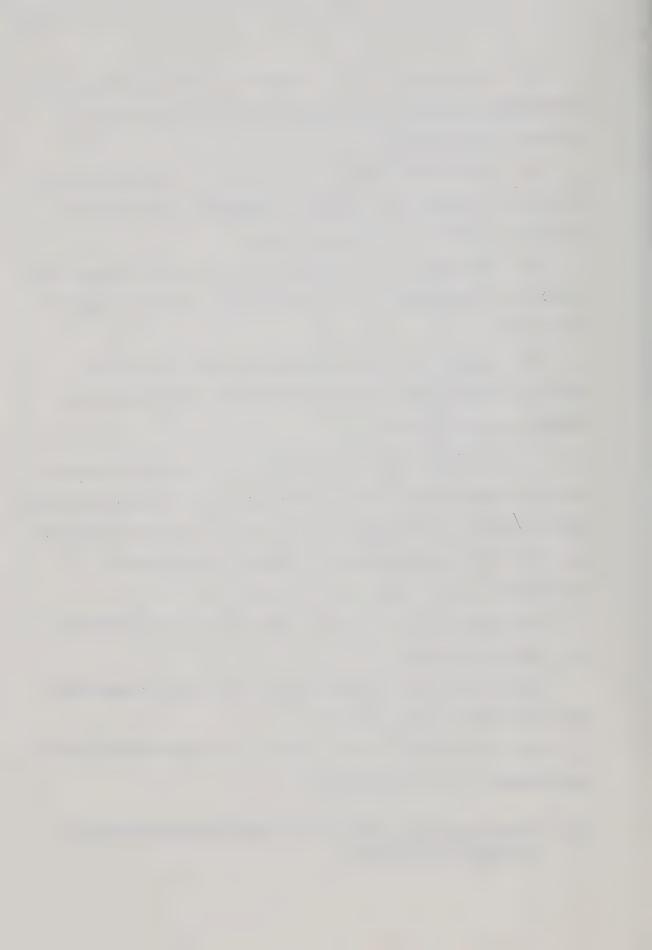
 $^{^2\}text{Theoretical lower and upper 5% critical points of }\beta$ under ANOVA model with normal distribution of true and error scores.



- (a) The variance of ${
 m MS}_{
 m e}$ is sensitive to the violation of the homogeneity assumptions, and formula (5.6) should not be used to calculate this statistic.
- (b) For the point estimation of reliability, the ANOVA model is quite robust against the violation of homogeneity of error variances provided that the distributions are normal.
- (c) The standard error of estimation is quite robust against the violation of the homogeneity of error variances. The best formula is still (5.10).
- (d) Formula (2.17) can be used freely without inflating or deflating Type one errors too much for the ETEM model provided that normality is not violated.

The effect of non-normal true or error score distributions under the ETEM model was investigated by performing 27 experiments with three levels of ρ , three types of true and error score distributions, and a set of non-homogeneous error variances. The following conclusions are tentatively made.

- (e) Formula (5.6) consistently underestimates the variance of ${\rm MS_e}$ under the ETEM model.
- (f) The interaction between the ETEM model and non-normal error score distribution seems negligible.
- (g) The conclusions drawn in Section 5.1.0 may be generalized to the ETEM model with little modification.
- 5.3.0 Relaxation of the Homogeneity of True Variance Constraint in the ANOVA or ETEM Models

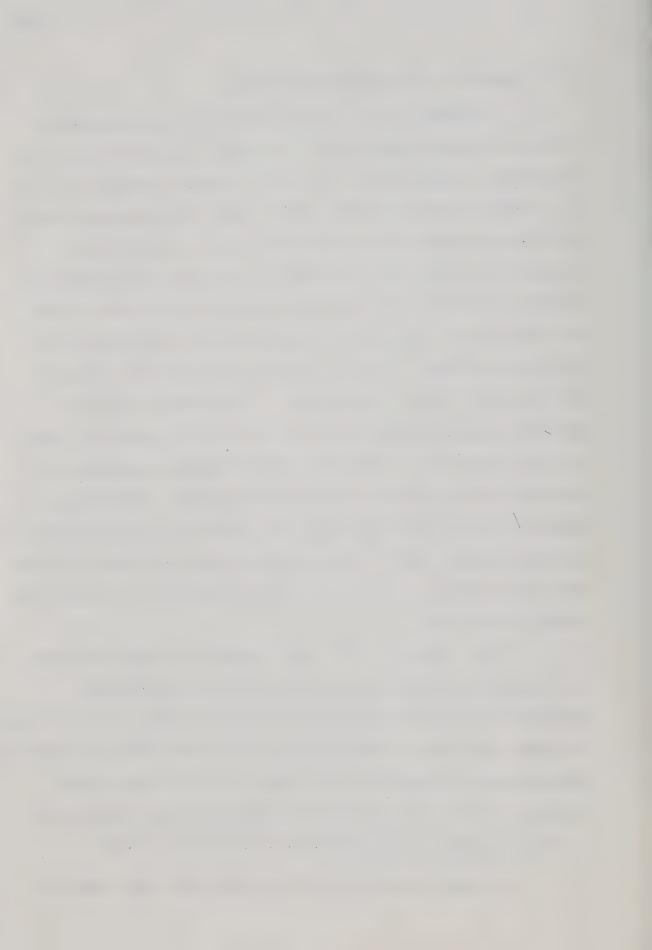


5.3.1 Reliability and the Alpha Coefficient

In Chapter Two, the ANOVA and ETEM models were expanded to include more general models such as the congeneric or multi-factor true score models through the use of the vector or matrix parameters $\,\lambda\,$ and Λ in equation (2.6) to produce (2.28). Under these more general models, the ETEM assumptions are not satisfied in general, and the Alpha coefficient is lower than the reliability coefficient. Therefore, one might be interested in two related but different distributions, namely, the sampling distributions of the Alpha coefficient estimates and the reliability estimates. However, the Alpha coefficient has attracted test theorist's interest only because it is considered a practical, and easily computable substitute for the reliability coefficient. Thus, the distribution of the Alpha coefficient estimates is meaningful only in lieu of the distribution of reliability estimates. Furthermore, because no direct estimation formula for reliability is available under these more general models, without exception Alpha coefficient estimates have been accepted as reliability estimates regardless of the underlying models or assumptions.

Test theorists know that the population Alpha coefficient is in general lower than the reliability, but this fact has been frequently confused with underestimation due to biasedness of the estimation procedure. Two kinds of underestimation problems that exist in reliability theory must be distinguished: one is due to deviation from the ETEM assumption, which is not a statistical inference problem, and the other is due to the nature of the estimation formula which is biased.

The sampling distribution of the Alpha coefficient under the



non-ETEM model is the most overlooked aspect of reliability theory.

No study has yet been reported on this subject to the author's know-ledge. Due to the mathematical complexity involved in these models, it seems almost impossible to investigate the problem by analytical means. Therefore, the problem was investigated as assumption violating cases of the ANOVA model using computer simulation techniques.

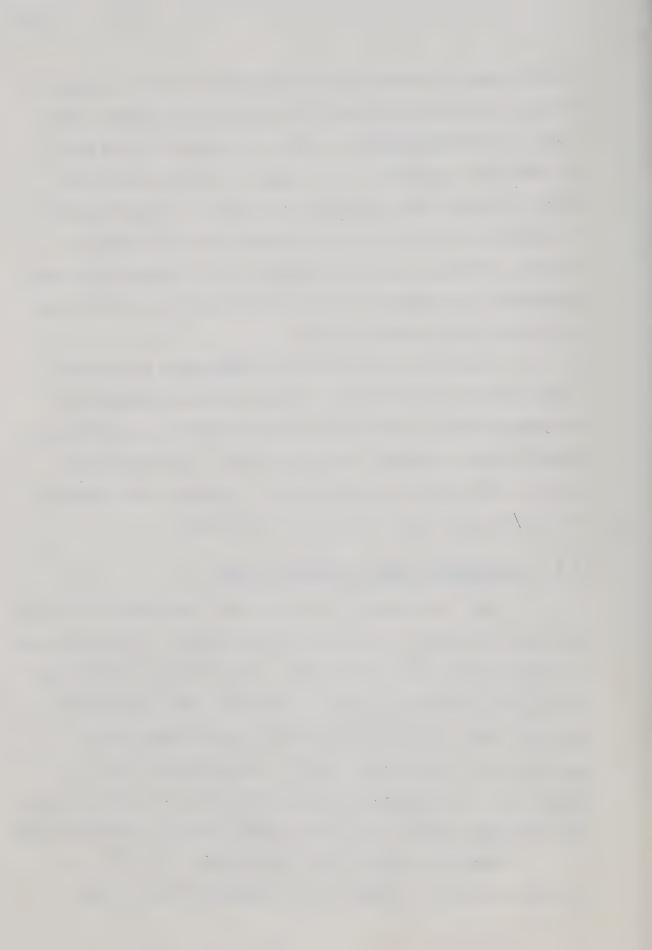
The major purpose is to find the effects of the violation of the ETEM assumptions, or homogeneity of true score variances and unifactorness of the true score dispersion matrix.

Because so many assumptions of ANOVA models are violated under these more general models, an exhaustive investigation of all the combinations of possible violation of assumptions is prohibitively expensive with the computer simulation method. The study in this section is limited to a few combinations. Therefore, the findings in this section have limited value for generalization.

5.3.2 Distributions Under the Congeneric Model

Under the congeneric true score model, each part-test measures the same trait except for the errors of measurement, i.e., the factorial structure of true scores is unifactor. Therefore all part-test scores have linearly related true scores. Test scores under the classically parallel, ANOVA (or essentially parallel), or ETEM models are all special cases of the congeneric model, as discussed more fully in Chapter Two. In these special cases any true score of a part-test must be essentially identical for a given subject, unlike the congeneric model.

Under the congeneric model, the variance, $\sigma_{Aj}^2 = \lambda_j^2$, of true score for part j depends on j, and there is not a common



variance parameter σ_A^2 which has played a key role in the ETEM or ANOVA models. To obtain the corresponding parameters for the congeneric model, a new parameter σ_A^2 is defined denoting the average of the all elements of the dispersion matrix $\frac{\lambda}{\Delta}$, namely,

(5.13)
$$\sigma_{A.}^{2} = (\underline{1}' \underline{\lambda} \underline{\lambda}' \underline{1})/J^{2} = (\sum_{j} \sum_{j'} \lambda_{j} \lambda_{j'})/J^{2}.$$

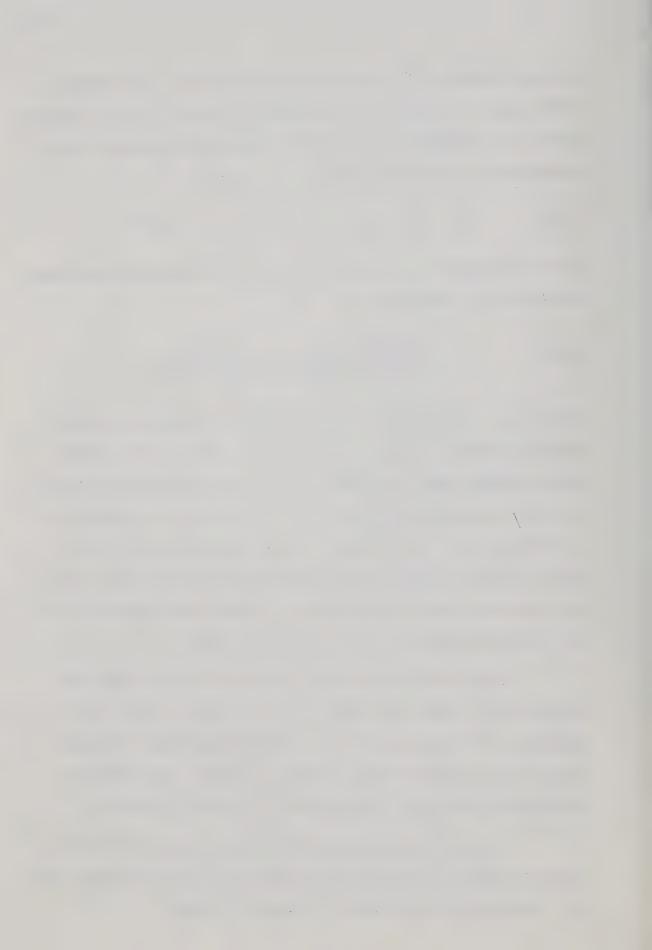
As this parameter is an average of true score variance and covariances, the reliability coefficient is,

(5.14)
$$\rho = \frac{\underline{1}' \underline{\lambda} \underline{\lambda}' \underline{1}}{\underline{1}' (\underline{\lambda} \underline{\lambda}' + \underline{\Psi}^2) \underline{1}} = \frac{J^2 \sigma_A^2}{J^2 \sigma_A^2 + J \sigma_e^2}$$

where σ_e^2 is the average of error variances as defined by (2.22), namely the mean of $\{\sigma_{ej}^2\}$. Since the distribution (2.17) obtained under the ANOVA model and normal distribution theory does not directly involve the parameters σ_A^2 and σ_e^2 , but only directly involves the reliability ρ , it is desirable to know whether the distribution of reliability estimates based on formula (2.13)-(b) is robust against the violation of ETEM assumptions, i.e., whether the relation (2.17) still holds approximately for the congeneric cases.

Under the congeneric model, formula (2.13)-(b) gives the estimate of the Alpha coefficient, not the reliability, but it is hoped that, with moderate violation of ETEM assumptions, inferences based on the estimate of Alpha would not invalidate the inferences of reliability too much as in the case of the previous section.

To see the effects of non-homogeneous true score variances, sampling experiments were performed using the following three sets of $\underline{\lambda}$'s representing three levels of reliability, namely,



$$\underline{\lambda}_{1} = \begin{bmatrix}
1.6 \\
1.8 \\
1.8 \\
2.0 \\
2.0 \\
2.2 \\
2.4
\end{bmatrix}, \qquad \underline{\lambda}_{2} = \begin{bmatrix}
0.8 \\
0.9 \\
0.9 \\
1.0 \\
1.0 \\
1.1 \\
1.1 \\
1.2
\end{bmatrix}, \qquad \underline{\lambda}_{3} = \begin{bmatrix}
0.72 \\
0.66 \\
0.66 \\
0.60 \\
0.54 \\
0.54 \\
0.48
\end{bmatrix},$$

which gives three levels of σ_{A}^2 namely 4.0, 1.0, and 0.36 and three levels of ρ , i.e., 0.8889, 0.6667, and 0.4186 respectively. The $\underline{\lambda}$'s were chosen such that the values of σ_{A}^2 equal σ_{A}^2 used for the ANOVA and ETEM model experiments in Sections 5.1.0 and 5.2.0, in order to facilitate the comparisons. The error variances $\{\sigma_{e_i}^2\}$ are fixed at $4.0\,$ as the ANOVA model, and the same constants are used for $\,$ N, $\,$ I, and J, i.e., 2000, 30, and 8 respectively. Employing three types of true and error score distributions, namely uniform (U1), normal (N0), and exponential (EX), altogether 27 experiments were performed by RELOI, and the results are summarized in Tables 5.11, 5.12, and 5.13. As in the previous sections, the distributions of MS's are examined first. From Table 5.11, it is noted that the effects of non-homogeneous true score variances are minimal, i.e., the results are almost identical with those under ANOVA model given in Table 5.1. Table 5.12 summarizes the means and standard errors of reliability estimates under this model and compares them with the values obtainable from formulas (5.3), (5.1)-(b), and (5.10). It is clearly noticed that formula (5.10) is still the best among the three. When the means of $\hat{\rho}$ in Table 5.12 are compared with the corresponding values of Table 5.2, it may be noticed that under the congeneric model the mean of $\hat{\rho}$ is lower than under the ANOVA model, as expected, since the formula used for the estimation, (2.13), is for the estimation of Alpha, and Alpha is lower than

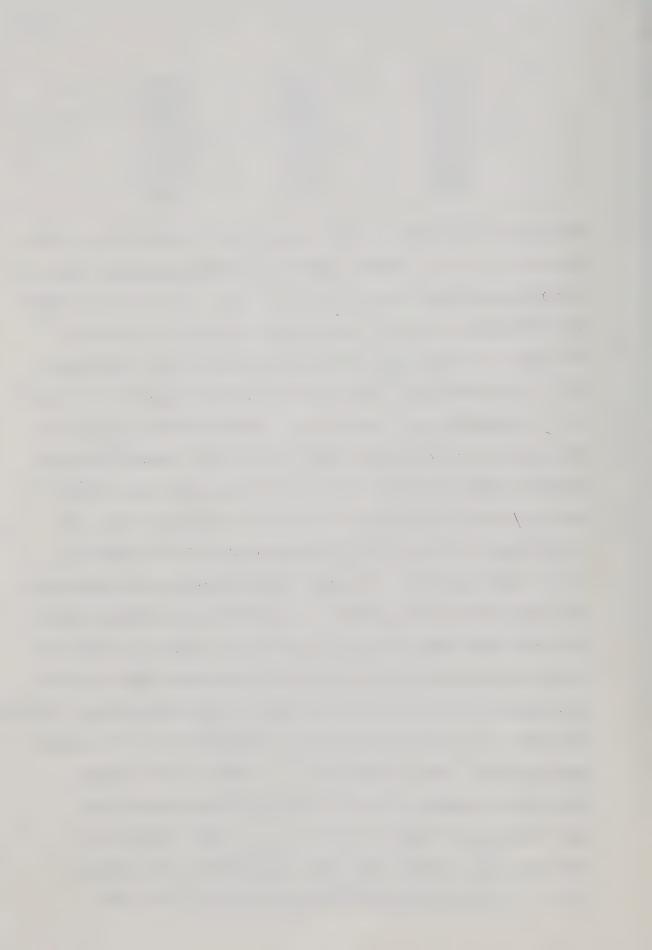


TABLE 5.11

Comparisons of Observed Means and Variances of MS's Under the Congeneric Model and Various Combinations of True and Error Score Distributions With the Values Obtainable From Formula (5.6), N = 2000, I = 30, J = 8

Ex.	Dis.		Obser	ved MS _A	Observ	ved MS _e	Var. by	(5.6)	Parameters
No.	Tr.	Er.	Mean	Var.	Mean	Var.	MSA	MSe	and E(MS)
			(1)	(2)	(3)	(4)			(7)
01 02 03 04 05 06 07 08 09 10 11 12 13 14 15 16	U1 U1 N0 N0 N0 EX EX EX U1 U1 N0 N0 N0 EX EX EX	U1 NO EX U1	(1) 36.052 36.102 36.057 35.931 36.016 36.130 35.335 35.358 35.380 11.924 12.028 12.028 12.030 12.051 12.029 12.076 12.005 11.883 11.913	(2) 47.112 45.563 45.036 81.750 85.812 90.374 258.849 270.871 269.881 7.389 7.147 7.657 9.555 9.492 10.484 23.121 22.484 23.485 2.910	(3) 4.075 4.068 4.036 4.075 4.069 4.040 4.071 4.064 4.009 4.008 3.999 4.010 4.009 3.999 4.010 3.998	0.089 0.168 0.531 0.090 0.167 0.525 0.091 0.168 0.525 0.085 0.168 0.560 0.086 0.169 0.560 0.086	(5) 48.339 48.419 48.819 89.299 89.379 89.779 294.099 294.179 294.579 7.291 7.371 7.771 9.851 9.931 10.331 22.651 22.731 23.131 2.853	(6) 0.078 0.158 0.558 0.078 0.158 0.558 0.078 0.158 0.558 0.078 0.158 0.558 0.078 0.158 0.558 0.078 0.158 0.078	$\sigma_{A}^{2} = 4.0$ $\rho = 0.8889$ Alpha = 0.8870 $E(MS_{A}) = 36.0$ $E(MS_{e}) = 4.0$ $\sigma_{A}^{2} = 1.0$ $\rho = 0.6667$ Alpha = 0.6652 $E(MS_{A}) = 12.0$ $E(MS_{e}) = 4.0$
20	υı	NO	6.869	2.886	4.012	0.171	2.933	0.158	
21	UI	EX	6.868	3.180	4.003	0.526	3.333 3.184	0.558 0.078	$\rho = 0.4186$
22	NO NO	U I NO	6.911	3.161 3.363	3.997 4.012	0.000	3.104	0.078	Alpha = 0.4177 E(MS _A) = 6.880
24	NO	EX	6.858	3.629	4.003	0.526	3.664	0.558	
25	EX	Ul	6.862	4.534	3.996	0.087	4.843	0.078	$E(MS_e) = 4.0$
26 27	EX	NO EX	6.865	4.627 4.995	4.012 4.004	0.173	4.923 5.323	0.158 0.558	

(5.6)
$$\begin{cases} (a) & \text{Var } (MS_A) = \left[\frac{2}{I-1} + \frac{1}{I} \left\{\rho^2 \gamma_A + (1-\rho)^2 \gamma_e / J\right\}\right] \left(J\sigma_A^2 + \sigma_e^2\right)^2 \\ (b) & \text{Var } (MS_e) = \left[\frac{2}{(I-1)(J-1)} + \frac{\gamma_e}{IJ}\right] \sigma_e^4 \end{cases}$$

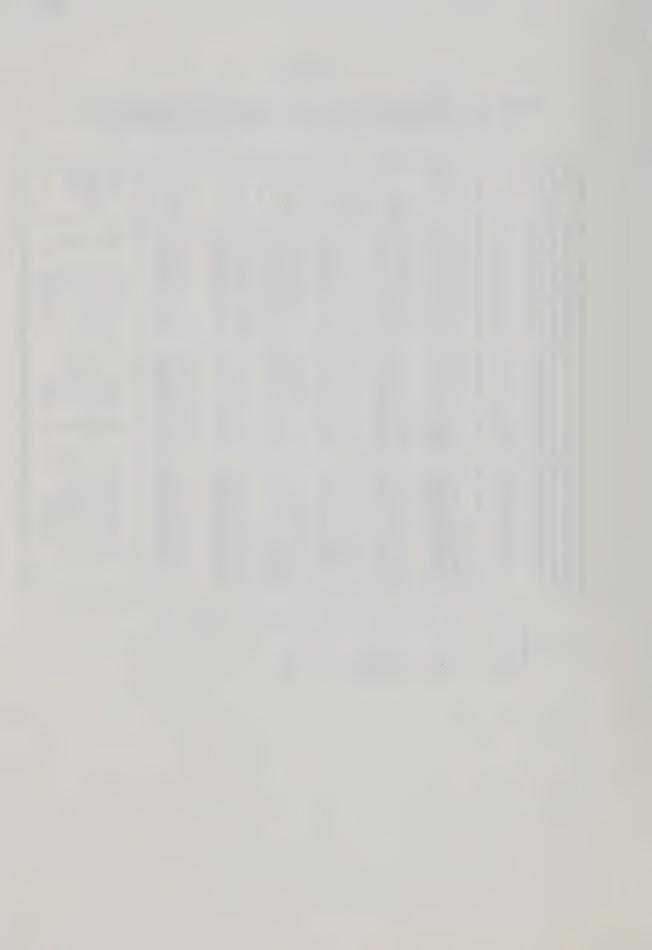


TABLE 5.12

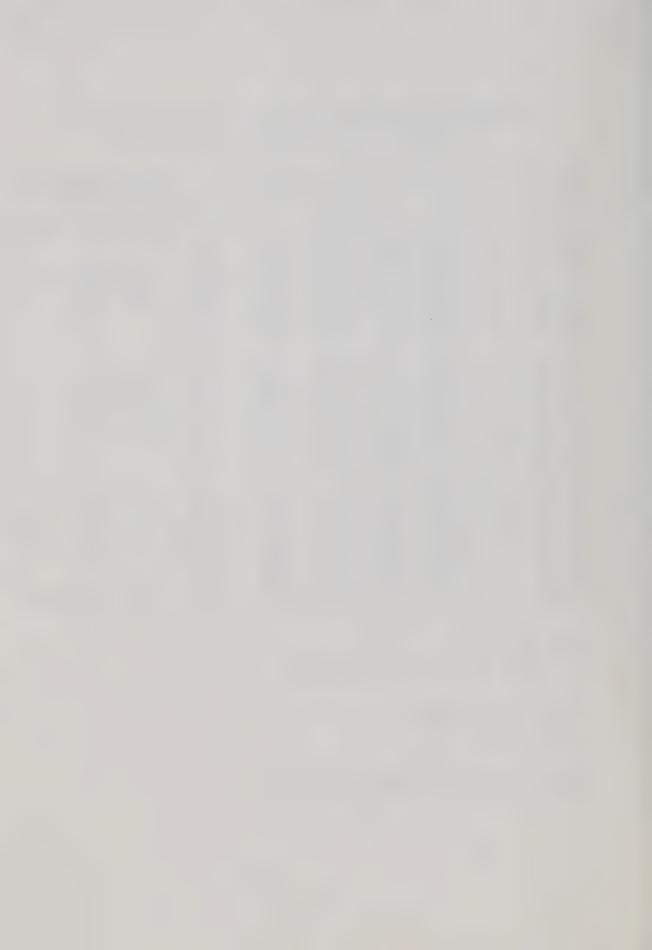
Comparisons of Observed Means and Standard Errors of Reliability Estimates Under the Congeneric True Score Model With the Values Obtainable From Various Formulas, N=2000, I=30, J=8

Exp.	Dis.		Observ	/ed ρ̂	S.E. b	y formulas		Parameters and expected
No.	Tr.	Er.	Mean	S.E.	(5.3)	(5.1)-(b)	(5.10)	values under ANOVA
			(1)	(2)	(3)	(4)	(5)	(6)
01 02 03 04 05 06 07 08	UI UI UI NO NO NO EX	UI NO EX UI NO EX UI	0.882 0.883 0.884 0.879 0.879 0.880 0.862 0.862	0.028 0.028 0.033 0.036 0.036 0.040 0.062 0.061	0.038 0.038 0.038 0.038 0.038 0.038 0.038	0.036 0.036 0.036 0.036 0.036 0.036 0.036	0.030 0.030 0.030 0.036 0.036 0.036 0.057	$\sigma_{A}^{2} = 4.0$ $\rho = 0.8889$ Alpha = 0.8870 $E(\beta) = 0.8807$
09	EX	EX U1	0.863	0.064	0.038	0.036	0.057	$\sigma_{\Delta}^2 = 1.0$
11 12 13 14	UI UI NO NO	NO EX U1 NO	0.649 0.651 0.643	0.091 0.098 0.106 0.105	0.101 0.101 0.101 0.101	0.108 0.108 0.108 0.108	0.098 0.100 0.108 0.108	p = 0.6667 Alpha = 0.6652
15 16 17 18	NO EX EX EX	EX U1 NO EX	0.646 0.613 0.611 0.615	0.114 0.155 0.156 0.157	0.101 0.101 0.101 0.101	0.108 0.108 0.108 0.108	0.109 0.146 0.147 0.148	E(s) = 0.6420
19 20 21 22 23 24 25 26 27	UI UI NO NO NO EX EX	UI NO EX UI NO EX UI NO EX	0.379 0.379 0.383 0.378 0.373 0.378 0.359 0.356 0.360	0.175 0.172 0.179 0.186 0.189 0.186 0.213 0.219 0.217	0.151 0.151 0.151 0.151 0.151 0.151 0.151 0.151	0.188 0.188 0.188 0.188 0.188 0.188 0.188 0.188	0.180 0.182 0.189 0.186 0.188 0.195 0.216 0.217	$\sigma_A^2 = 0.36$ $\rho = 0.4186$ Alpha = 0.4177 $E(\hat{\rho}) = 0.3755$

(5.1)
$$\begin{cases} (a) & E(\beta) = 1 - (1-\rho) \frac{1-1}{1-3} \\ (b) & Var(\beta) = (1-\rho)^2 \frac{2(1-1)(\nu+1-3)}{(J-1)(1-3)^2(1-5)} \end{cases}$$

(5.3)
$$\operatorname{Var}(\beta) = \frac{(1-\rho^2)^2}{1}$$

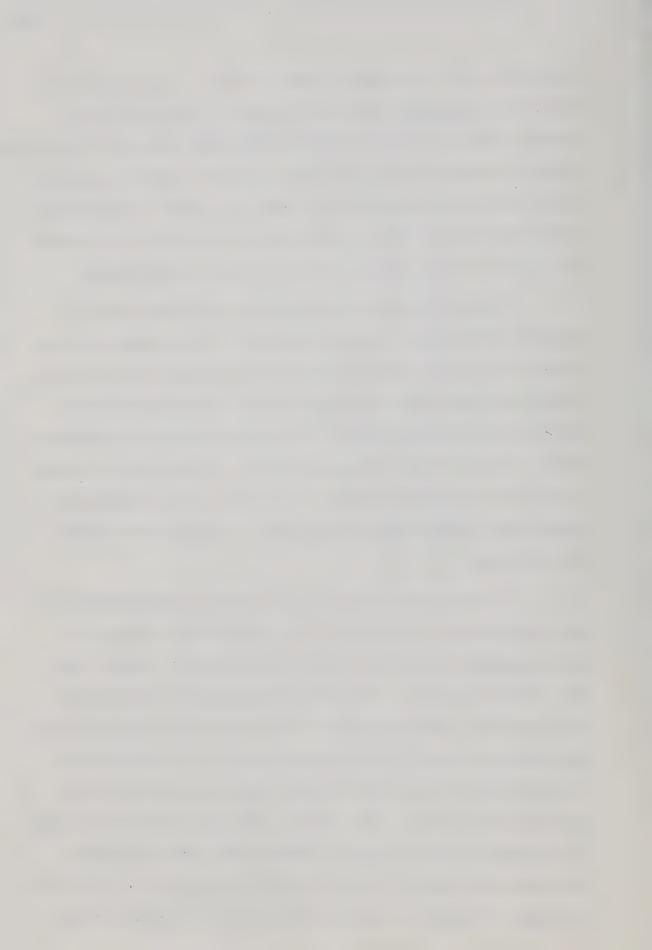
(5.10) Var
$$(\beta) \simeq (1-\rho)^2 \left[\frac{2(1-1)(1J-J-2)}{(J-1)(1-3)^2(1-5)} + \frac{\gamma_y}{i} \right]$$

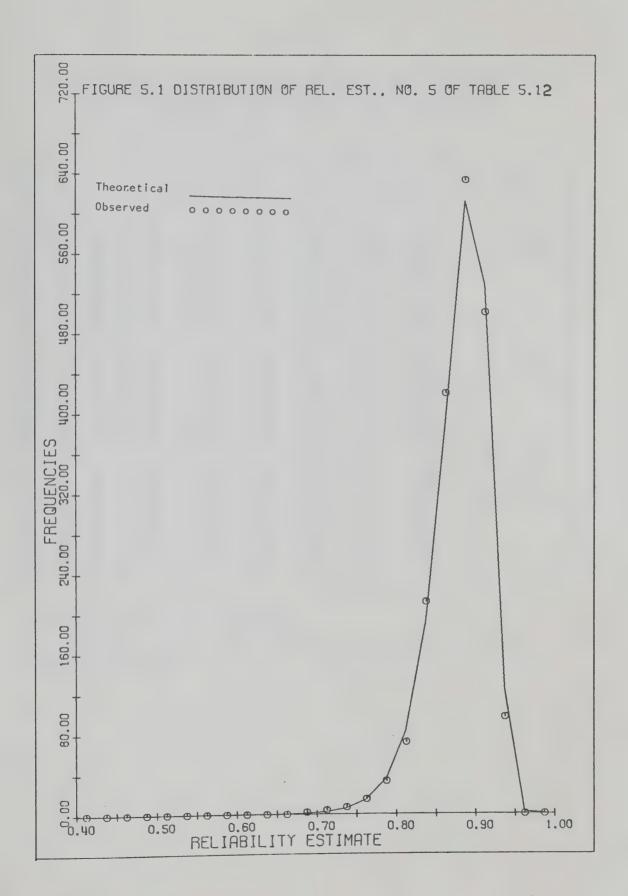


reliability under the congeneric model. However, as can be seen in Figure 5.1, the shapes of the distributions are almost the same as expected from (2.17), namely under the ANOVA model and normal distribution theory. Therefore similar conclusions as cited in Section 5.1.5 may be obtained from the observation of Table 5.13, namely the real significance levels of the F-test, or the lower and upper 5% critial points of $\hat{\rho}$ are almost the same as the values under the ANOVA model.

To make the comparisons between the ANOVA model and the congeneric model, and to separate the effects of non-homogeneous true scores variances from the effects of non-homogeneous error variances, further experiments were performed under the same conditions as the ANOVA model cases except that the true score variances were allowed to differ. However, there is some possibility of the existence of interaction effects between the effects of violating the two homogeneity assumptions, although each case was found to be quite robust against the violations.

To investigate this problem, 15 additional experiments were performed employing three sets of $\underline{\lambda}$'s as before and five sets of non-homogeneous error variances used in Section 5.2.0, namely EV3, EV4, EV5, EV6, and EV7. The results are summarized in Tables 5.14, 5.15, and 5.16. When the entries of these tables are compared with the corresponding values of Tables 5.5, 5.6, and 5.7, little difference is noted between the two sets of values suggesting non-existence of such interaction effects. For example, experiment 3 of Table 5.5 gives the observed variance of MS_A as 88.222, while the corresponding value under the congeneric model is given in experiment 1 of Table 5.14 as 89.270. Therefore, it may be concluded that, the effect of non-





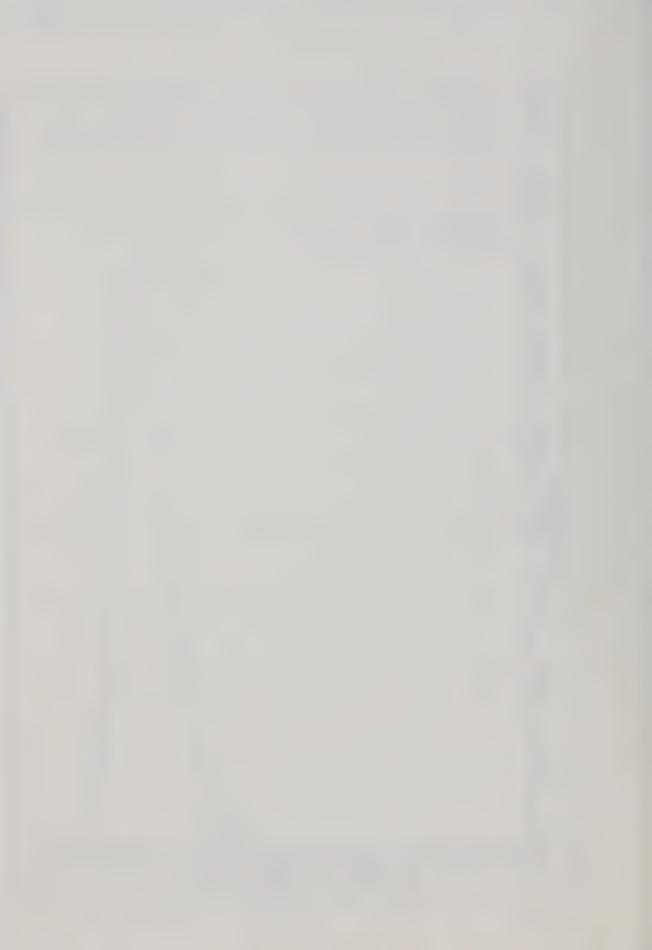


TABLE 5.13

Comparisons of Observed Lower and Upper 5% Critical Points of Reliability Estimates
Under the Congeneric True Score Model with the Values Obtainable Under the
ANOVA and Normal Theory, and Real Type One Error of F-Test When the
Nominal Value is 5%, N = 2000, I = 30, J = 8

Exp.	Dis.		True Si	g. (%)	Observe	ed C.P.	Theoreti	cal C.P. ²	
No.	Tr.	Er.	Lower	Upper	Lower	Upper	Lower	Upper	Parameters
		:	(1)	(2)	(3)	(4)	(5)	(6)	(7)
01 02 03 04 05 06 07 08 09 10 11 12 13 14 15 16 17 18	U1 U1 NO NO NO EX EX EX U1 U1 NO NO NO EX EX U1 U1 NO NO NO NO NO NO NO EX EX EX U1 U1 NO NO NO NO NO NO NO NO NO NO NO NO NO	UI NO EX UI NO	1.90 1.85 2.75 5.15 4.60 5.65 17.85 18.35 3.35 3.05 3.75 4.60 6.05 11.70 12.05 12.80 3.85 3.65 4.80 5.25	1.35 1.65 4.05 2.90 3.95 6.95 9.64 10.45 11.70 2.80 3.35 4.85 4.80 7.10 10.45 11.05 11.85 4.85 4.60 4.55 4.60	0.834 0.835 0.826 0.813 0.816 0.810 0.745 0.745 0.475 0.482 0.470 0.448 0.325 0.328 0.319 0.058 0.068 0.040 0.030 0.020 0.020	0.917 0.918 0.925 0.924 0.925 0.930 0.938 0.940 0.942 0.768 0.771 0.781 0.778 0.780 0.791 0.812 0.812 0.812 0.618 0.610 0.614 0.614 0.616 0.617	0.814 0.814 0.814 0.814 0.814 0.814 0.814 0.814 0.814 0.442	0.927 0.927 0.927 0.927 0.927 0.927 0.927 0.927 0.927 0.781 0.781 0.781 0.781 0.781 0.781 0.781 0.781	$\sigma_{A}^{2} = 4.0$ $\rho = 0.8889$ Alpha = 0.887 $\sigma_{A}^{2} = 1.0$ $\rho = 0.6667$ Alpha = 0.6652 $\sigma_{A}^{2} = 0.36$ $\rho = 0.4186$ Alpha = 0.4177
24 25 26	NO EX EX	EX U1 NO	5.00 7.15 8.40	4.65 6.95 7.20	-0.027	0.635	0.027	0.618	
27	EX	EX	7.40	8.40	-0.052	0.648	0.027	0.618	

Observed lower and upper 5% critical points.

 $^{^{2}}$ Theoretical lower and upper 5% critical points under ANOVA with normal distribution of true and error scores.

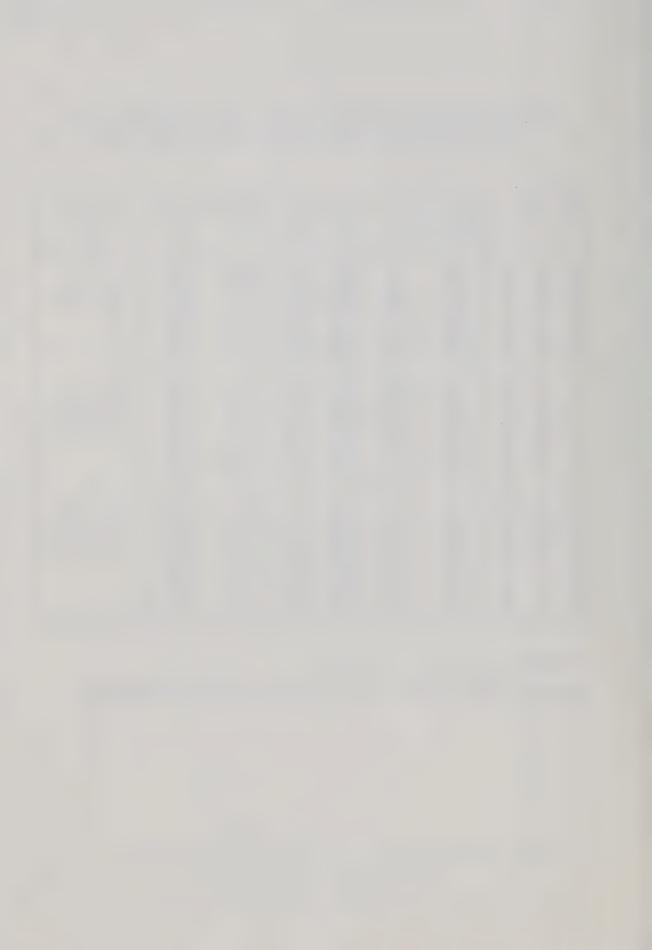


TABLE 5.14

Comparisons of Observed Means and Variances of MS's Under Congeneric True Scores, Non-Homogeneous Error Variances and the Normal Distributions With the Values
Obtainable Under ANOVA Model, N = 2000, I = 30, J = 8

Exp.	Er. Type	Observe Mean	Var.	Observe Mean	Var.	E (MSA)	Var. by	MSe	Parameters
		(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
01 02 03 04 05	EV3 EV4 EV5 EV6	36.101 35.611 36.308 38.742 36.915	89.270 83.103 87.363 103.316 96.880	3.832 3.630 4.321 6.472 4.819	0.224 0.239 0.441 0.708 0.618	35.750 35.562 36.250 38. 37 5 36.750	88.142 87.220 90.625 101.561 93.142	0.139 0.125 0.178 0.400 0.222	$\sigma_{A}^2 = 4.0$
06 07 08 09	EV3 EV4 EV5 EV6 EV7	11.795 11.633 12.249 14.477 12.740	9.654 9.566 10.121 15.206 11.321	3.758 3.574 4.693 6.376 4.775	0.241 0.223 0.432 0.702 0.609	11.750 11.562 12.250 14.375 12.750	9.522 9.220 10.349 14.251 11.211	0.139 0.125 0.178 0.400 0.222	σ _A . = 1.0
11 12 13 14 15	EV3 EV4 EV5 EV6 EV7	6.700 6.430 7.120 9.306 7.593	3.203 2.779 3.491 5.915 3.782	3.768 3.564 4.258 6.394 4.753	0.221 0.232 0.430 0.771 0.620	6.630 6.442 7.130 9.255 7.630	3.032 2.862 3.506 5.907 4.015	0.139 0.125 0.178 0.400 0.222	$\sigma_{A}^{2} = 0.36$

$$E(MS_e) = \sigma_e^2 = 3.750 (EV3)$$

3.563 (EV4)
4.250 (EV5)
6.375 (EV6)
4.750 (EV7)

(5.6)
$$\begin{cases} (a) & \text{Var } (MS_A) = \left[\frac{2}{i-1} + \frac{1}{i} \left\{\rho^2 \gamma_A + (1-\rho)^2 \gamma_e / J\right\}\right] \left(J\sigma_A^2 + \sigma_e^2\right)^2 \\ \\ (b) & \text{Var } (MS_e) = \left[\frac{2}{(1-1)(J-1)} + \frac{\gamma_e}{IJ}\right] \sigma_e^4 \end{cases}$$

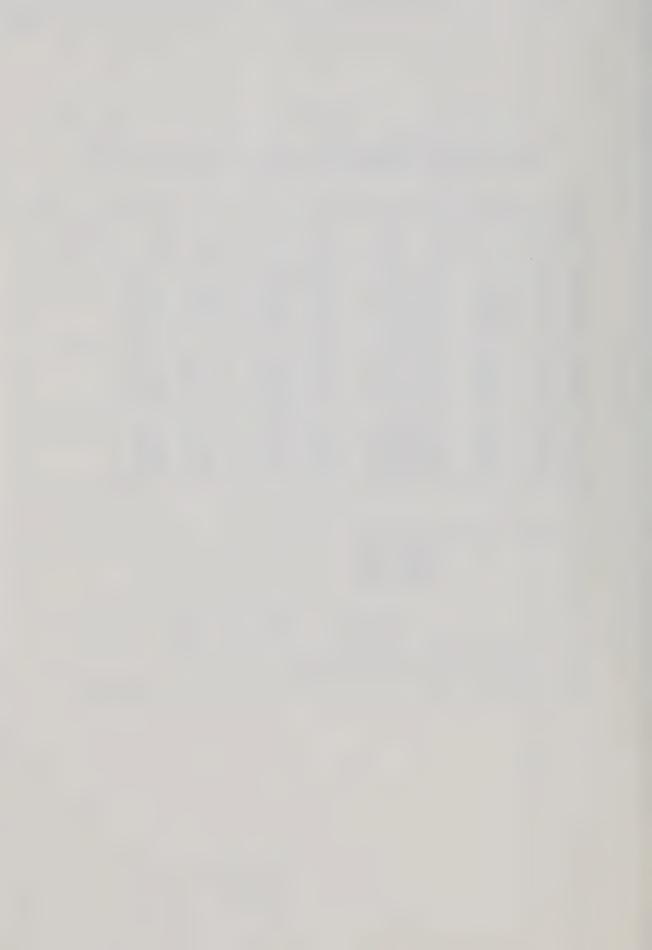


TABLE 5.15

Comparisons of the Observed Means and Standard Error of Reliability Estimates Under Congeneric True Score, Non-Homogeneous Error Variances and Normal Distributions With the Values Obtainable From Formulas (5.1), (5.3), and (5.10), N = 2000, I = 30, J = 8

Exp. No.	Er. Var.	Rel.	Alpha (2)	E(β) by (5.1)-(a) (3)	Observ Mean (4)	/ed β S.E. (5)	S.E. (5.3) (6)	by (5.10) (7)	Parameter (8)
01 02 03 04 05 06 07 08 09 10	EV3 EV4 EV5 EV6 EV7 EV3 EV4 EV7	0.895 0.900 0.883 0.834 0.871 0.681 0.692 0.653 0.557 0.628	0.893 0.898 0.881 0.832 0.869 0.679 0.690 0.652 0.555 0.626	0.887 0.892 0.874 0.822 0.861 0.657 0.669 0.627 0.524 0.600	0.886 0.891 0.873 0.821 0.860 0.658 0.670 0.628 0.528 0.601	0.036 0.034 0.041 0.055 0.048 0.102 0.114 0.140 0.119	0.036 0.035 0.040 0.056 0.044 0.098 0.095 0.105 0.126 0.111	0.034 0.032 0.038 0.054 0.042 0.103 0.100 0.112 0.143 0.121	$\sigma_{A}^{2} = 4.0$ $\sigma_{A}^{2} = 1.0$ $\sigma_{A}^{2} = 0.36$
14	EV6 EV7	0.311	0.311	0.260	0.268	0.207	0.165	0.223	

(5.1)
$$\begin{cases} (a) & E(\beta) = 1 - (1-\rho) \frac{1-1}{1-3} \\ (b) & Var(\beta) = (1-\rho)^2 \frac{2(1-1)(y+1-3)}{(J-1)(1-3)^2(1-5)} \end{cases}$$

(5.3) Var
$$(\beta) = \frac{(1-\rho^2)^2}{1}$$

(5.10) Var (
$$\hat{\rho}$$
) $\simeq (1-\rho)^2 \left[\frac{2(1-1)(1J-J-2)}{(J-1)(1-3)^2(1-5)} + \frac{\gamma_y}{1} \right]$

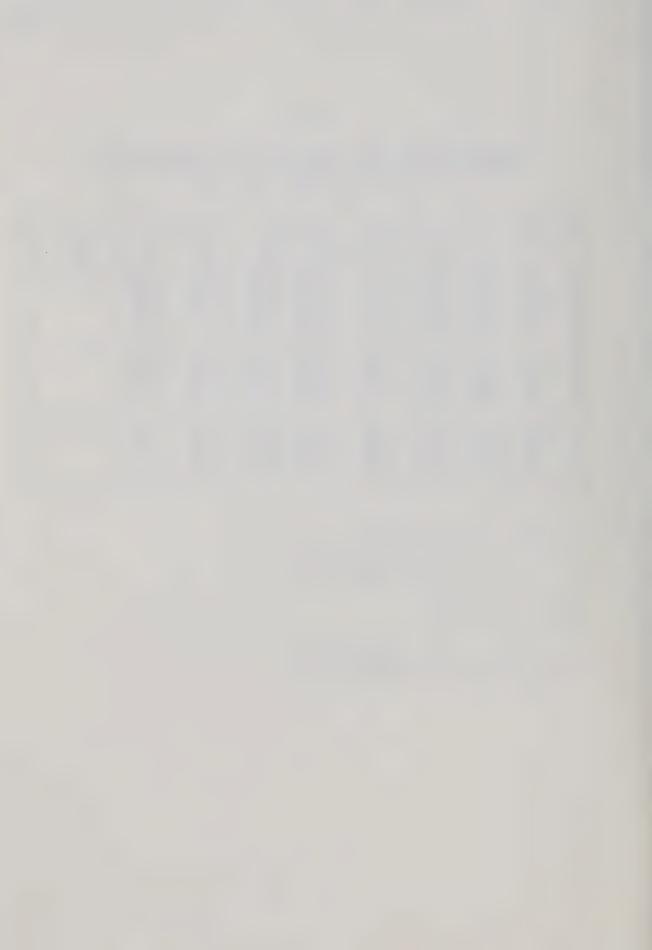


TABLE 5.16

Comparisons of Observed Lower and Upper 5% Critical Points Under Congeneric True Scores, Non-Homogeneous Error Score Variance, and Normal Distributions With the Values Obtainable Under the ANOVA and Normal Theory, and Real Type One Errors of F-Test When the Nominal Value is 5%,

N = 2000, I = 30, J = 8

Exp.	Er.		Pol E(β) by		ed C.P.	Theoreti	Theoretical C.P. ²		Sig. (%)	
No.	Var.	Rel.	(5.1)-(b)	Lower	Upper	Lower	Upper	Lower	Upper	Parameter
		(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	· (9)
01 02 03 04 05 06 07 08 09 10	EV3 EV4 EV5 EV6 EV7 EV3 EV4 EV5 EV6 EV7	0.895 0.900 0.883 0.834 0.871 0.681 0.692 0.653 0.557 0.628 0.434 0.447 0.404	0.887 0.892 0.874 0.822 0.861 0.657 0.669 0.627 0.524 0.600 0.393 0.406 0.360 0.260	0.821 0.829 0.795 0.720 0.774 0.448 0.485 0.417 0.271 0.377 0.059 0.096 0.022	0.930 0.934 0.924 0.892 0.917 0.792 0.802 0.773 0.713 0.757	0.824 0.832 0.804 0.722 0.784 0.466 0.484 0.419 0.258 0.376 0.053 0.074 0.002 -0.153	0.931 0.934 0.923 0.891 0.915 0.791 0.798 0.772 0.709 0.755 0.629 0.637 0.609 0.548	5.90 5.90 6.50 5.25 6.50 5.80 5.00 5.15 4.40 4.90 4.80 4.70 4.10 4.30	4.50 4.80 5.60 5.25 6.20 5.10 5.60 5.15 5.95 5.20 5.35 3.90 4.05 4.70	$\sigma_{A.}^{2} = 4.0$ $\sigma_{A.}^{2} = 1.0$ $\sigma_{A.}^{2} = 0.36$
15	EV7	0.378	0.331	-0.035	0.582	-0.042	0.591	4.75	4.15	

 $^{^{1}}$ Observed lower and upper 5% critical points of $\,$ $\,$ $\,$

 $^{^2\}text{Theoretical lower}$ and upper 5% critical points of $\,\beta\,$ under ANOVA model.

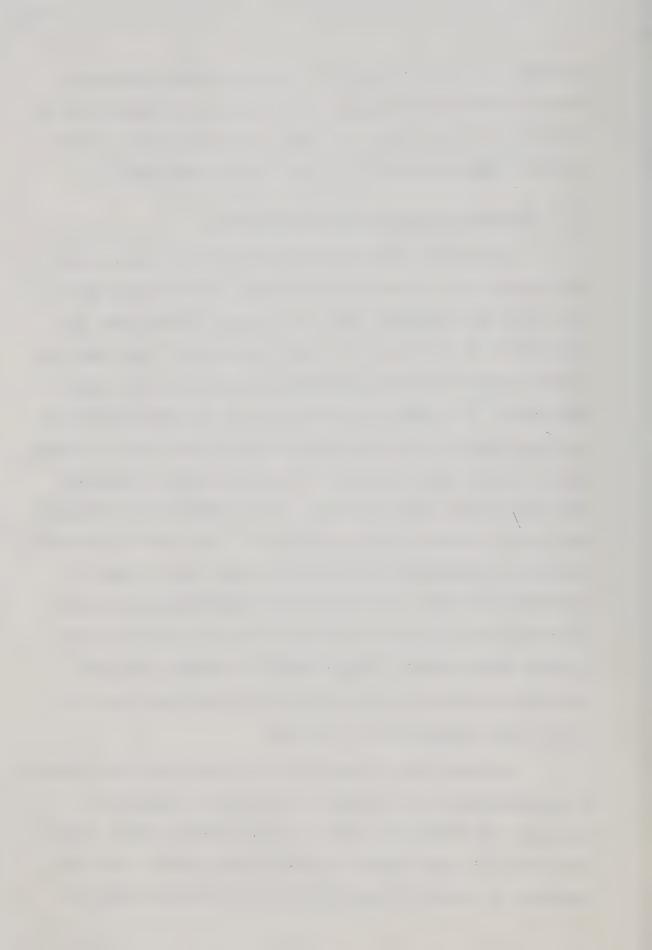


homogeneous true score variance, or violation of ETEM assumption will affect the sampling distribution of the reliability estimates given by (2.17) very little as long as the degree of non-homogeneity is within a moderate range as with the λ 's used in these experiments.

5.3.3 <u>Distributions Under the Multi-Factor Model</u>

Classically, the assumption of a one-factor true score has been referred to as one which produces 'unit rank correlation matrix' (e.g., Kuder and Richardson, 1937), but as seen in Chapter Two, the unifactorness of true scores is inherent to the ANOVA linear model and its more general form such as the ETEM or congeneric models. Under these models, it is implicitly assumed that the test measures only one trait, and therefore, the true score can have only one factor structure. However, in real test score data, it is seldom possible to separate measurement of one trait from others. The psychological or achievement tests usually measure more than one trait at a time, and it is sometimes unrealistic to assume that only one factor exists and to regard all other factors as error. This fact has been well demonstrated by the rejection by many researchers of Spearman's so-called g-factor theory in modern factor analysis. Thus violation of unifactor true score assumption may not be considered simply as an exceptional case; this may be rather a common case for real data.

In Chapter Two, the multi-factor test model has been introduced as a generalization of the congeneric test model by expanding the linear model of ANOVA step by step to a factor analytic model. However, since most of the test theories are based on the unifactor true score assumption, no reliability theory has ever been developed under this



model. Therefore the multi-factor model has been referred to as an assumption violating case of the classical model rather than a separate model in its own right. Following this traditional line, in this study, the reliability distribution under the multi-factor model is treated as an assumption violating case of the ANOVA model as are other models examined in the previous sections.

Since the Alpha coefficient is a measure of the first factor concentration (Cronbach, 1951), the coefficient is expected to be much lower than the reliability coefficient if second or higher factor is not negligible. Therefore, it is hardly expected that the sampling distribution of Alpha coefficient, as a substitute for the reliability estimate, is robust against the violation of the unifactor assumption.

To support this conjecture, a number of sampling experiments were performed and the results are compared with those obtainable under ANOVA model. The parameters σ_A^2 and σ_e^2 are not defined under this model as with the congeneric model case, but the average of true and error score variance may be used to determine the effectiveness of the ANOVA model under the multi-factor model, namely,

(5.15)
$$\sigma_{A}^{2} = (\underline{1}' \underline{\Lambda} \underline{\Lambda}' \underline{1})/J^{2} = (\sum_{j} \sum_{j'} \sum_{r} \lambda_{jr} \lambda_{j'r})/J^{2},$$

and σ_{e}^{2} as in the previous section.

If these parameters are used in place of σ_A^2 and σ_e^2 , most of the formulas introduced in Section 5.1.0 can be used directly and the robustness of the ANOVA model under multi-factor true score cases can be examined empirically by the simulation techniques.



Using the following two $\underline{\Lambda}$ matrices, an error score standard deviation matrix $\underline{\Psi}$, and three types of true and error score distributions, altogether 18 experiments were performed under the multi-factor true score model with N = 2000, I = 30, J = 6,

$$\underline{\Lambda}_{1} = \begin{bmatrix} 0.887 & 0.302 \\ 0.410 & 0.663 \\ 0.242 & 0.735 \\ 0.369 & 0.816 \\ 0.417 & 0.557 \\ 0.669 & 0.482 \end{bmatrix}, \qquad \underline{\Lambda}_{2} = \frac{1}{2} \underline{\Lambda}_{1} = \begin{bmatrix} 0.4435 & 0.1510 \\ 0.2050 & 0.3315 \\ 0.1210 & 0.3675 \\ 0.1845 & 0.4080 \\ 0.2085 & 0.2785 \\ 0.3345 & 0.2410 \end{bmatrix}$$

$$\underline{\Psi} = \begin{bmatrix} 0.34942 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 0.62636 & 0.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & 0.63341 & 0.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & 0.0 & 0.63341 & 0.0 & 0.0 & 0.0 \\ 0.0 & 0.0 & 0.0 & 0.0 & 0.44495 & 0.0 & 0.0 \\ 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.71823 & 0.0 \\ 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.56579 \end{bmatrix}.$$

Table 5.17 compares the observed means and variances of the MS's under the multi-factor model with the values obtainable from formula (5.6) treating the model as an ANOVA model. It is noted that rather close agreement exists between the means of the observed MS_A and E(MS_A) given in colums (1) and (7), but the agreement is rather poor between the means of observed MS_e and E(MS_e) given in columns (3) and (7) indicating the effect of the violation of unifactor true score assumption. Even for the normal true and error score distributions, the difference between the two values are too big to be explained as sampling fluctuation. For example, experiment 5 gives the mean of MS_e as 0.413 while the theoretical value of E(MS_e) = 0.3249 if the ANOVA model and $\sigma_{\rm e}^2$ are used. This implies that the E(MS_e) undervalues the real expected value of MS_e. When the variances of MS's, in colums (2) and (4), are compared with the values obtainable from formula (5.6)

TABLE 5.17

Comparisons of Observed Means and Variances of MS's Under the Multi-Factor True Score Model and Various Combinations of True and Error Score Distributions With the Values Obtainable Under ANOVA Model by Formula (5.6), N = 2000, I = 30, J = 6

Exp.	Dis		0bserv	ed MSA	Observ	ved MS _e	Var. by	y (5.6)	Parameters
No.	Tr.	Er.	Mean	Var.	Mean	Var.	MSA	MSe	and E(MS)
			(1)	(2)	(3)	(4)	(5)	(6)	(7)
01 02 03 04 05 06	U1 U1 U1 NO NO	U1 NO EX U1 NO EX	3.916 3.915 3.902 3.919 3.919 3.913	0.761 0.800 0.814 1.087 1.066 1.036	0.436 0.414 0.414 0.413 0.413	0.0017 0.0026 0.0067 0.0019 0.0027 0.0066	0.542 0.544 0.548 1.062 1.063 1.066	0.0008 0:0015 0.0050 0.0008 0.0015 0.0050	$\sigma_{A.}^{2} = 0.6001$ $\sigma_{e.}^{2} = 0.3249$ $E(MS_{A}) = 3.9235$
07 08 09	EX EX	U1 NO EX	3.898 3.895 3.887	2.341 2.278 2.309	0.414 0.414 0.413	0.0027 0.0036 0.0073	3.655 3.656 3.659	0.0008 0.0015 0.0050	$E(MS_e) = 0.3249$
10 11 12 13 14 15 16 17	U1 U1 NO NO NO EX EX EX	UI NO EX UI NO EX UI NO EX	1.233 1.220 1.218 1.231 1.223 1.225 1.220 1.216 1.242	0.086 0.089 0.089 0.103 0.103 0.109 0.181 0.174 0.188	0.345 0.346 0.346 0.348 0.346 0.346 0.347 0.346	0.0010 0.0019 0.0058 0.0010 0.0019 0.0059 0.0011 0.0020 0.0063	0.070 0.071 0.075 0.103 0.103 0.107 0.265 0.266 0.269	0.0008 0.0015 0.0050 0.0008 0.0015 0.0050 0.0008 0.0015 0.0050	$\sigma_{A.}^{2} = 0.1500$ $\sigma_{e.}^{2} = 0.3249$ $E(MS_{A}) = 1.225$ $E(MS_{e}) = 0.3249$

(5.6)
$$\begin{cases} (a) & \text{Var } (MS_A) = \left[\frac{2}{1-1} + \frac{1}{1} \left\{\rho^2 \gamma_A + (1-\rho)^2 \gamma_e / J\right\}\right] (J\sigma_A^2 + \sigma_e^2)^2 \\ (b) & \text{Var } (MS_e) = \left[\frac{2}{(1-1)(J-1)} + \frac{\gamma_e}{1J}\right] \sigma_e^4 \end{cases}$$



given in columns (5) and (6), rather poor agreement is noticed, suggesting inapplicability of the formula.

Table 5.18 gives means and standard errors of reliability estimates and compares them with the values obtainable from formulas (5.3), (5.1)-(b), and (5.10). It is observed that, for all experiments, the mean of $\hat{\rho}$ is much lower then population Alpha or $E(\hat{\rho})$ under ANOVA and normal theory, indicating the effect of the multi-factor true score structure. This result is probably due to the fact that the Alpha coefficient measures mainly the variance due to the first factor, and thus underestimates the true score variance and overestimates the error score variance, and at the same time shifting the distribution of reliability estimates considerably to the left as shown in Figure 5.2. Although formula (5.10) seems still to be the best among the three, the fit is very poor suggesting inapplicability of most of the formulas derived under the ANOVA model and normal theory for multi-factor true score test.

Discrepancies between observed and theoretical distributions based on ANOVA model are clearly seen when the real significance level of F-test is compared with the nominal value of 5%, as summarized in Table 5.19. The real significance level for the lower tail range from 14.40% to 27.50% for Λ_1 and 5.80% to 12.30% for Λ_2 , clearly indicating the inapplicability of the conventional F-test to multifactor tests. For the upper tail, the true significance levels are in general lower than the nominal value, but the results are not predictable. For example, experiment 2 gives a value as low as 0.45%, while experiment 18 gives one as high as 8.10%. All of these results

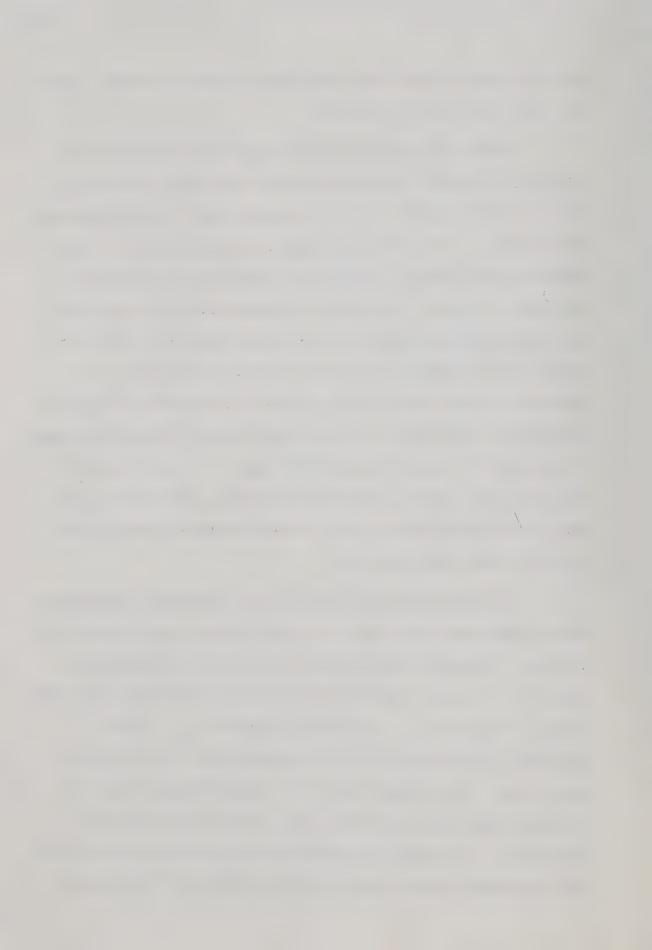


TABLE 5.18

Comparisons of Observed Means and Standard Errors of Reliability Estimates Under the Multi-Factor True Score Model and Various Combinations of True and Error Score Distributions With the Values Obtainable From Formulas (5.3), (5.1)-(b) and (5.10), N= 2000, 1 = 30, J = 6

			Observ	/ed β	Calcula	ated S.E. by		Parameters and $E(\beta)$,
Ex.	Dis. Tr.	Er.	Mean	S.E.	(5.3)	(5.1)-(b)	(5.10)	ANOVA and Normal
		LI.	(1)	(2)	(3)	(4)	(5)	(6)
01 02 03 04 05 06 07 08	U1 U1 U1 NO NO NO EX EX	UI NO EX UI NO EX UI	0.888 0.888 0.887 0.886 0.886 0.887 0.879	0.032 0.033 0.039 0.037 0.038 0.038 0.042	0.029 0.029 0.029 0.029 0.029 0.029 0.029 0.029	0.027 0.027 0.027 0.027 0.027 0.027 0.027	0.023 0.023 0.023 0.027 0.027 0.027 0.044 0.044	$\sigma_{A.}^{2} = 0.6001$ $\sigma_{e.}^{2} = 0.3249$ $\rho = 0.9172$ Alpha = 0.8943 $E(\beta) = 0.9111$
10 11 12 13 14 15 16 17	EX U1 U1 U1 NO NO NO EX EX EX	EX UI NO EX UI NO EX UI NO EX UI NO EX	0.880 0.702 0.698 0.700 0.695 0.696 0.696 0.682 0.682	0.049 0.085 0.088 0.097 0.093 0.096 0.106 0.115 0.118 0.120	0.029 0.084 0.084 0.084 0.084 0.084 0.084 0.084	0.027 0.088 0.088 0.088 0.088 0.088 0.088 0.088	0.044 0.078 0.079 0.080 0.088 0.088 0.089 0.124 0.124	$\sigma_{A}^{2} = 0.1500$ $\sigma_{e}^{2} = 0.3249$ $\rho = 0.7348$ Alpha = 0.7164 $E(\beta) = 0.7151$

(5.1)
$$\begin{cases} (a) & E(\beta) = 1 - (1-\beta) \frac{1-1}{1-3} \\ (b) & Var(\beta) = (1-\beta)^2 \frac{2(1-1)(y+1-3)}{(J-1)(1-3)^2(1-5)} \end{cases}$$

(5.3) Var
$$(\hat{\rho}) = \frac{(1-\rho^2)^2}{1}$$

(5.10) Var (ô) =
$$(1-p)^2 \left[\frac{2(1-1)(1J-J-2)}{(J-1)(1-3)^2(1-5)} + \frac{\gamma_y}{1} \right]$$



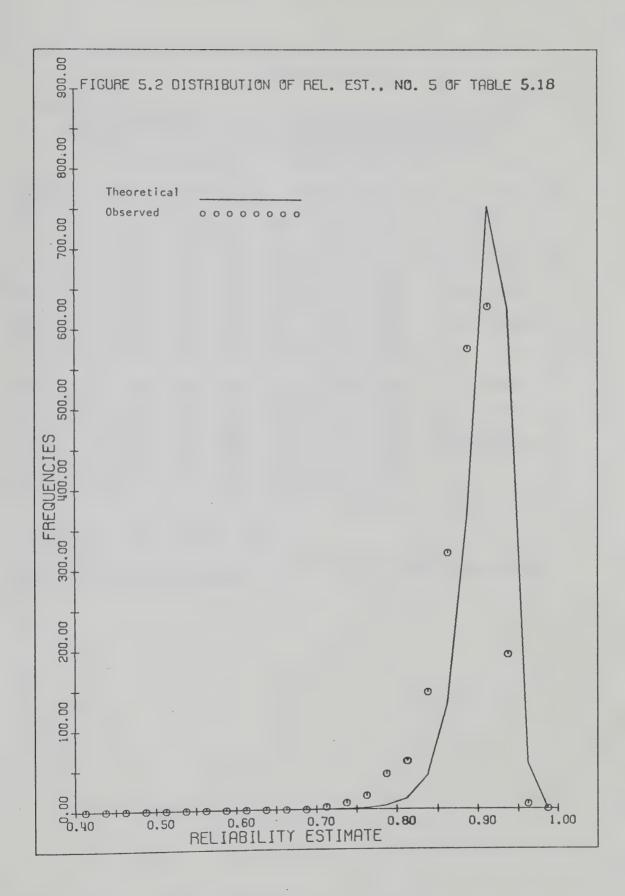




TABLE 5.19

Comparisons of Observed Lower and Upper 5% Critical Points of Reliability Estimates and Real Type One Errors of F-Test When the Nominal Value is 5% Under the Multi-Factor True Score Model and Various Combinations of True and Error Score Distributions With the Values Obtainable Under the ANOVA Model and Normal Theory, N = 2000, I = 30, J = 6

Exp.	Dis.		Real	Sig. (%)	Observ	ved C.P.	Theore	tical C.P. ²	Parameters
No.		Er.	Lower	Upper	Lower	Upper	Lower	Upper	
			(1)	(2)	(3)	(4)	(5)	(6)	(7)
01	บา บา	U1 NO	15.35	0.50	0.813	0.929	0.860	0.946	$\sigma_{A.}^{2} = 0.6001$
03	U1 NO	EX U1	19.50	1.45	0.817	0.934	0.860	0.946	$\sigma_{\rm e.}^2 = 0.3249$
05 06 07	NO NO EX	NO EX U1	18.90 20.90 27.50	0.55 1.45 1.25	0.815 0.819 0.814	0.932 0.936 0.939	0.860 0.860 0.860	0.946 0.946 0.946	ρ = 0.9172 Alpha = 0.8943
08 09	EX	NO EX	26.45 26.80	1.55	0.797	0.936	0.860	0.946	
10 11	U1	U1 NO	5.80 6.85	2.25	0.541	0.813	0.552	0.828 0.828	$\sigma_{A.}^{2} = 0.1500$
12 13 14	U 1 NO NO	EX U1 NO	7.95 7.55 8.20	4.05 2.40 2.95	0.522 0.524 0.508	0.825 0.814 0.814	0.552 0.552 0.552	0.828 0.828 0.828	$\sigma_{\rm e.}^2 = 0.3249$ $\rho = 0.7348$
15	NO EX	EX U1	8.45 12.06	4.70	0.500	0.826	0.552	0.828 0.828	Alpha = 0.7164
17 18	EX	NO EX	12.30 11.56	4.85 8.10	0.450	0.828 0.845	0.552	0.828	

Observed lower and upper 5% critical points of δ .

Theoretical lower and upper 5% critical points of $\,\beta\,$ under the ANOVA model with normal distribution of true and error scores.



strongly suggest that ANOVA model and normal theory are not robust against the violation of the assumption of unifactor true score.

5.3.4 Conclusions for the Effects of Non-ETEM Model

Based on the above discussions, the following conclusions are tentatively made.

- (a) Formula (5.6) may be used for the congeneric test case if σ_A^2 and σ_e^2 are used in place of σ_A^2 and σ_e^2 of ANOVA model. However, this formula is valueless for the case of multi-factor true score model.
- (b) The non-homogeneity of true score variance has little effect on the distribution, although the ETEM assumption is violated if the violation is moderate. The conclusions obtained in Section 5.1.5 may be generalized to the congeneric true score cases with moderate violation of ETEM assumption.
- (c) The effects of violation of the unifactor true score assumption are the most critical. If this assumption is violated, the formulas derived under the ANOVA model cannot be applied directly even with a normal true score distribution.
- (d) The F-test based on (2.17) may be used for the congeneric model if the true score distribution is approximately normal as in the ANOVA model case and the homogeneity of true score variance is satisfied approximately, but it would be misleading in multi-factor model cases. This is especially true for inferences based on lower portions or high reliability case. As previous sections showed, these effects diminish with the lower values of reliability.

Findings in this section are based on rather limited combinations of possible parameters and distributions of true and

error scores, and therefore, generalization must be made with care.

5.4.0 Summary

Sampling distributions of reliability estimates for the continuous part-test cases are investigated under the ANOVA, ETEM, and congeneric and multi-factor true score models with various combinations of true and error scores distributions by analytical and computer simulation methods. Tukey's results for the calculation of the variance of variance estimate under an ANOVA model were applied to test theory to obtain an approximate formula for standard error of reliability estimates when the distributions of true and error scores are not necessary normal.

To investigate sampling distributions of reliability estimates based on formula (2.13) under these models and distributional assumptions not necessarily normal, to see robustness of the ANOVA model and normal theory represented by the formula (2.17), and to evaluate the new formula for the standard error of reliability estimates, altogether 156 experiments were performed by RELO1, each requiring approximately 6 minutes of computer C.P.U. time. From the experiments, the following conclusions may be obtained.

- (a) The equation (2.17) obtained under the ANOVA model and normal theory is quite robust against the violation of the following assumptions if the reliability estimate is based on (2.13), i.e., the estimation formula for Alpha coefficient:
 - i) Normality of error score distributions.
 - ii) Homogeneity of error score variances.
 - iii) Homogeneity of true score variances, if violation is moderate.

(x,y) = (x,y) + (x,y

.

But the ANOVA model and normal theory is not robust against violation of the following assumptions.

- i) Unifactorness of true score dispersion matrix.
- ii) Normality of true score distributions.

The effects of the violation of these last two assumptions will decrease as the values of reliability decrease.

- (b) For the F-test based on the equation (2.17), the multifactor true score model increases Type one error for the lower tail and decreases it for the upper tail by shifting the distributions of reliability estimates leftward substantially, when second or higher factors of the true score dispersion matrix cannot be ignored.
- (c) The effects of non-normal true score distributions depend on the magnitude of their kurtosis. For negative kurtosis, Type one errors for both tails are less than the nominal value, while for positive kurtosis, they are greater than the nominal value. The greater the absolute value of kurtosis, the greater is the discrepancy from the nominal value.
- (d) If true scores are distributed as normal, the ANOVA, ETEM, and congeneric models give almost identical distributions of reliability estimates with moderate departures from homogeneity assumptions of error and/or true score variances.
- (e) The new standard error formula (5.10) is superior to the traditional formulas (5.1) or (5.3), if the true scores are not distributed as normal.

CHAPTER SIX

RESULTS FOR BINARY ITEM TEST SCORE CASES

This chapter presents the results of computer simulated experiments for the binary item test score cases. Section 6.1 deals with the overall factors which might affect the distribution of reliability estimates. In Section 6.2, the effects of non-normal error distributions are investigated with normal latent score distributions and homogeneous biserial correlations. Section 6.3 deals with the cases of non-normal latent scores with homogeneous biserial correlations and normal error scores, while Section 6.4 deals with non-normal latent scores and non-homogeneous biserial correlations. For all cases, both homogeneous and non-homogeneous item difficulty parameters are employed to determine the effects of non-homogeneous difficulty parameters.

6.1 Factors Related to Binary Item Test Scores Distribution

As discussed in Chapter Three, for a composite test consisting of J binary items as its part-tests, direct decomposition of observed score \mathbf{x}_{ij} , which takes the value unity for a correct response and zero otherwise, into two independent parts, namely true and error scores, is impossible. Thus the linear model equation (3.3) can only be applied to an intervening variable or 'response strength variable' \mathbf{y}_{ij} which is a hypothetical continuous variable.

Under the normal ogive model, it was possible to evaluate test parameters such as the variance σ_X^2 , reliability ρ , and KR20 by means of numerical methods if the item parameters, such as difficulty

parameters $\{\pi_j\}$ and biserial correlations $\{\lambda_j\}$, are specified. Unfortunately, however, the computational formulas given in Chapter Three are valid if and only if the normal ogive model is valid, namely, if the $\{f_i\}$ and $\{\epsilon_{ij}\}$ are independently and identically distributed as N(0,1) as discussed in Section 4.6 of Chapter Four. Thus the nonnormal distributions of these two types of random variables would affect not only the sampling distribution of reliability estimates, but also the population test parameters.

Furthermore, for the continuous part score case, the fixed constant for each part, β_i , indicates the relative difficulty level of each part-test, but these parameters do not enter any formula for reliability or any other test parameters, and are independent of the sampling distribution of reliability estimates. Therefore it was not necessary to consider the effects of $\{\beta_i\}$ on the distribution of reliability estimates. For the binary item case, however, the item difficulty parameters, the analogue of β_i for the continuous case, enter the formula (3.15) through threshold constants and consequently affect such test score parameters, as the mean, variance, reliability and KR20. Furthermore, as shown in Section 3.4 of Chapter Three, the ETEM assumption is satisfied if and only if the items are all homogeneous, namely they have equal difficulty and biserial correlation parameters. Therefore, if the difficulty parameters are not homogeneous, it is expected that the KR20 will be lower than the reliability and subsequently the sampling distribution of reliability estimates may differ from that of the homogeneous case, though there is some indication that the effects are not great (Nitko and Feldt, 1969).

:

As a result, for the binary item cases, the following factors must be taken into account for a study of sampling distributions of reliability estimates:

- (a) The effect of non-normal distributions of $\{f_i\}$ and $\{\epsilon_{ij}\}$, i.e., the effect of the violation of the normal ogive model.
- (b) Homogeneity of item difficulty parameters and biserial correlations, i.e., the effect of the violation of the ETEM assumption.

Obviously it is impossible to investigate the sampling distributions of reliability estimates under all possible combinations of the above factors and all possible sets of parameters by computer simulation techniques. In this chapter, to conserve the overall computer time, the experiments and investigations are limited to only three distributions for $\{f_i\}$ and $\{\epsilon_{ij}\}$, namely uniform (U1), normal (N0), and exponential (EX); four sets of difficulty parameters, two of which are non-homogeneous, and six sets of biserial correlations, three sets of which are non-homogeneous. The parameter sets used for the experiments are given in Tables 6.1 and 6.2

TABLE 6.1

Item Difficulty Parameters

Nota-	Homoge-		Item Number									Mean Var.	
tion	neity	1	2	3	4	5	6	7	8	9			
DI	Homo.	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.0	
D2	Non-Homo.	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	0.5	0.0667	
D3	Homo.	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	
D4	Non-Homo.	0.5	0.55	0.6	0.65	0.7	0.75	0.8	0.85	0.9	0.7	0.0167	

TABLE 6.2

Item Biserial Correlations

Nota-	Homoge-		Item Number									
tion	neity	1	2	3	4	5	6	7	8	9	Mean	Var.
Bì	Homo.	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0
B2	Non-Homo.	0.5	0.55	0.6	0.65	0.7	0.75	0.8	0.85	0.9	0.7	0.0167
В3	Homo.	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.0
В4	Non-Homo.	0.4	0.45	0.5	0.55	0.6	0.65	0.7	0.75	0.8	0.6	0.0167
B5	Homo.	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.0
В6	Non-Homo.	0.2	0.25	0.3	0.35	0.4	0.45	0.5	0.55	0.6	0.4	0.0167

With these distribution-parameter combinations, altogether 216 experiments $(3 \times 3 \times 4 \times 6)$ are possible. However, previous results indicated that the error distribution has little effect on the distribution of reliability estimates, and the same tendency may be expected for the binary item cases. Since this was the case, as will be seen in the following section, only the first step of the investigation will involve the case of non-normal error distributions. Thus the total number of experiments run were 96, resulting in a saving of computer time.

6.2 The Effects of Non-Normal Error Distribution and Non-Homogeneous Item Difficulty Parameters

In order to separate possible effects of non-normal latent score distribution and non-homogeneous biserial correlations such as B2, B4, and B6, from those of non-homogeneous item difficulty parameters or non-normal errors, which are of major interest in this section, three homogeneous biserial correlation sets B1, B3, and B5, normal distribution of latent variables, four sets of difficulty parameters, three types

of error distributions are used, i.e., altogether 36 $(3\times4\times3)$ experiments with N = 1000, I = 30 and J = 9 are performed.

Table 6.3 presents population parameters calculated from the formulas given in Chapter Three and the results obtained from the parallel form method, with sample size 30030. Comparisons of data in Table 6.3 indicate:

- (a) Calculated test parameters based on formulas given in Chapter Three agree reasonably well with the results obtained by computer simulation, thus partially validating the computer simulation method. For example, experiment 2 was performed with normal error score distribution, and satisfies the normal ogive model. It gives the test score mean, variance, reliability, and KR20 as 4.491, 8.094, 0.813, and 0.812, while the theoretical values based on the normal ogive model are 4.5, 8.118, 0.813, and 0.813 respectively.
- (b) For normal latent score distributions, the observed test score means given in column (5) seem to depend only on the average of the item difficulty parameters as expected, and are affected neither by non-homogeneous difficulty parameters nor non-normal error score distributions. For example, the values of experiments 1-6 inclusive in column (5) are almost identical to theoretical value 4.5, although experiments 1, 3, 4, 6 have non-normal error score distributions, and experiments 4, 5, and 6 have non-homogeneous difficulty parameters.
- (c) The non-homogeneous difficulty parameter sets, D2 and D4, (e.g., experiments 4, 5, 6, and 10, 11, 12) result in lower test score variance, reliability, and KR20 when compared with the same average level of difficulty, but homogeneous, namely D1, and D3

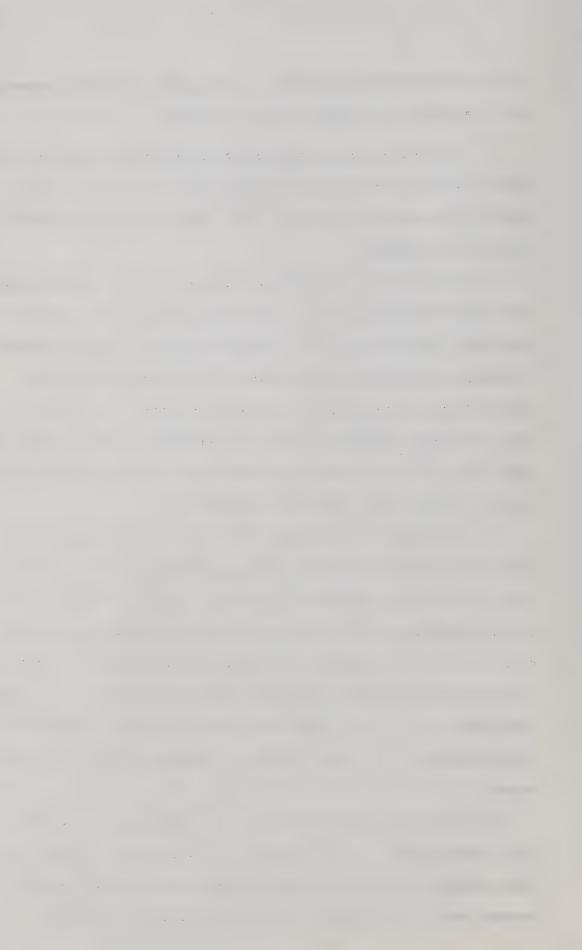


TABLE 6.3

Comparisons of Calculated Test Parameters Under the Normal Ogive Model
With Empirical Values Based on the Parallel Form Method, Normal
Latent Scores, and Homogeneous Biserial Correlations,
NI = 30030, J = 9

		1		Theoretical (N.O.)				Observed by P.F.M.				
Exp.	Err. Dis.	Bis.	Dif.	Mean	Var.	Rel.	KR20	Mean	Var.	Re1.	KR20	
NO.	015.			(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	
01	Ul	B1	DI	4.5	8.118	0.813	0.813	4.494	-8.044	0.811	0.810	
02	NO	Bì	DI	4.5	8.118	0.813	0.813	4.431	8.094	0.813	0.812	
03	EX	B1	DI	4.5	8.118	0.813	0.813	4.484	8.103	0.812	0.813	
04	Ul	B1	D2	4.5	4.979	0.769	0.752	4.496	4.941	0.768	0.750	
05	NO	Bl	D2	4.5	4.979	0.769	0.752	4.495	5.012	0.772	0.754	
06	EX	Bl	D2	4.5	4.979	0.769	0.752	4.506	4.968	0.768	0.751	
07	Ul	B1	D3	6.3	6.589	0.802	0.802	6.289	6.493	0.802	0.802	
08	NO	Bl	D3	6.3	6.589	0.802	0.802	6.299	6.621	0.804	0.804	
09	EX	B1	D3	6.3	6.589	0.802	0.802	6.281	6.622	0.803	0.803	
10	UI	B1	D4	6.3	5.671	0.788	0.780	6.269	5.714	0.789	0.780	
11	NO	B1 .	D4	6.3	5.671	C.788	0.780	6.296	5.632	0.785	0.777	
12	EX	Bì	D4	6.3	5.671	0.788	0.780	6.283	5.689	0.787	0.780	
13	וט	В3	DI	4.5	6.470	0.734	0.734	4.514	6.447	0.732	0.732	
14	NO	В3	DI	4.5	6.470	0.734	0.734	4.498	6.460	0.733	0.733	
15	EX	В3	DI	4.5	6.470	0.734	0.734	4.494	6.487	0.735	0.735	
16	Ul	83	D2	4.5	4.092	0.684	0.671	4.480	4.129	0.687	0.675	
17	NO	В3	D2	4.5	4.092	0.684	0.671	4.487	4.053	0.678	0.675	
18	EX	В3	D2	4.5	4.092	0.684	0.671	4.499	4.079	0.681	0.670	
19	Ul	В3	D3	6.3	5.230	0.718	0.718	6.286	5.259	0.719	0.719	
20	NO	В3	D3	6.3	5.230	0.718	0.718	6.276	5.215	0.715	0.715	
21	EX	В3	D3	6.3	5.230	0.718	0.718	6.267	5.276	0.719	0.719	
22	UI	В3	D4	6.3	4.559	0.702	0.696	6.298	4.573	0.703	0.697	
23	NO	В3	04	6.3	4.559	0.702	0.696	6.295	4.546	0.701	0.694	
24	EX	83	D4	6.3	4.559	0.702	0.696	6.283	4.557	0.700	0.694	
25	U1	85	DI	4.5	4.091	0.506	0.506	4.483	4.063	0.502	0.502	
26	NO	85	DI	4.5	4.091	0.506	0.506	4.498	4.104	0.509	0.508	
27	EX	B5	DI	4.5	4.091	0.506	0.506	4.500	4.141	0.513	0.514	
28	UI	B5	D2	4.5	2.735	0.452	0.446	4.497	2.696	0.442	0.437	
29	NO	B5	D2	4.5	2.735	0.452	0.446	4.495	2.727	0.453	0.450	
30	EX	B5	D2	4.5	2.735	0.452	0.446	4.490	2.776	0.461	0.455	
31	UI	B5	D3	6.3	3.317	0.484	0.484	6.304	3.347	0.490	0.490	
32	NO	B5	D3	6.3	3.317	0.484	0.484	6.295	3.243	0.469	0.469	
33	EX	B5	D3	6.3	3.317	0.484	0.484	6.292	3.344	0.486	0.488	
34	υı	B5	D4	6.3	2.956	0.466	0.463	6.297	2.959	0.465	0.461	
35	NO	85	D4	6.3	2.956	0.466	0.463	6.292	2.980	0.469	0.466	
36	EX	B5	D4	6.3	2.956	0.466	0.463	6.289	2.955	0.467	0.462	



respectively (e.g., experiments 1, 2, 3, and 7, 8, 9). For non-homogeneous difficulty, i.e., D2 and D4, the KR20 coefficients are lower than the reliability as expected since the ETEM assumption is not satisfied. For example, experiment 12, with non-homogeneous difficulty set of D4, gives reliability and KR20 as 0.787 and 0.780 respectively.

- (d) For homogeneous item difficulty, the higher the item difficulty is above the ideal 0.5 level, the lower the test variance, reliability and KR20. The same trends are observed for difficulty lower than 0.5 level, though the results are not reported in this paper since almost exactly the same results as high difficulty cases are obtained for lower difficulty cases except for test means, i.e., the test parameters. except for the test means, are highest when the item difficulty parameters are all equal to 0.5 which is a well-known fact in test theory. For example, experiment 1 has homogeneous difficulty of 0.5 for all items and gives variance and reliability as 8.044 and 0.811 respectively, while experiment 7, which is comparable to experiment 1 except the higher difficulty of 0.7, gives 6.493, and 0.802 respectively. However, this conclusion would not apply in general to the non-homogeneous item difficulty cases, i.e., the non-homogeneous item difficulty effects interact with the effects of item difficulty level, and the results are not predictable, as it can be seen when the results of experiments 4. 5, and 6 are compared with those of experiments 10, 11, and 12.
- (e) The non-normal distributions of error scores have very little effect on the test parameters. For example, experiment 12, which has an exponential error distribution, gives parameter values as 6.283, 5.689, 0.787, and 0.780 which can be compared reasonably well with

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theoretical values given in columns (1)-(4) inclusive, namely 6.3, 5.671, 0.788, and 0.780 respectively. Alternatively, they can also be compared reasonably well with the corresponding values of experiment 11 which has a normal error distribution, namely 6.296, 5.632, 0.785, and 0.777.

Table 6.4 gives the means and standard error of reliability estimates over N = 1000 trials and compares them with theoretical values which can be obtained from continuous part scores under the ANOVA model and normal distributional theory, i.e., treating binary test scores $\{x_{i,j}\}$ as if they were continuous part scores as in the previous chapter. From the table, it is noted that the observed means of reliability estimates given in column (2), which is based on estimation formula (2.13), compares fairly well with the theoretical values given in column (4) based on (5.1)-(a), the largest difference being only 0.018 (experiment 32) which is probably too small to be meaningful in test theory. The standard error obtained from formula (5.3) or (5.1)-(b), given in columns (5) and (6), also predict the observed standard errors given in column (3) reasonably well, although formula (5.3) seems to consistently underestimate the standard errors for lower reliability cases, namely the case of biserial correlation set B5. In general, formula (5.1)-(b) seems quite satisfactory, the largest difference between the theoretical and observed values being only 0.0111 (experiment 28). The sum of squares from the observed standard errors are 0.00101 and 0.00956 for formulas (5.1)-(b) and (5.3) respectively, suggesting the superiority of formulas (5.1)-(b) to (5.3). No attempts are made to use formula (5.10) since neither kurtosis formulas of test

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TABLE 6.4

Comparisons of Observed Means and Standard Errors of Reliability Estimates Under Normal Latent Scores, Homogeneous Biserial Correlations With the Values Obtainable From ANOVA Model and Normal Theory, $N = 1000, \quad I = 30, \quad J = 9$

Exp.	Err.	Bis.	Dif.	Rel.*	Observ	ed β	E(\$) by	Expecte	d S.E. by
No.	Dis.	DIS.	DII.		Mean	S.E.	(5.1)-(a)	(5.3)	(5.1)-(b)
				(1)	(2)	(3)	(4)	(5)	(6)
01	UI	B1	DI	0.811	0.800	0.0591	0.797	0.0626	0.0608
02	NO	B1	DI	0.813	0.802	0.0600	0.799	0.0618	0.0600
03	EX	B1	DI	0.812	0.804	0.0561	0.799	0.0621	0.0602
04	U1	Bl	D2	0.768	0.736	0.0714	0.751	0.0749	0.0745
05	NO	B1	D2	0.769	0.742	0.0667	0.752	0.0745	0.0740
06	EX	B1	D2	0.768	0.738	0.0685	0.751	0.0748	0.0744
07	Ul	B1	D3	0.802	0.787	0.0688	0.787	0.0653	0.0637
08	NO	81	03	0.802	0.789	0.0708	0.788	0.0651	0.0635
09	EX	B1	D3	0.803	0.789	0.0693	0.788	0.0649	0.0633
10	Ul	B1	D4	0.789	0.765	0.0737	0.773	0.0689	0.0677
11	NO	- B1	D4	0.788	0.760	0.0770	0.772	0.0693	0.0682
12	EX	B1	D4	0.787	0.764	0.0786	0.771	0.0695	0.0683
13	Ul	B3	DI	0.732	0.717	0.0821	0.712	0.0847	0.0859
14	NO	B3	DI	0.734	0.718	0.0826	0.714	0.0843	0.0855
15	EX	B3	Dl	0.735	0.722	0.0793	0.715	0.0840	0.0851
16	Ul	83	D2	0.687	0.656	0.0947	0.664	0.0964	0.1004
17	NO	B3	D2	0.684	0.646	0.1035	0.660	0.0972	0.1015
18	EX	В3	D2	0.681	0.650	0.1024	0.657	0.0979	0.1024
19	Ul	B3	D3	0.719	0.701	0.0932	0.698	0.0881	0.0901
20	NO	B3	D3	0.718	0.694	0.0986	0.698	0.0883	0.0904
21	EX	83	D3	0.719	0.700	0.0917	0.699	0.0881	0.0901
22	Ul	B3	D4	0.703	0.676	0.0970	0.681	0.0923	0.0953
23	NO	В3	D4	0.702	0.672	0.0995	0.680	0.0927	0.0957
24	EX	B3	D4	0.700	0.673	0.0959	0.677	0.0932	0.0964
25	U1	B5	DI	0.502	0.469	0.1585	0.465	0.1367	0.1600
26	NO	B5	DI	0.506	0.474	0.1619	0.470	0.1358	0.1585
27	EX	85	DI	0.513	0.482	0.1561	0.477	0.1345	0.1563
28	U1	B5	D2	0.442	0.401	0.1682	0.400	0.1470	0.1793
29	NO	B5	D2	0.452	0.407	0.1807	0.411	0.1453	0.1759
30	EX	B5	D2	0.461	0.415	0.1733	0.421	0.1438	0.1731
31	UI	B5	D3	0.490	0.452	0.1636	0.453	0.1387	0.1636
32	NO	B5	D3	0.484	0.428	0.1739	0.446	0.1398	0.1656
33	EX	B5	D3	0.486	0.452	0.1614	0.448	0.1394	0.1650
34	UI	85	D4	0.465	0.425	0.1719	0.425	0.1431	0.1718
35	NO	85	D4	0.466	0.428	0.1776	0.427	0.1429	0.1713
36	EX	B5	D4	0.467	0.425	0.1615	0.427	0.1428	0.1711

^{*}Theoretical value if error scores are normal, otherwise the value was obtained by the parallel form method.

(5.1) (a)
$$E(\beta) = 1 - (1-\rho) \frac{1-1}{1-3}$$
 (b) $Var(\beta) = (1-\rho)^2 \frac{2(1-1)(y+1-3)}{(y-1)(1-3)^2(1-5)}$

(5.3)
$$\operatorname{Var}(\beta) = \frac{(1-\rho^2)^2}{1}$$



score for binary item test nor any numerical means to evaluate the parameter are available at present.

Table 6.5 indicates the shapes of the lower and upper portions of the distributions of reliability estimates by giving the lower and upper 5% critical points of the distributions in columns (2) and (3), and by comparing them with those results obtainable theoretically from (2.17), given in columns (4) and (5). The results, in general, suggest that the theoretical values are very close to the observed values except for the upper tail portions for some experiments with high or medium reliability, i.e., with Bl and B2, and non-homogeneous difficulty set D2, namely experiments 4, 5, 6, 16, 17, and 18. For those experiments, the distributions are systematically shifted toward lower reliability primarily due to the fact that KR20 is substantially lower than reliability, because of extreme non-homogeneity of item difficulty parameter set D2. This is illustrated in Figure 6.1. Consequently the real Type one errors of the F-test for upper tails are much smaller than the nominal 5% level, some dropping as low as 1.1% level [column (7) of experiment 4]. The effect of non-homogeneous item difficulty parameters on the real significance level diminishes as the variation of item difficulty parameters decrease, as shown by experiments 10, 11, 12, 22, 23, and 24. The effect of item difficulty also diminishes with lower reliability level, and no meaningful differences are observed for low reliability cases illustrated by experiments 25-36 inclusive.

From the above observations, the following conclusions are tentatively made.

TABLE 6.5

Comparisons of Observed Lower and Upper 5% Critical Points Under Normal Latent Scores and Homogeneous Biserial Correlations With the Values
Obtainable From the ANOVA Model and Normal Theory, and Real
Type One Error of F-Test When Nominal Value is Fixed to
the 5% Level, N = 1000, I = 30, J = 9

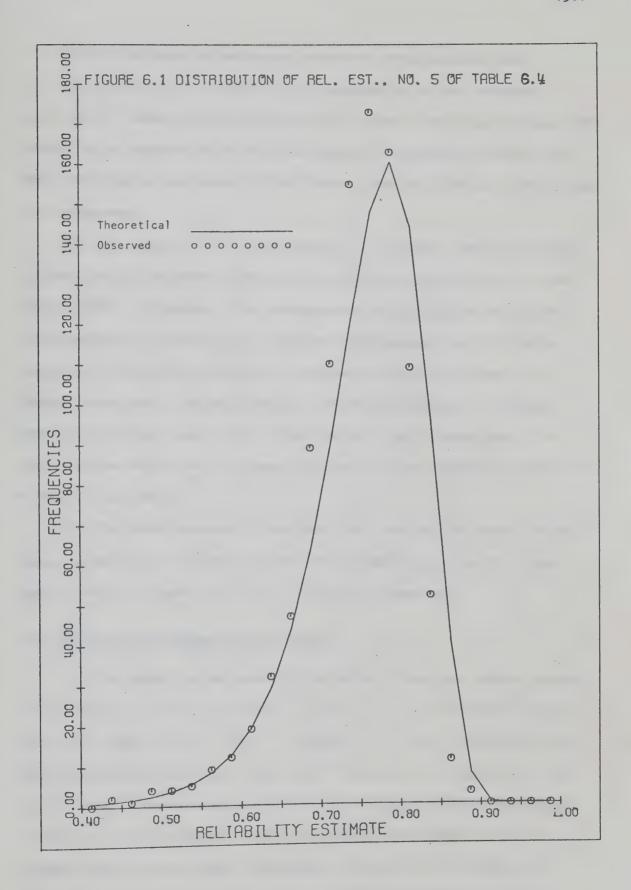
Exp. No.	Err. Dis.	Bis.	Dif.	Rel. 1	Observe Lower (2)	d C.P. ² Upper (3)	Theoret Lower (4)	ical C.P. ³ Upper (5)	Real Sig Lower (6)	(0/0) Upper
01 02 03 04 05 06 07 08 09 10	UI NO EX	B1 B1 B1 B1 B1 B1 B1 B1 B1	D1 D1 D1 D2 D2 D2 D2 D3 D3 D3 D4 D4	0.811 0.813 0.812 0.768 0.769 0.768 0.802 0.802 0.803 0.789 0.788	0.693 0.698 0.697 0.604 0.614 0.605 0.655 0.655 0.665 9.629 0.622	0.877 0.882 0.878 0.828 0.831 0.825 0.877 0.879 0.877 0.857	0.684 0.688 0.687 0.612 0.615 0.613 0.669 0.670 0.670 0.648	0.875 0.877 0.876 0.847 0.848 0.847 0.869 0.870 0.870 0.861 0.860	4.30 3.80 3.90 5.60 5.20 5.70 6.60 6.70 5.50 7.30 6.40 6.70	5.60 7.40 5.70 1.10 1.50 1.60 8.00 6.80 7.00 4.00 4.90 4.60
13 14 15 16 17 18 19 20 21 22 23 24	U1 NO EX U1 NO EX U1 NO EX U1 NO EX U1 NO EX	B3 B3 B3 B3 B3 B3 B3 B3 B3 B3 B3	D1 D1 D2 D2 D2 D3 D3 D3 D4 D4	0.732 0.734 0.735 0.687 0.684 0.681 0.719 0.718 0.719 0.703 0.702	0.560 0.572 0.574 0.487 0.464 0.465 0.528 0.505 0.531 0.507 0.484 0.482	0.830 0.828 0.827 0.783 0.777 0.776 0.821 0.825 0.823 0.797 0.801	0.553 0.555 0.557 0.478 0.472 0.467 0.531 0.530 0.531 0.504 0.502 0.498	0.823 0.824 0.825 0.794 0.791 0.790 0.815 0.814 0.815 0.804	4.70 3.90 3.70 4.30 4.90 5.10 5.40 6.20 5.10 4.90 6.40	6.60 5.60 5.60 3.40 3.00 2.40 6.00 7.90 6.70 5.60 4.20 4.60
25 26 27 28 29 30 31 32 33 34 35 36	UI NO EX	B5 B5 B5 B5 B5 B5 B5 B5 B5 B5	D1 D1 D2 D2 D2 D3 D3 D3 D4 D4	0.502 0.506 0.513 0.442 0.452 0.461 0.490 0.484 0.486 0.465 0.466	0.194 0.189 0.186 0.093 0.056 0.069 0.149 0.106 0.140 0.097 0.104 0.126	0.684 0.678 0.678 0.621 0.637 0.637 0.663 0.663 0.661 0.647 0.648 0.650	0.168 0.176 0.187 0.067 0.085 0.099 0.149 0.138 0.142 0.106 0.109 0.110	0.671 0.674 0.679 0.632 0.639 0.644 0.664 0.660 0.661 0.647 0.648	3.70 4.70 5.00 4.20 5.60 5.80 5.00 5.10 5.10 5.50 4.40	6.30 5.30 4.80 4.00 4.60 4.20 5.70 6.70 5.00 5.00 4.80 5.20

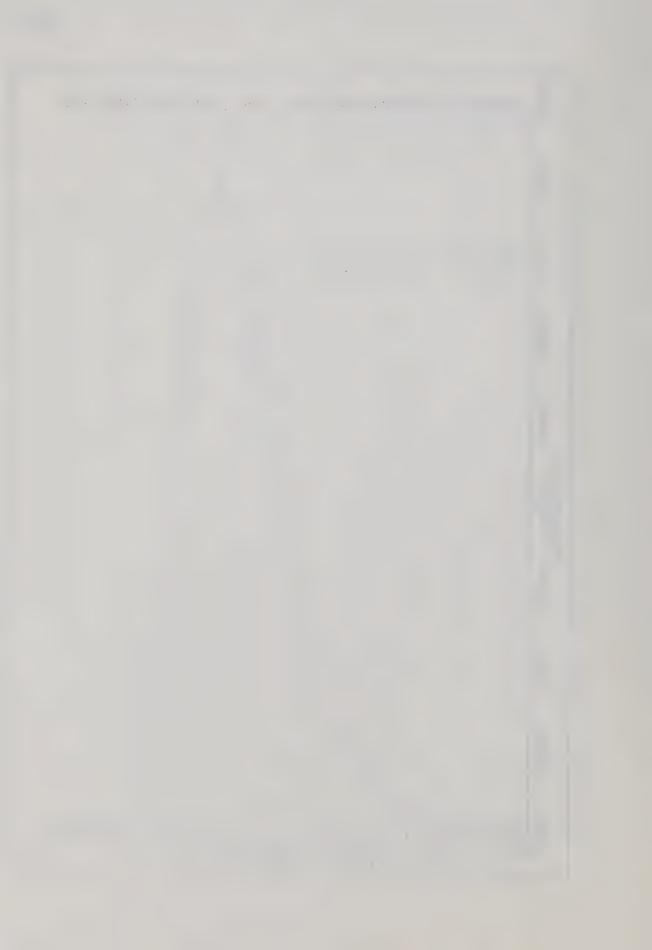
¹Theoretical value if error scores are normal, otherwise the value was obtained by the parallel form method.

 $^{^2}$ Observed lower and upper 5% critical points of the distribution of β .

 $^{^3}$ Theoretical lower and upper 5% critical points of the distribution of β under ANOVA and normal theory.







- (a) The effects of non-normal error distributions are small.
- (b) Formula (5.1), both for the expected value and standard error of $\hat{\rho}$, seems quite satisfactory for binary item cases although the assumption of continuity of observed scores is violated, provided that the latent scores are normally distributed, and the biserial correlations are homogeneous.
- (c) The item difficulty parameters $\{\pi_j\}$ affect the distribution systematically, contrary to the previous findings reported by Nitko and Feldt (1969). In general, the heterogeneity of difficulty shifts the distributions to the left, and the more heterogeneous the difficulty parameters, the more distortion is observed, and it also appears to cause a large shift leftward for high reliability cases. If F-tests based on (2.17) are used with a fixed nominal significance level, the real Type one errors for the upper tail portion are affected by the item difficulty parameters.
- (d) The distributions of the lower tail portion for high or middle range reliability, or both tails for low reliability are quite stable against the heterogeneity of item difficulty parameters.

6.3 Effects of Non-Normal Latent Scores

The normal ogive model for the binary item test scores assumes the existence of latent variables or scores $\{f_i\}$ distributed independently and identically as N(0,1). However, it is not conceivable that these assumptions are always satisfied. Therefore, the effects of nonnormal latent distributions are one of the important factors which must be examined rather closely. For the continuous part score cases, it is known that the non-normal true scores affect the distribution of reliability estimates significantly, and inflate or deflate the real

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Type one errors for the F-test. Thus it must be determined whether the same is true for the binary item test cases when the latent scores are not normal. Because it is known, from the experiments of the previous section, that the effects of non-normal errors are small, and to save computer time, experiments were performed using only normal error scores.

Using two kinds of non-normal latent score distributions, namely uniform (UI) and exponential (EX), four types of item difficulty sets and three kinds of homogeneous biserial correlation sets were selected. A total of 24 ($2 \times 4 \times 3$) additional experiments were performed with N = 1000, I = 30, and J = 9. The results of these 24 experiments are summarized in Tables 6.6, 6.7, and 6.8, together with the results of 12 experiments of the previous section which uses normal latent and error scores, for the purposes of comparisons.

As in the previous section, the population parameters were first examined to determine the effects of non-normality of latent scores. From Table 6.6, it is clearly observed that the test means are almost identical for both methods, namely by theoretical calculations under the normal ogive model given in column (1) and by the parallel form method given in column (5), except for the exponential distributions which have non-zero skewness. Using the exponential distribution, the means are in general lower than the theoretical values suggesting the effects of skewness, since, unlike the variance, the means are in general more sensitive to non-zero skewness.

The effects of non-normal latent scores can be seen rather clearly when the observed variance, reliability and KR20, given in columns (6), (7), and (8), are examined. The values of variance,

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TABLE 6.6

Comparisons of Calculated Test Parameters Under the Normal Ogive Model With Empirical Values Based on the Parallel Form Method, Normal Error Scores, Homogeneous Biserial Correlations, NI = 30030, J = 9

Exp.	Tr.	Bis	Dif.			cal (N.O.)	0Ь	served by			
No.	Dis.	013		Mea n (1)	Var. (2)	Rel. (3)	KR20 (4)	Mean (5)	Var. (6)	Rel. (7)	(8)	
01	U1 NO	B1 B1	D1 D1	4.5 4.5	8.118 8.118	0.813	0.813	4.504 4.491	9.034 8.094	0.845	0.845	
03	EX	B1	DI	4.5	8.118	0.813	0.813	4.156	6.997	0.766	0.765	
04	UI	Bl	D2	4.5	4.979	0.769	0.752	4.488	5.342	0.788	0.772	
05	NO	B1	D2	4.5	4.979	0.769	0.752	4.495	5.012	0.772	0.754	
06	EX	В1	D2	4.5	4.979	0.769	0.752	4.348	4.247	0.720	0.702	
07	UI	B1	03	6.3	6.589	0.802	0.802	6.235	7.081	0.820	0.821	
80	NO	B1	D3	6.3	6.589	0.802	0.802	6.299	6.621	0.804	0.804	
09	EX	B1	D3	6.3	6.589	0.802 0.788	0.802	6.209 6.266	4.589 5.987	0.653	0.653	
10	U1 NO	B1 B1	D4	6.3	5.671 5.671	0.788	0.780	6.296	5.632	0.785	0.777	
12	EX	BI	D4	6.3	5.671	0.788	0.780	6.224	3.957	0.648	0.636	
13	U1	B3	DI	4.5	6.470	0.734	0.734	4.498	7.025	0.764	0.765	
14	NO	В3	DI	4.5	6.470	0.734	0.734	4.498	6.460	0.733	0.733	
15	EX	В3	DI	4.5	6.470	0.734	0.734	4.299	5.610	0.675	0.675	
16	Ul	В3	D2	4.5	4.092	0.684	0.671	4.477 4.487	4.298 4.053	0.701 0.678	0.690	
17	NO EX	B3 B3	D2 D2	4.5 4.5	4.092 4.092	0.684 0.684	0.671	4.406	3.653	0.638	0.626	
18 19	U1	B3	D3	6.3	5.230	0.718	0.718	6.232	5.568	0.738	0.738	
20	NO	B3	D3	6.3	5.230	0.718	0.718	6.276	5.215	0.715	0.715	
21	EX	B3	D3	6.3	5.230	0.718	0.718	6.228	3.822	0.561	0.560	
22	UI	В3	D4	6.3	4.559	0.702	0.696	6.268	4.792	0.701	0.713	
23	NO	В3	D4	6.3	4.559	0.702	0.696	6.295	4.546	0.701	0.694	
24	EX	В3	D4	6.3	4.559	0.702	0.696	6.250	3.397	0.559	0.551	
25	UΊ	85	DI	4.5	4.091	0.506	0.506	4.512	4.199	0.522	0.522	
26	NO	B5	DI	4.5	4.091	0.506	0.506	4.451	4.104 3.834	0.509	0.508	
27	EX	B5	D1	4.5	4.091	0.506	0.506	4.451 4.496	2.767	0.460	0.455	
28	U1	B5	D2	4.5 4.5	2.735 2.735	0.452 0.452	0.446	4.495	2.747	0.453	0.450	
29	NO F	B5 B5	D2 D2	4.5	2.735	0.452	0.446	4.458	2.613	0.422	0.418	
30 31	EX	B5	D3	6.3	3.317	0.484	0.484	6.279	3.384	0.492	0.494	
32	NO	B5	D3	6.3	3.317	0.484	0.484	6.295	3.243	0.469	0.469	
33	EX	B5	D3	6.3	3.317	0.484	0.484	6.272	2.828	0.366	0.369	
34	UI	B5	D4	6.3	2.956	0.466	0.463	6.276	2.990	0.474	0.468	
35	NO	B5	D4	6.3	2.956	0.466	0.463	6.292	2.980 2.552	0.469	0.466	
36	EX	B5	D4	6.3	2.956	0.466	0.463	6.279	2.552	0.303	0.559	



reliability and KR20 under uniform distributions are always higher than the corresponding values under normal distributions, while the values under exponential distributions are lower than the values under normal distributions. Thus the normal ogive model gives lower values for the uniform distribution cases than the real values and higher values for the exponential distribution. For example, with biserial correlation and difficulty parameters fixed to set Bl and D2, the theoretical values under the normal ogive model are 4.979, 0.769, and 0.752 for variance, reliability and KR20 respectively (experiment 5). The parallel form method under normal distribution gives 5.012, 0.772, and 0.754, closely approximating the theoretical values as expected. However, for uniform latent scores (experiment 4), the corresponding values are 5.342. 0.788, and 0.772, which are much higher than theoretical [given in columns (2), (3), and (4) of experiment 4] or observed values under normal distribution of latent scores [given in columns (6), (7), and (8) of experiment 5]. On the other hand, for exponential distributions (experiment 6), the observed values, i.e., 4.247, 0.720, and 0.702, are much less than the theoretical or observed values under normal distribution.

Therefore it may be concluded that the reliability parameters to be used for equation (2.17) must be ρ^* , the value obtained by the parallel form method, rather than ρ for non-normal latent score distribution cases, since these values are closer to the actual values than the theoretical values obtained under the normal distribution assumption of latent scores.

Table 6.7 presents the results for observed means and standard errors of reliability estimates using $\,N\,=\,1000\,$, and compares them The second of th

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TABLE 6.7

Comparisons of Observed Means and Standard Errors of Reliability Estimates Under Normal Errors and Homogeneous Biserial Correlations With the Values Obtainable From ANOVA Model and Normal Theory, $N = 1000, \quad I = 30, \quad J = 9$

Exp. No.	Tr. Dis.	Bis.	Dif.	Rel.*	Observ Mean	ed β S.E.	E(β) by (5.1)-(a)	Expected S (5.3)	(5.1)-(b)
				(1)	(2)	(3)	(4)	(5)	(6)
01	Ul	Bl	DI	0.845	0.838	0.0469	0.833	0.0522	0.0498
02	NO	B1	DI	0.813	0.802	0.0600	0.799	0.0618	0.0600
03	EX	B1	D1	0.766	0.751	0.0783	0.748	0.0755	0.0752
04	UI	B1	D2	0.788	0,762	0.0584	0.772	0.0693	0.0682
05	NO -	Bl	D2	0.769	0.742	0.0667	0.752	0.0745	0.0740
06	EX	B1	D2	0.720	0.680	0.1024	0.699	0.0880	0.0900
07	Ul	Bl	D3	0.820	0.811	0.0562	0.807	0.0597	0.0577
08	NO	B1	D3	0.702	0.789	0.0708	0.788	0.0651	0.0635
09	EX	Bl	D3	0.653	0.636	0.1010	0.627	0.1048	0.1115
10	Ul	B1	D4	0.803	0.786	0.0553	0.789	0.0647	0.0631
11	NO	B1	D4	0.788	0.760	0.0770	0.772	0.0693	0.0682
12	EX	Bl	D4	0.648	0.620	0.0983	0.622	0.1059	0.1129
13	UI	B3	Dl	0.764	0.754	0.0667	0.746	0.0761	0.0758
14	NO	B3	DI	0.734	0.718	0.0826	0.714	0.0843	0.0855
15	EX	B3	Dì	0.675	0.654	0.1035	0,651	0.0993	0.1042
16	Ul	B3	D2	0.701	0.675	0.0850	0.679	0.0928	0.0959
17	NO	В3	D2	0.684	0.646	0.1035	0.660	0.0972	0.1015
18	EX	В3	D2	0.638	0.598	0.1261	0.611	0.1082	0.1161
19	Ul	В3	D3	0.738	0.723	0.0779	0.719	0.0831	0.0841
20	NO	В3	D3	0.718	0.694	0.0986	0.698	0.0883	0.0904
21	EX	В3	D3	0.561	0.537	0.1283	0.529	0.1250	0.1408
22	Ul	B3	D4	0.719	0.697	0.0854	0.698	0.0882	0.0902
23	NO	В3	D4	0.702	0.672	0.0995	0.680	0.0927	0.0957
24	EX	В3	D4	0.559	0.528	0.1263	0.526	0.1256	0.1416
25	Ul	B5	DI	0.522	0.494	0.1402	0.487	0.1327	0.1533
26	NO	B5	DI	0.506	0.474	0.1619	0.470	0.1358	0.1585
27	EX	B5	DI	0.464	0.429	0.1752	0.425	0.1432	0.1719
28	UI	B5	D2	0.460	0.419	0.1669	0.420	0.1440	0.1735
29	NO	B5	D2	0.452	0.407	0.1807	0.411	0.1453	0.1759
30	EX	B5	D2	0.422	0.374	0.1886	0.379	0.1501	0.1857
31	Ul	B5	D3	0.492	0.461	0.1544	0.455	0.1383	0.1629
32	NO	B5	D3	0.848	0.428	0.1739	0.446	0.1398	0.1656
33	EX	B5	D3	0.366	0.330	0.1883	0.320	0.1581	0.2034
34	Ul	B5	D4	0.474	0.437	0.1481	0.435	0.1416	0.1689
35	NO	B5	D4	0.466	0.428	0.1776	0.427	0.1429	0.1713
36	EX	B5	D4	0.636	0.322	0.1904	0.315	0.1586	0.2046

^{*}Theoretical value if true scores are normal, otherwise the value was obtained by the parallel method.

(5.1) (a)
$$E(\hat{\rho}) = 1 - (1-\rho) \frac{1-1}{1-3}$$
 (b) $Var(\hat{\rho}) = (1-\rho)^2 \frac{-2(1-1)(\nu+1-3)}{(1-1)(1-3)^2(1-5)}$

(5.3) Var
$$(\beta) = \frac{(1-\rho^2)^2}{1}$$

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with the calculated values based on formulas (5.1), and (5.3). It is noted that $E(\beta)$ of (5.1)-(a) given in column (4) predicts very well the observed means of reliability estimates given in column (2) regardless of the distributions of latent scores, the largest discrepancy being only 0.019 (experiment 6), suggesting robustness of the estimation formula (2.13) as far as point estimations are concerned. The observed standard error of estimation given in column (3) suggests that the uniform distributions of latent scores produces smaller standard errors while the exponential gives larger standard errors than under the normal distributions for high reliability cases. Formula (5.3) or (5.1)-(b) predicts the standard errors of reliability estimates reasonably well, though (5.1)-(b) seems better than (5.3).

Table 6.8 summarizes the shapes of the distributions of β at the tail portions by comparing lower and upper 5% critical points given in columns (2) and (3) with theoretical values given in columns (4) and (5). From the table, it may be concluded that the effects of item difficulty parameters as noted in the previous section can be generalized to non-normal latent score cases. On the other hand, from the observations of the real Type one errors, the effect of non-normal latent score distributions are not so obvious. The Type one errors are fluctuating substantially, but with no clear sign of systematic inflation or deflation of Type one errors due to non-normal distribution of latent scores, unlike the case of continuous part scores discussed in Chapter Five. This suggests robustness of the ANOVA model and normal distributional theory for the case of binary item tests.

From the above observations, the following conclusions were tentatively made.

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TABLE 6.8

Comparisons of Observed Lower and Upper 5% Critical Points Under Normal Error Scores and Homogeneous Biserial Correlations With the Values
Obtainable From ANOVA Model and Normal Theory, and Real Type
One Error of F-Test When Nominal Value is Fixed to the
5% Level, N = 1000, I = 30, J = 9

Exp.	Tr. Dis.	Bis.	Dif.	Rel.	Observe Lower	d C.P. ² Upper	Theoret Lower	ical C.P. ³ Upper	Real Sig Lower	(0/0) Upper
				(1)	(2)	(3)	(4)	(5)	(6)	(7)
01	Ul	B1	DI	0.845	0.749	0.901	0.741	0.898	3.80	6.30
02	NO	B1	Dì	0.813	0.698	0.882	0.688	0.877	3.80	7.40
03	EX	Bl	DI	0.766	0.611	0.851	0.609	0.846	4.60	6.70
04	Ul	B1	D2	0.788	0.654	0.835	0.645	0.860	3.80	1.50
05	NO	B1	D2	0.769	0.614	0.831	0.615	0.848	5.20	1.50
06	EX	Bl	D2	0.720	0.500	0.805	0.532	0.815	7.50	3.20
07	Ul	B1	D3	0.820	0.716	0.887	0.700	0.882	3.20	6.70
08	NO	B1	D3	0.802	0.650	0.879	0.670	0.870	6.70	6.80
09	EX	B1	D3	0.653	0.446	0.775	0.420	0.771	3.70	5.70
10	Ul	B1	D4	0.803	0.682	0.863	0.672	0.870	4.00	2.90
11	NO	B1	D4	0.788	0.622	0.857	0.645	0.860	6.40	4.90
12	EX	Bl	D4	0.648	0.222	0.749	0.413	0.768	3.20	2.10
13	U1	В3	Dl	0.764	0.631	0.844	0.605	0.844	3.00	5.10
14	NO	В3	DI	0.734	0.572	0.828	0.555	0.824	3.90	5.60
15	EX	В3	DI	0.675	0.450	0.790	0.458	0.786	5.40	5.50
16	Ul	B3	D2	0.701	0.528	0.786	0.501	0.803	3.60	1.90
17	NO	В3	D2	0.684	0.464	0.777	0.472	0.791	4.90	3.00
18	EX	B3	D2	0.638	0.366	0.754	0.396	0.761	7.20	4.00
19	U1	В3	D3	0.738	0.582	0.829	0.562	0.827	3.80	5.60
20	NO	В3	D3	0.718	0.505	0.825	0.530	0.814	6.20	7.90
21	EX	В3	D3	0.561	0.290	0.703	0.267	0.711	4.20	3.80
22	Ul	83	D4	0.719	0.530	0.806	0.531	0.815	5.10	3.00
23	NO	В3	D4	0.702	0.484	0.797	0.502	0.803	6.40	4.20
24	EX	В3	D4	0.559	0.305	0.697	0.263	0.709	2.90	3.60
25	UI	B5	Dl	0.522	0.243	0.683	0.203	0.685	3.60	4.70
26	NO	B5	DI	0.506	0.189	0.678	0.176	0.674	4.70	5.30
27	EX	B5	Dl	0.464	0.115	0.653	0.106	0.647	4.80	5.70
28	Ul	B5	D2	0.460	0.105	0.641	0.098	0.644	4.70	4.80
29	NO	B5	D2	0.452	0.056	0.637	0.085	0.639	5.60	4.60
30	EX	B5	D2	0.422	0.021	0.616	C.034	0.619	5.50	4.70
31	Ul	B5	D3	0.492	0.166	0.669	0.152	0.665	4.50	5.30
32	NO	B5	D3	0.484	0.106	0.663	0.138	0.660	5.20	6.70
33	EX	B5	D3	0.366	-0.024	0.580	0.058	0.582	3.90	4.90
34	Ul	B5	D4	0.474	0.179	0.643	0.121	0.653	3.00 5.50	4.00 4.80
35	NO	B5	D4	0.466	0.104	0.573	-0.064	0.580	3.20	4.00
36	EX	B5	D4	0.363	-0.002	0.5/3	-0.004	0.500	3.20	4.00

¹Theoretical values if true scores are normal, otherwise the values obtained by the parallel form method.

 $^{^{2}}$ Observed lower and upper 5% critical points of the distribution of β .

 $^{^3}$ Theoretical lower and upper 5% critical points of the distribution of β under ANOVA and normal theory.

- (a) The non-normal latent score distributions affect the test parameters such as variance, reliability and KR20, and with lesser degree the mean, if the distribution is skewed. The normal ogive model provides smaller values than the actual values of the variance, reliability and KR20 if the latent scores are distributed as uniform, and the opposite is true for exponential distribution.
- (b) Formulas (5.1) and (5.3) are quite robust against the violation of assumptions of normality for the binary item score cases.
- (c) The effects of item difficulty parameters are the same as observed in the previous section.
- (d) The non-normal latent scores do not systematically inflate or deflate real Type one errors for the F-test. The F-test seems quite robust against the violation of distributional assumptions, if difficulty parameters are homogeneous.

6.4 Effects of Non-Homogeneous Biserial Correlations

For the previous two sections, the biserial correlations were limited to homogeneous cases, namely Bl, B3, and B5. In this section, three non-homogeneous biserial correlation sets, B2, B4, and B6 are used to investigate the effects of such non-homogeneity. Since it is known that for the continuous part-test score cases the non-homogeneity of true score variance, which corresponds to the square of biserial correlation for the binary item case under the congeneric true score model, does not affect the sampling distribution of the reliability estimates if the non-homogeneity is moderate, and it is of interest to know whether the same conclusion can be made for the binary item cases.

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Employing three kinds of latent score distributions, U1, N0, and EX, and four sets of difficulty parameters, as in the previous section, and three sets of non-homogeneous biserial correlation sets, altogether $36 \ (3 \times 4 \times 3)$ additional experiments were performed with N = 1000, I = 30, and J = 9. The results are summarized in Tables 6.9, 6.10, and 6.11.

If the test parameters estimated by the parallel form method in Table 6.9 are compared with the corresponding entries of Table 6.6, the latter table using the same parameter distribution combinations as in this section except that the biserial correlations are not homogeneous, although the averages of the biserial correlations are the same, it is noted that the results of the two tables are almost identical. This suggests that the effects of non-homogeneous biserial correlations are small, even though the non-homogeneous biserial correlations do violate the ETEM assumptions, and consequently lower the KR20 relative to the reliability.

Although the biserial correlations are not homogeneous, almost the same conclusions may be made for Tables 6.10 and 6.11 as for Tables 6.7 and 6.8 respectively;

- (a) the means and standard errors of reliability estimates are almost identical in the two sets of the experiments,
- (b) the F-tests are quite robust against the violation of the ANOVA model and normal distribution theory for the binary item cases if difficulty parameters are homogeneous, and
- (c) the item difficulty parameters affect the distribution considerably, if they are not homogeneous, thus inflating or deflating real Type one errors for the F-tests.

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TABLE 6.9

Comparisons of Calculated Test Parameters Under the Normal Ogive Model With Empirical Values Based on the Parallel Form Method, Normal Error Scores, Non-Homogeneous Biserial Correlations, NI = 30030, J = 9

			•		Theoreti	cal (N.O		0	bserved b	y P.F.M.	
Exp.	Tr.	Bis.	Dif.	Mean	Var.	Rel.	KR20	Mean	Var.	Rel.	KR20
No.	Dis.			(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
01 02 03 04 05 06 07 08 09	UI NO EX UI NO EX UI NO EX UI	B2 B2 B2 B2 B2 B2 B2 B2 B2 B2	D1 D1 D2 D2 D2 D3 D3 D3 D4	4.5 4.5 4.5 4.5 4.5 4.5 6.3 6.3 6.3	8.160 8.160 8.160 5.009 5.009 6.634 6.634 6.634 5.470 5.470	0.820 0.820 0.820 0.777 0.777 0.777 0.810 0.810 0.810 0.775	0.815 0.815 0.815 0.754 0.754 0.754 0.804 0.804 0.767 0.767	4.520 4.504 4.147 4.441 4.507 4.443 6.181 6.290 6.211 6.226 6.290 6.343	9.131 8.127 7.130 5.459 4.984 3.924 7.257 6.632 4.723 5.758 5.552 3.472	0.853 0.819 0.779 0.796 0.776 0.696 0.831 0.809 0.672 0.783 0.778	0.848 0.814 0.773 0.777 0.754 0.674 0.825 0.804 0.667 0.778 0.772 0.585
12 13 14 15 16 17 18 19 20 21 22 23 24	EX U1 NO EX	B2 B4 B4 B4 B4 B4 B4 B4 B4	D1 D1 D1 D2 D2 D2 D3 D3 D3 D4 D4	6.3 4.5 4.5 4.5 4.5 6.3 6.3 6.3	5.470 6.474 6.474 4.109 4.109 4.109 5.241 5.241 5.241 4.373 4.373	0.775 0.739 0.739 0.739 0.690 0.690 0.725 0.725 0.725 0.682 0.682	0.767 0.734 0.734 0.673 0.673 0.673 0.719 0.719 0.719 0.677 0.677	4.503 4.500 4.254 4.462 4.495 4.446 6.226 6.310 6.221 6.280 6.287 6.305	7.109 6.462 5.684 4.302 4.099 3.342 5.600 5.244 3.854 4.446 4.365 3.065	0.775 0.740 0.688 0.705 0.691 0.579 0.746 0.725 0.570 0.685 0.682 0.506	0.769 0.733 0.682 0.689 0.674 0.584 0.740 0.720 0.564 0.681 0.675 0.499
25 26 27 28 29 30 31 32 33 34 35 36	U1 NO EX U1 NO EX U1 NO EX U1 NO EX	B6 B6 B6 B6 B6 B6 B6 B6 B6 B6	D1 D1 D2 D2 D2 D3 D3 D3 D4 D4	4.5 4.5 4.5 4.5 4.5 6.3 6.3 6.3	4.072 4.072 4.072 2.737 2.737 2.737 3.307 3.307 3.307 2.814 2.814 2.814	0.510 0.510 0.510 0.457 0.457 0.457 0.489 0.489 0.489 0.433 0.433	0.503 0.503 0.503 0.447 0.447 0.482 0.482 0.482 0.482 0.429 0.429	4.475 4.503 4.417 4.487 4.500 4.481 6.296 6.295 6.275 6.287 6.292 6.303	4.218 4.108 3.769 2.815 2.731 2.452 3.354 3.328 2.782 2.824 2.797 2.338	0.533 0.513 0.461 0.469 0.454 0.380 0.500 0.493 0.361 0.433 0.428 0.296	0.525 0.509 0.454 0.463 0.444 0.372 0.490 0.485 0.357 0.428 0.424 0.292



TABLE 6.10

Comparisons of Observed Means and Standard Errors of Reliability Estimates Under Normal Error Scores and Non-Homogeneous Biserial Correlations With the Values Obtainable From ANOVA Model and Normal Theory, N=1000, I=30, J=9

Exp.	Tr. Dis.	Bis.	Dif.	Rel.*	Observ		Ε(ρ̂) by		d S.E. by
NO.	DIS.		,		Mean	S.E.	(5.1)-(a)	(5.3)	(5.1)-(b)
				(1)	(2)	(3)	(4)	(5)	(6)
01	Ul	B2	D1	0.853	0.842	0.0436	0.842	0.0499	0.0473
02	NO	B2	Dl	0.813	0.805	0.0564	0.799	0.0618	0.0600
03	EX	B2	D1	0.779	0.760	0.0739	0.763	0.0716	0.0708
04	Ul	B2	D2	0.796	0.766	0.0596	.0.781	0.0668	0.0653
05	NO	B2	D2	0.769	0.740	0.0707	0.752	0.0745	0.0740
06	EX	B2	D2	0.696	0.654	0.0986	0.674	0.0941	0.0975
07	Ul	B2	D3	0.831	0.817	0.0505	0.819	0.0565	0.0542
08	NO	B2	D3	0.802	0.790	0.0676	0.788	0.0651	0.0635
09	EX	B2	D3	0.672	0.650	0.0988	0.647	0.1002	0.1053
10	Ul	B2	D4	0.783	0.763	0.0681	0.767	0.0705	0.0695
11	NO	B2	D4	0.788	0.752	0.0859	0.772	0.0693	0.0682
12	EX	B2	D4	0.593	0.561	0.1191	0.563	0.1183	0.1306
13	Ul	84	Dì	0.775	0.759	0.0630	0.759	0.0728	0.0721
14	NO	B4	DI	0.734	0.719	0.0839	0.714	0.0843	0.0855
15	EX	В4	Dl	0.688	0.659	0.1088	0.665	0.0962	0.1002
16	Ul	B4	D2	0.705	0.673	0.0841	0.684	0.0917	0.0945
17	NO	В4	D2	0.684	0.654	0.0998	0.660	0.0972	0.1015
18	EX	B4	D2	0.597	0.555	0.1348	0.567	0.1174	0.1293
19	U1	В4	D3	0.746	0.723	0.0838	0.727	0.0810	0.0816
20	NO	B4	D3	0.718	0.700	0.0951	0.698	0.0883	0.0904
21	EX	В4	D3	0.570	0.540	0.1278	0.539	0.1232	0.1379
22	Ul	В4	D4	0.685	0.662	0.0948	0.661	0.0970	0.1013
23	NO	B4	D4	0.702	0.647	0.1185	0.680	0.0927	0.0957
24	EX	B4	D4	0.506	0.470	0.1474	0.469	0.1358	0.1586
25	Ul	В6	DI	0.533	0.496	0.1448	0.498	0.1308	0.1500
26	NO	В6	Dl	0.506	0.476	0.1566	0.470	0.1358	0.1585
27	EX	В6	D1	0.461	0.414	0.1791	0.421	0.1438	0.1731
28	Ul	В6	D2	0.469	0.428	0.1578	0.430	0.1424	0.1704
29	NO	В6	D2	0.452	0.405	0.1729	0.411	0.1453	0.1759
30	EX	В6	D2	0.380	0.329	0.1963	0.334	0.1563	0.1991
31	Ul	B6	D3	0.500	0.458	0.1585	0.463	0.1370	0.1605
32	NO	В6	D3	0.484	0.448	0.1638	0.446	0.1398	0.1656
33	EX	B6	D3	0.361	0.314	0.1962	0.313	0.1588	0.2052
34	Ul	B6	D4	0.433	0.388	0.1736	0.391	0.1484	0.1821
35	NO	В6	D4	0.466	0.378	0.1901	0.427	0.1429	0.1713
36	EX	В6	D4	0.296	0.248	0.2106	0.244	0.1666	0.2259

^{*}Theoretical values if true scores are normal, otherwise the value was obtained by the parallel form method.

(5.1) (a)
$$E(\beta) = 1 - (1-\rho) \frac{1-1}{1-3}$$
 (b) $Var(\beta) = (1-\rho)^2 \frac{2(1-1)(\nu+1-3)}{(J-1)(1-3)^2(1-5)}$

(5.3)
$$\operatorname{Var}(\hat{\rho}) = \frac{(1-\rho^2)^2}{1}$$

TABLE 6.11

Comparisons of Observed Lower and Upper 5% Critical Points Under Normal Error Scores and Non-Homogeneous Biserial Correlations With the Values
Obtainable From the ANOVA Model and Normal Theory, and Real
Type One Error of F-Test When Nominal Value is Fixed to the 5% Level, N = 1000, I = 30, J = 9

Exp.	Tr. Dis.	Bis.	Dif.	Rel. 1	Observe Lower (2)	d C.P. ² Upper (3)	Theoret Lower (4)	ical C.P. ³ Upper	Real Sig	Upper
01 02 03 04 05 06	U1 NO EX U1 NO	B2 B2 B2 B2 B2 B2	D1 D1 D1 D2 D2	0.853 0.813 0.779 0.796 0.769	0.765 0.704 0.629 0.653 0.598	0.902 0.877 0.856 0.845 0.828	0.754 0.688 0.632 0.660 0.615	0.903 0.877 0.855 0.866 0.848	(6) 3.40 4.60 5.20 5.90 7.10	4.60 4.00 5.40 1.40 0.80
06 07 08 09 10 11	EX UI NO EX UI NO EX	B2 B2 B2 B2 B2 B2 B2 B2	D2 D3 D3 D3 D4 D4	0.696 0.831 0.802 0.672 0.783 0.788 0.593	0.462 0.733 0.670 0.465 0.629 0.592 0.345	0.778 0.884 0.877 0.780 0.858 0.856 0.722	0.493 0.718 0.670 0.452 0.638 0.645 0.321	0.800 0.889 0.870 0.784 0.857 0.860 0.732	6.90 3.20 6.70 4.20 6.10 7.70 4.00	1.40 3.70 6.00 4.20 5.10 5.90 3.30
13 14 15 16 17 18 19 20 21 22 23 24	UI NO EX UI NO EX UI NO EX UI	84 84 84 84 84 84 84 84 84	D1 D1 D2 D2 D2 D3 D3 D3 D4 D4	0.775 0.734 0.688 0.705 0.684 0.597 0.746 0.718 0.570 0.685 0.702	0.648 0.564 0.470 0.513 0.482 0.308 0.597 0.526 0.304 0.467 0.416 0.193	0.845 0.824 0.801 0.783 0.777 0.720 0.831 0.820 0.717 0.787 0.796 0.667	0.625 0.555 0.479 0.508 0.472 0.328 0.576 0.530 0.283 0.473 0.502 0.175	0.852 0.824 0.794 0.806 0.791 0.734 0.832 0.814 0.717 0.792 0.803 0.674	3.10 5.20 5.40 4.80 5.20 5.90 5.50 6.20 3.80 5.40 7.30 4.30	3.40 4.60 6.10 2.30 2.10 2.50 4.50 5.20 5.00 4.00 6.20 4.00
25 26 27 28 29 30 31 32 33 34 35	UI NO EX UI NO EX UI NO EX UI NO EX UI	B6 B6 B6 B6 B6 B6 B6 B6 B6 B6 B6	D1 D1 D2 D2 D2 D2 D3 D3 D3 D4 D4	0.533 0.506 0.461 0.469 0.452 0.380 0.500 0.484 0.361 0.433 0.466 0.296	0.220 0.174 0.052 0.129 0.085 -0.028 0.165 0.128 -0.056 0.063 0.026 -0.146	0.682 0.674 0.657 0.650 0.635 0.594 0.657 0.672 0.579 0.629 0.624	0.220 0.176 0.100 0.114 0.085 -0.036 0.165 0.138 -0.068 0.053 0.109	0.692 0.674 0.644 0.650 0.639 0.591 0.670 0.660 0.578 0.626 0.648	5.10 5.40 6.10 4.30 5.20 4.60 5.50 4.40 4.40 5.80 4.50	3.90 4.10 5.90 5.00 4.50 5.10 4.30 6.00 5.10 5.30 5.20 3.50

¹Theoretical values if true scores are normal, otherwise the values obtained by the parallel form method.

 $^{^2}$ Observed lower and upper 5% critical points of the distribution β .

 $^{^3}$ Theoretical lower and upper 5% critical points of the distribution of $\,\beta\,$ under ANOVA and normal theory.

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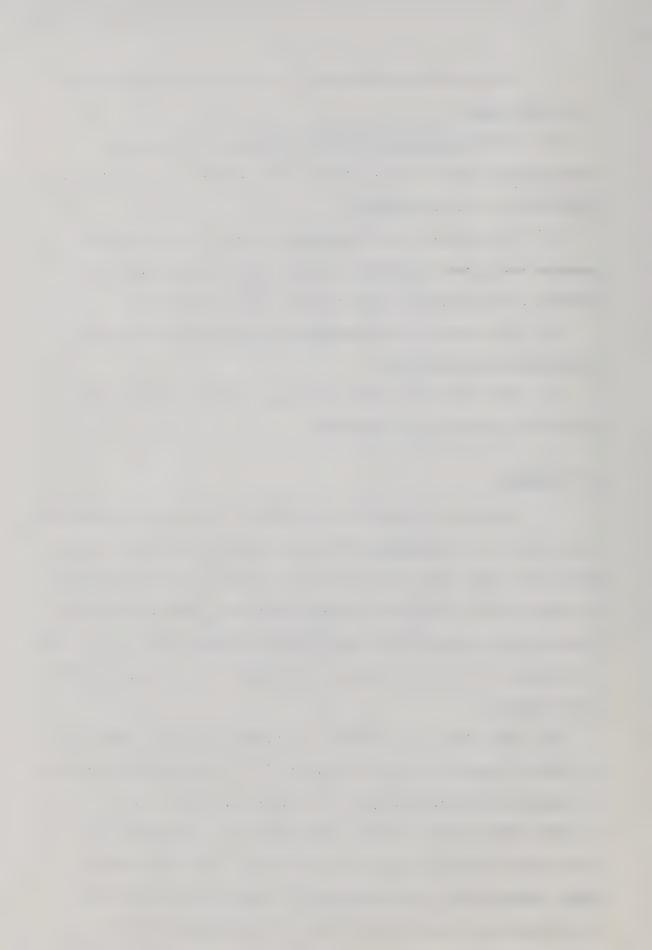
From the above observations, the following conclusions are tentatively made.

- (a) The non-homogeneous biserial correlation distorts the distribution slightly to the left for high reliability cases, but the differences are not substantial.
- (b) The effects of non-homogeneous biserial correlations on expected values and standard errors of reliability estimates are minimal, and formulas (5.1) and (5.3) are quite satisfactory.
- (c) The effects of non-homogeneous biserial correlations on test parameters are minimal.
- (d) The F-tests are robust for binary item test cases if the difficulty parameters are homogeneous.

6.5 Summary

In order to investigate the effects of non-normal latent and error scores, non-homogeneous difficulty parameters and biserial correlations on the sampling distribution of reliability estimates based on formula (2.13), altogether 96 experiments were performed by REL02 using various combinations of distribution parameter sets with N = 1000, I = 30, and J = 9. The findings in this chapter may be summarized as the following:

- (a) The effects of non-normal distribution of error scores $\{\epsilon_{ij}\}$ in terms of response strength variables $\{y_{ij}\}$ are negligible, as was the case for the continuous part score cases in Chapter Five.
- (b) The non-normal latent scores affect the population parameters such as variance, reliability and KR20. The normal ogive model underestimates these parameters for the uniform latent score distribution, and overestimates them for the exponential case.



- (c) Formulas (5.1) and (5.3) are quite satisfactory for binary item cases; formula (5.1)-(b) seems superior to (5.3) for the calculation of the standard error of reliability estimates.
- (d) The item difficulty parameters are the most important factor for the distribution of reliability estimates. They will affect the test score variance, reliability and KR20. The non-homogeneous difficulty sets give lower values for these parameters.
- (e) The item difficulty parameters systematically affect the distribution of reliability estimates. The non-homogeneous difficulty sets shift the distribution leftward.
- (f) The effect of non-homogeneous biserial correlations are negligible if the heterogeneity is moderate.
- (g) The F-test based on (2.17) is robust if any one of the following conditions is satisfied.
 - i) Relibability is low, i.e., ρ is close to zero.
 - (ii) Only lower portions of the sampling distribution of reliability estimates are used for the inference, namely the null hypothesis is directional, being bounded only by the lower end.
 - iii) The difficulty parameters are almost homogenous.
- (h) The difficulty parameter sets may deflate the real Type one errors if they are not homogeneous for inference which uses only upper tail of the sampling distribution.

CHAPTER SEVEN

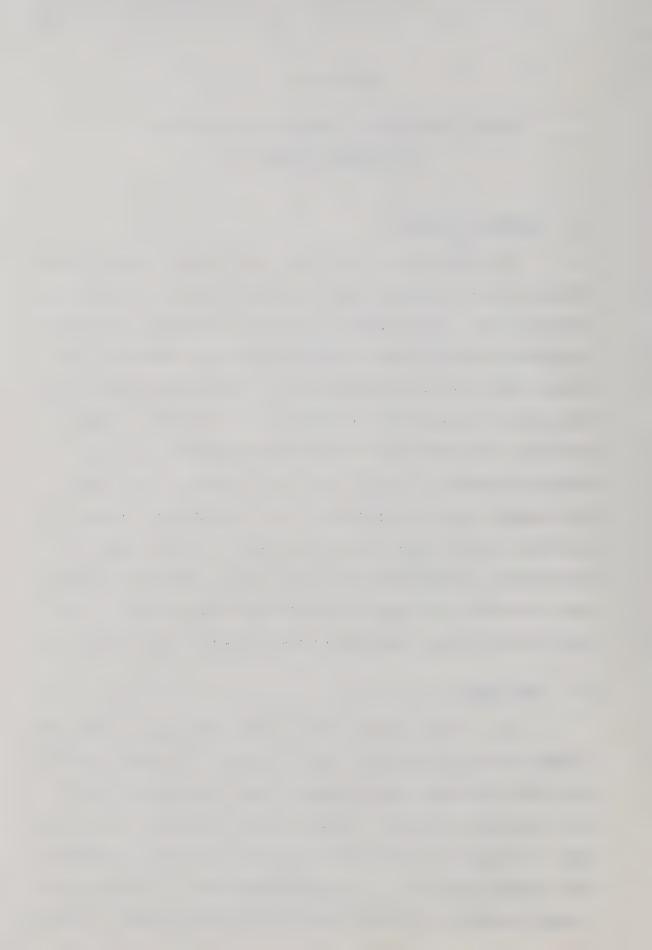
SUMMARY, IMPLICATIONS, EXAMPLES OF APPLICATION, AND RECOMMENDATIONS

7.1.0 Summary of Findings

The purpose of this study was (a) to review the more liberal concepts of test reliability theory in terms of models and assumptions underlying them, (b) to examine the sampling distribution of reliability estimates based on Alpha or KR20 formulas using these models with various combinations of the distribution of true and error scores, and (c) to compare the empirical distributions thus obtained by computer simulation under these model-distribution combinations with those obtainable theoretically under a mixed model ANOVA and normal theory Using computer simulated hypothetical test score matrices, a number of statistical sampling experiments were performed to obtain empirical distributions, and some analytical means were also employed to obtain a new formula for the standard error of reliability estimates. Findings in this study are summarized in the following three sections.

7.1.1 Test Models

(a) The most general model for the continuous part test score is found to be the multi-factor true score model. The model includes other more restrictive models as special cases. By imposing a uniffactor true score constraint, the model becomes a congeneric true score model. If homogeneity of true score variance is assumed, the congeneric model becomes essentially τ equivalent measurement. The latter model includes the ANOVA or essentially parallel measurement model as a special



case with the additional assumption of the homogeneity of error variances. The classical parallel test model is a special case of ANOVA model, namely the means of part test scores are all equal. The Alpha coefficient is equal to the reliability if, and only if the essentially τ equivalent measurements condition is satisfied, otherwise it is in general lower than the reliability. The sampling distribution of reliability estimates is known only for the case of the ANOVA model and normality assumptions of true and error scores.

(b) For the binary item test case, a similar model as the continuous case may be considered for the hypothetical 'response strength' variable. A mathematical model and distributional assumptions are required to associate the response strength variable to the observed item scores. Under the normal ogive model, the test parameters such as variance, reliability, and KR20 are amenable for calculation by means of numerical methods if the item parameters, such as biserial correlation and difficulty parameters, are specified. The essentially the equivalent measurement assumption is satisfied if and only if all biserial correlations and difficulty parameters are equal, i.e., all items are homogeneous; otherwise KR20 is lower than reliability. The sampling distribution of reliability estimates for binary item test is not yet known, except by approximation using the ANOVA model and normal theory.

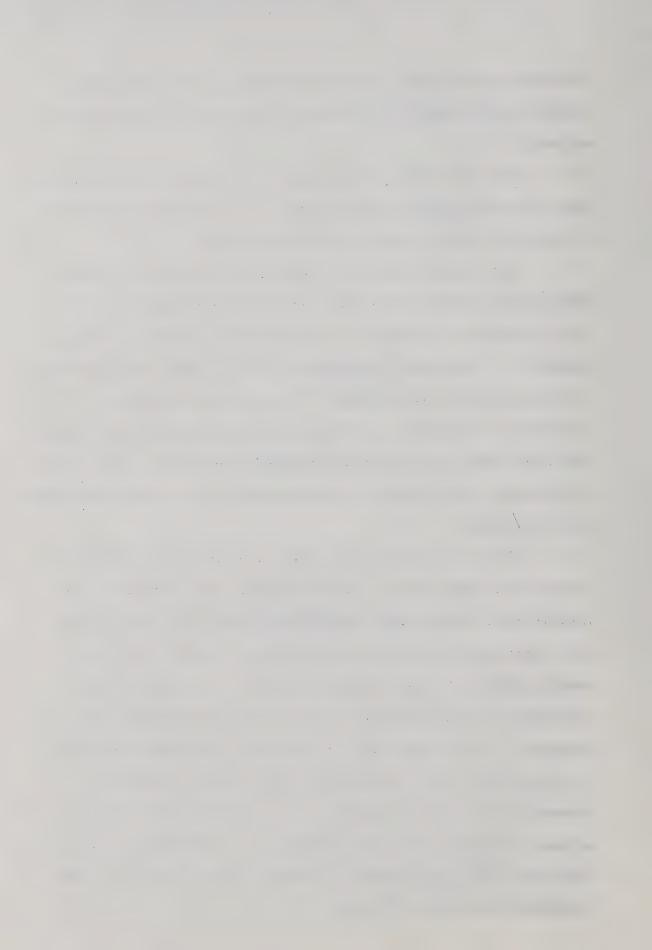
7.1.2 Sampling Distribution Under Various Models and Assumptions

(a) Applying Tukey's result, a new formula for the standard error of reliability estimate was derived. The formula depends only on sample size, number of part tests, reliability, and the kurtosis

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of the test scores, and is found to be superior to the traditional formula based on normal theory when the distribution of true score is not normal.

- (b) The effects of non-normal error scores distributions are found to be negligible for not too small J, the number of part tests or items, for both the continuous and binary cases.
- (c) For continuous test score cases, the effects of non-normal distributions of true scores are found to be significant, i.e., the distribution of reliability is systematically distorted. If the essentially τ equivalent assumption is not satisfied, the distribution is systematically shifted leftward or to the lower direction of reliability. This effect is more clearly observed for the multi-factor true score model case indicating inappropriateness of the Alpha formula for the model. The effects of non-homogeneous error variance were found to be negligible.
- (d) For the binary item case the effect of non-normal distributions of latent scores is not so obvious. The formula for the standard error derived under the ANOVA model and normal theory seems quite robust against violation of assumptions imposed by a binary scoring scheme. The test parameters depend on the shape of latent score distributions for fixed biserial correlation and difficulty parameters. If the essentially τ equivalent measurement assumption is not satisfied, i.e., biserial correlation and/or difficulty parameters are not all homogeneous, the distribution of reliability estimates is shifted leftward systematically. The effects of non-homogeneous difficulty parameters seems more severe than that of non-homogeneous biserial correlations.



7.1.3 Robustness of F-Test

The F-test based on ANOVA model and normal theory is robust against violation of the following assumptions:

- (a) Normality of error scores for both continuous and binary cases.
 - (b) Homogeneity of error score variances for continuous cases.
- (c) Homogeneity of biserial correlations for the binary case if the violation is not too extreme.
 - (d) Normality of latent score distributions for binary case.

The F-test may be misleading if the following conditions are not satisfied.

- (a) Uni-factorness of true and latent score distributions.
- (b) Normality of true scores for continuous case. Especially positive kurtosis of true scores results in severe distortions.
- (c) Essentially τ equivalent assumptions (approximately at least).
- (d) Homogeneity of item difficulty parameters (approximately at least).

Nevertheless, in all cases, the F-test is robust against any violation of assumptions if the population reliability is close to zero for both continuous and binary cases. If only the lower tail portion of the distribution is used for the binary item test, the significance test is also robust in most cases.

7.2.0 Implications to Test Theory and Applications

In this study, it has been demonstrated that the distribution of the reliability estimate depends significantly on the models employed,

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the underlying assumptions, and the parameters of part tests or items. Therefore the validity of any statistical inference about reliability largely depends on the validity of models and assumptions like any other statistical inference. Therefore it is essential, for statistical inference about reliability, to know the models appropriate for the test in use, and the population characteristics for the test must be known a priori. For a casual user of psychological and educational tests, this is an almost impossible task. Therefore, for test users and/or other researchers, the findings in this study may not be of any practical use without knowledge of the above information about the test except when robust conditions are present.

However, for a test author, or for a test reviewer, the task of gathering the necessary data may be accomplished as a by-product of the usual procedure for the test development, since an administration of the test to a comparatively large sample of subjects from the population for whom the test is developed is usually involved in order to standardize and to obtain test norms. The test statistics based on such large samples may be used to obtain such information.

Although there is no agreed upon statistical and psychometric methods to obtain such parameters, some efficient methods for the calculation of part test parameters have been developed recently by a number of psychometricians.

For example, Kristof (1969) considered the estimation of the true score variance σ_A^2 and error score variance $\{\sigma_{ej}^2\}$ under an essentially τ equivalent measurement assumption by employing maximum likelihood method. He derived the likelihood equations and found that these could be solved rapidly by a simple Newton-Raphson procedure.

For the binary item test cases, the item difficulty is easily

calculated, and the biserial correlation parameters may be obtained by factor analysis of the tetrachoric correlation matrix from the results of (3.14), if the latent score has a uni-factor structure.

Jöreskog (1971) has shown some examples of model identification techniques by employing maximum likelihood factor analysis on the disperson matrices of test scores obtained from large samples.

In regard to distributions, the distribution of error score is found to be not important, but the shape of the distribution of true scores can affect the reliability estimate significantly. Although the distribution of true scores is not observable directly, since only the kurtosis of true score will affect the distribution of reliability estimates, and it can be indirectly evaluated by the test score kurtosis divided by the square of reliability from the results of (5.9), the normality of true score may be investigated partly by examining the test score kurtosis if it is obtained from a large sample.

Therefore, a test author or reviewer would be doing a service to the users of a test, if he provided information about the model involved, and distributions and parameter values in the population for which the test is developed. If the test satisfies the ANOVA model and normal theory assumptions, or violates only those assumptions which are known to be unimportant, the author or reviewer may recommend the use of the F-test for the inference about reliability. In this case the author or reviewer needs to supply only the information about the population reliability. Otherwise, the author or reviewer should either provide all information necessary for simulation of such tests by the computer program developed in this study, or alternatively, provide a table of upper and lower critical points of the distribution of

reliability estimates as a function of sample size, and should probably also provide the values of the standard errors. Then the user could easily determine whether the observed reliability is significantly different or not from the population value at a specific significance level.

7.3.0 Example 1: Application to Continuous Case

Since it was not possible to find an appropriate example of a test and its manuals which provide the necessary information for the test models and the other information necessary for the application of computer simulation techniques, somewhat arbitrary example data were selected to show how the findings in this study and the computer programs developed might be applied in a practical situation.

Jöreskog (1971) analyzed a dispersion matrix based on four measures used by Votaw (1948) to establish methods of obtaining reader reliability in essay scoring for an English composition test, and identified the model as a congeneric true score model. The dispersion matrix was obtained from 126 subjects, and is given in Table 7.1.

TABLE 7.1

Dispersion Matrix of Votaw's Essay Test Data,

| = 126

Measure	1	2	3	4
1	25.0704	12.4363	11.7257	20.7510
2	12.4363	28.2021	9.2281	11.9732
3	11.7257	9.2281	22.7390	12.0692
4	20.7510	11.9732	12.0692	21.8707

He employed maximum likelihood factor analysis, and gave the estimate of the standard deviation of true score or factor loading as,

$$\underline{\lambda}' = [4.57 \ 2.68 \ 2.65 \ 4.53]$$
.

Therefore, if a test author published a test consisting of four part tests and obtained the same results as above based on a large sample, these values may be regarded as population parameter values if small discrepancies in covariance terms are ignored. Then the test score model would be as follows,

$$\underline{Y}_{i} = \begin{bmatrix} 4.57 \\ 2.68 \\ 2.65 \\ 4.53 \end{bmatrix} \begin{bmatrix} f_{i} \\ \end{bmatrix} + \begin{bmatrix} 2.0459 & 0.0000 & 0.0000 & 0.0000 \\ 0.0000 & 4.5847 & 0.0000 & 0.0000 \\ 0.0000 & 0.0000 & 3.9644 & 0.0000 \\ 0.0000 & 0.0000 & 0.0000 & 1.1618 \end{bmatrix} \begin{bmatrix} \underline{\epsilon}_{i} \\ \end{bmatrix}$$

Then,

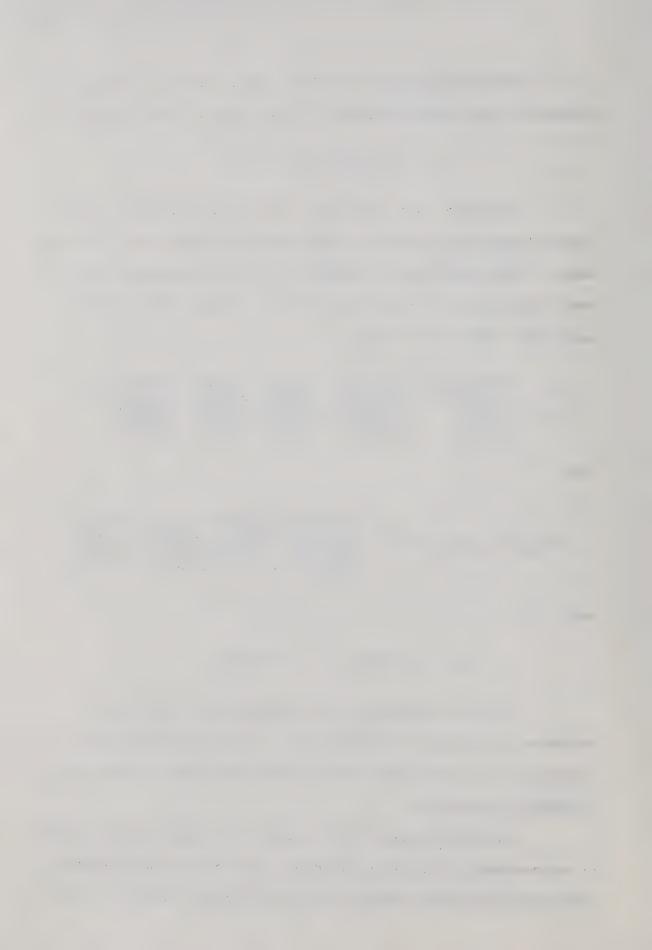
$$D\left(\underline{y_i}\right) = \underline{\Sigma} = \underline{\lambda} \ \underline{\lambda'} + \underline{\Psi}^2 = \begin{bmatrix} 25.0704 & 12.2476 & 12.1105 & 20.7021 \\ 12.2476 & 28.2021 & 7.1020 & 12.1404 \\ 12.1105 & 7.1020 & 22.7390 & 12.0045 \\ 20.7021 & 12.1404 & 12.0045 & 21.8707 \end{bmatrix},$$

and,

Alpha = 0.812329,
$$\rho$$
 = 0.831249.

Since the assumption of the homogeneity of true score variances is violated, the essentially τ equivalent measurement assumption is not valid and hence the Alpha coefficient is lower than reliability as expected.

From the findings of this study, it is known that the effects of non-homogeneous true score variance is not too great with moderate differences among the elements of the factor loading vector $\underline{\lambda}$, but



the differences for this data seem exceptionally large and also the difference between Alpha coefficient and the reliability is substantial. Therefore a systematic distortion of the distribution of reliability estimates toward lower reliability is expected. Seven computer simulation experiments were performed with the Jöreskog's model with N = 2000 and assumed normality of true and error scores. Both estimation formulas, namely the Alpha formula of (2.13) and Kristof's unbiased formula of (5.2)-(a) were used for estimation of sample reliability. Observed upper and lower 5% critical points together with standard errors are summarized in Table 7.2. The observed values are also compared with those obtainable under the ANOVA model and normal theory. The sample sizes I, the number of subjects, used for these experiments are 10, 15, 20, 25, 30, 35, and 40 respectively. Figures 7.1 - 7.7 compares empirical distribution with the theoretical distributions indicating the effect of the violation of the essentially τ equivalent measurement assumptions.

A table similar to Table 7.2 might accompany the test manuals or test review report so that test users may consult the table whenever they make inferences about the reliability. For example, if a teacher administered the test to a sample of 20 students and obtained $\hat{\rho}=0.892$, then by consulting this table—she may conclude that the difference between the population value 0.812 and her sample value is not significant at 5% level of Type one error. Therefore, she may not claim that her sample is significantly different from the population for which the test is developed as far as the reliability is concerned. The author or researcher could develop a slightly different table if the population test score is not normal. For

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 $(x_1, x_2, \dots, x_n) = (x_1, \dots, x_n) + (x_1, \dots, x_n)$

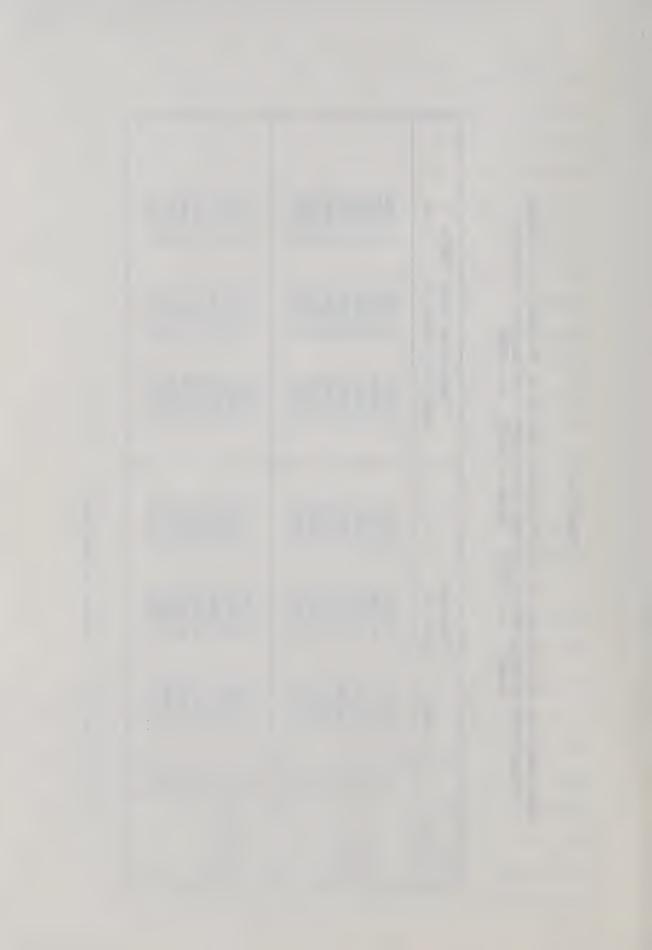
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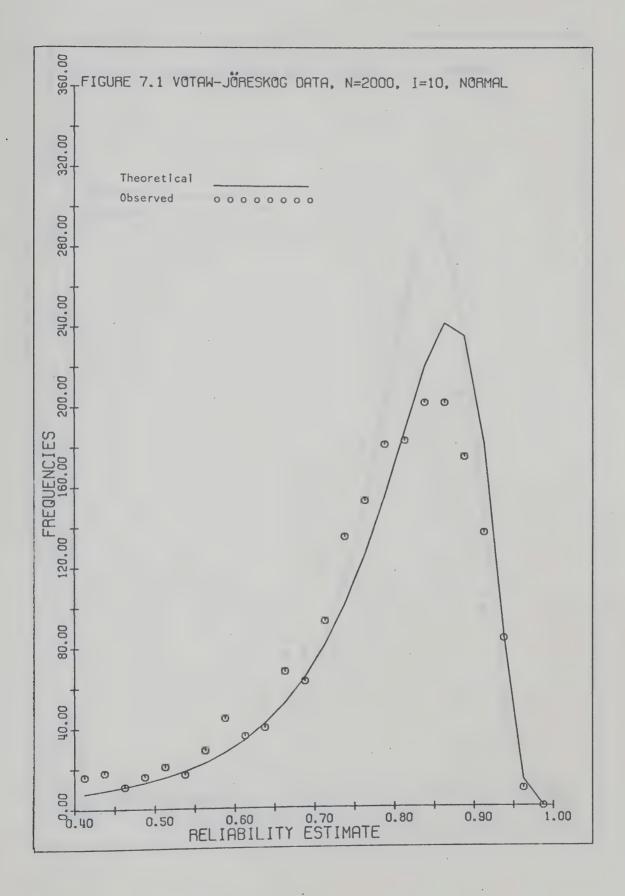
TABLE 7.2

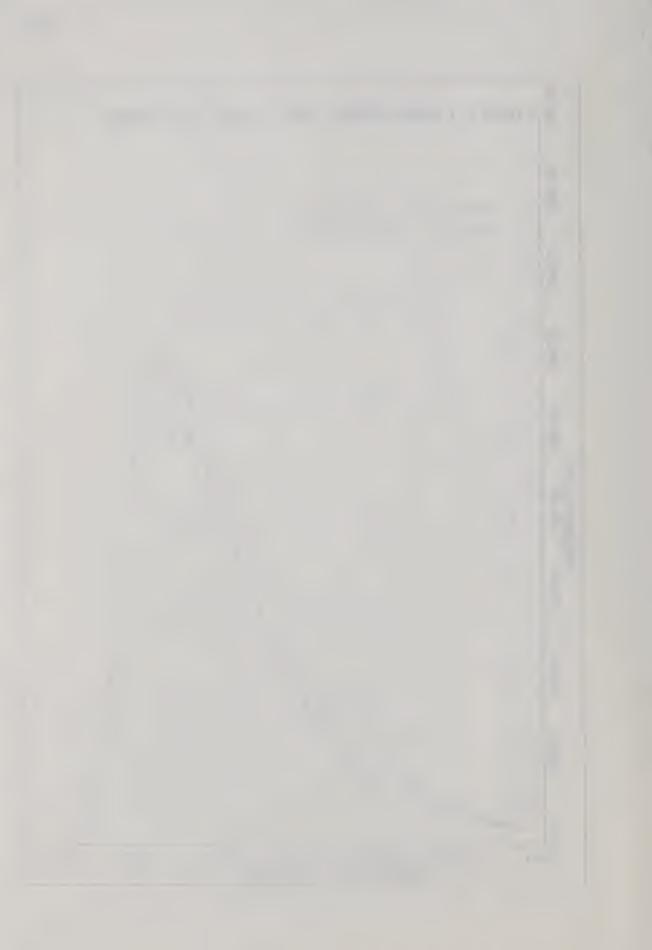
Lower and Upper 5% Critical Points of the Distribution of Reliability Estimates Votaw-Jöreskog Data, Normal True and Error Score Distributions, Congeneric Model, $\rho=0.8313$, Alpha = 0.8123, N = 2000

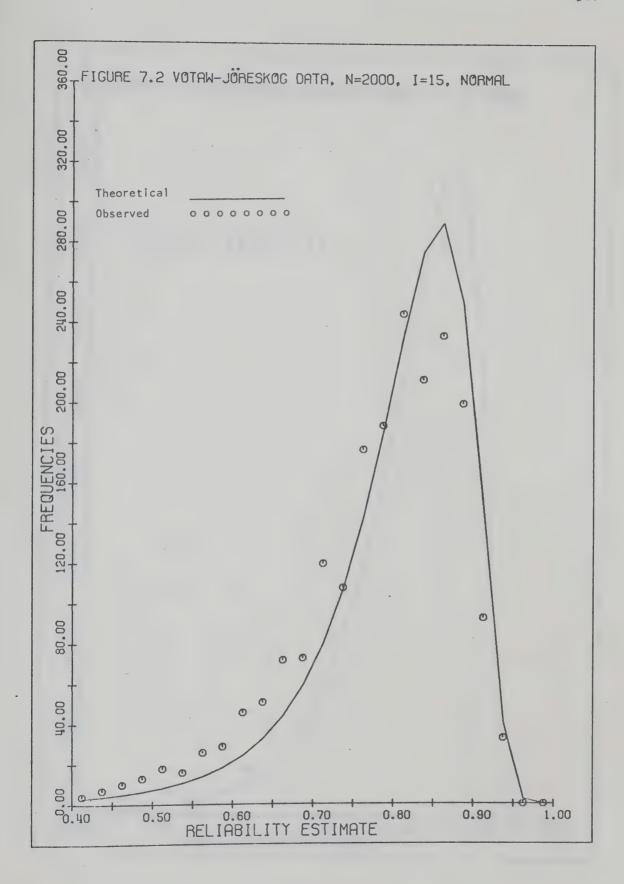
ANOVA S.E.	0.1540 0.0998 0.0785 0.0665 0.0587 0.0531	0.1198 0.0856 0.0702 0.0610 0.0546 0.0499
Theoretical Under ANOVA er 5% Upper 5%	0.9250 0.9128 0.9048 0.8989 0.8944 0.8907	0.9417 0.9252 0.9148 0.9073 0.8972 0.8934
Theore Lower 5%	0.7141 0.6186 0.6651 0.6920 0.7226 0.7323	0.6221 0.6731 0.7003 0.7176 0.7298 0.7389 0.7460
S.E.	0.1671 0.1130 0.0881 0.0733 0.0624 0.0608	0.1301 0.0970 0.0790 0.0673 0.0582 0.0572
Observed Upper 5%	0.9223 0.9048 0.8952 0.8917 0.8841 0.8808	0.9395 0.9184 0.9062 0.9007 0.8878 0.8826
Lower 5%	0.4501 0.5565 0.6194 0.6586 0.6872 0.6918	0.5723 0.6199 0.6595 0.6871 0.7099 0.7099
_	10 15 20 25 30 35 40	10 20 25 30 35 40
Est. Formula	Alpha (2.13) Bíased	Kristof's (5.2)-(a)

1 : sample size, i.e., number of subjects.

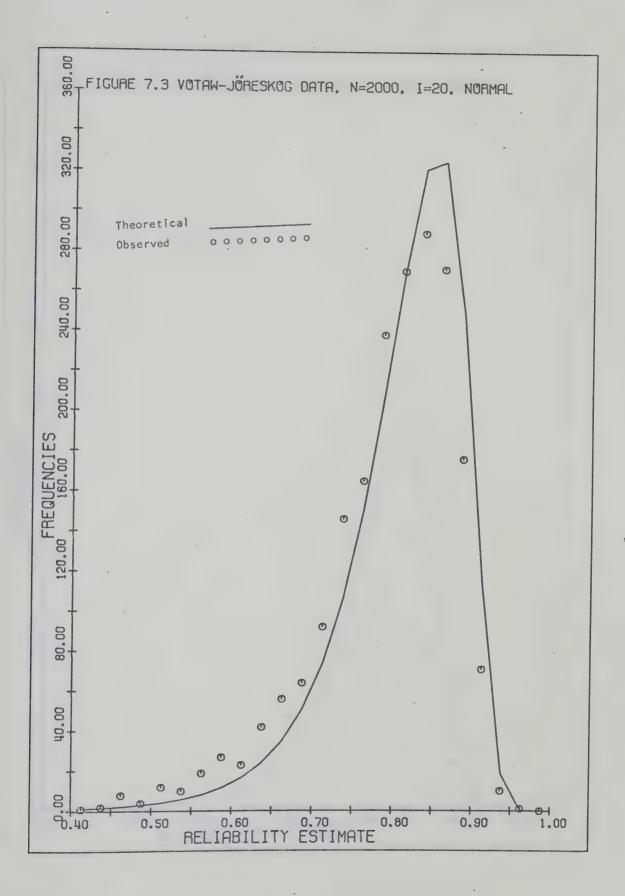




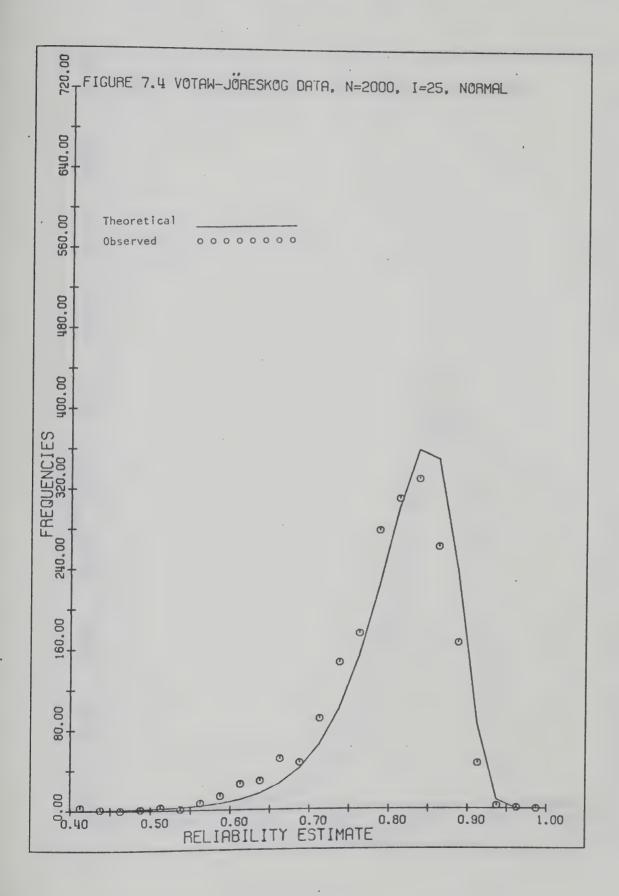




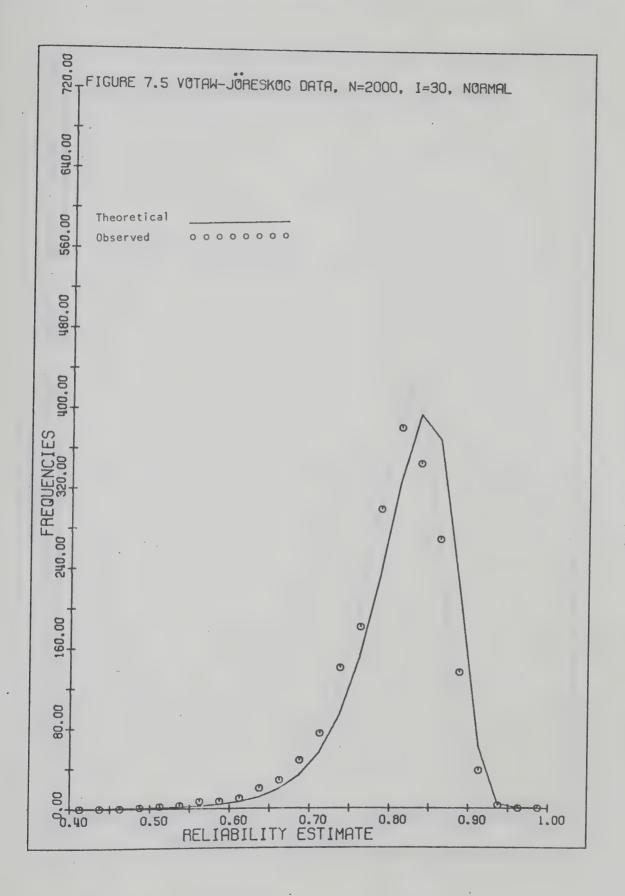




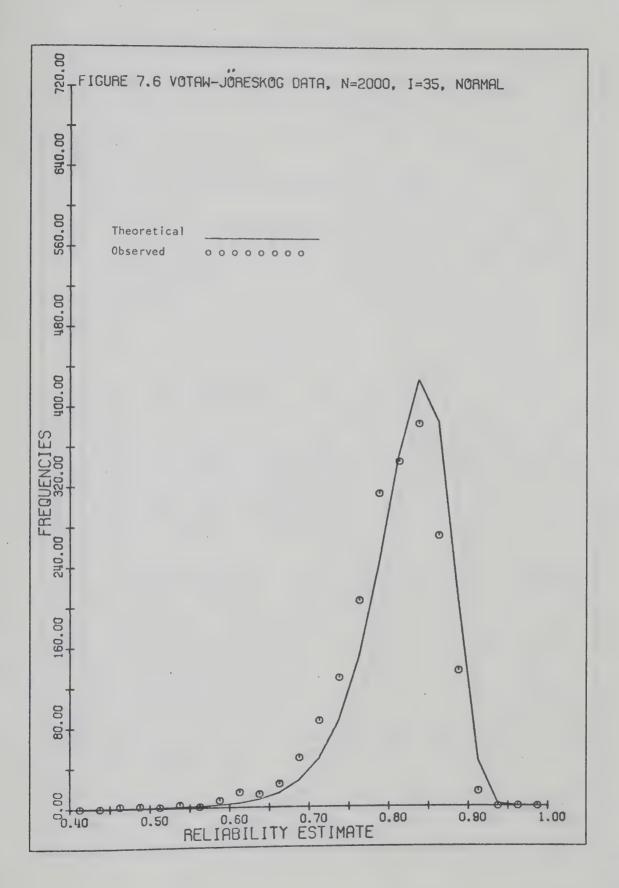




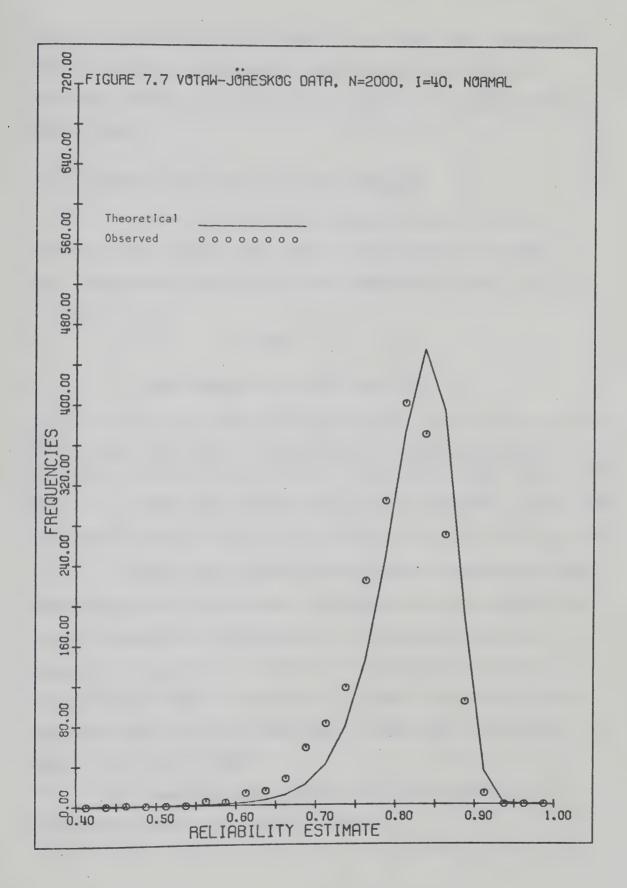














example, if ranked marks were assigned for each part test, the greater likelihood is that the true scores would be distributed uniformly rather than normally, and the shapes of reliability estimates would be much different.

7.4.0 Example 2: Application to Binary Item Case

A hypothetical binary item test consisting of 9 items is considered as an example. The values of item parameters are taken from Lord and Novick (1968, p. 379), and summarized in Table 7.3.

TABLE 7.3

Item Parameters of a Nine Item Test

Items	1	2	3	4	5	6	7	8	9
Difficulty	0.096	0.199	0.338	0.434	0.471	0.574	0.676	0.801	0.822
Biserial Cor.	0.490	0.717	0.549	0.593	0.595	0.640	0.476	0.530	0.495

It may be noted that the item difficulty parameters are rather heterogeneous with a value as small as 0.096 to as high as 0.822. Therefor it is expected that the essentially τ equivalent measurement assumption is substantially violated. To investigate the sampling distribution of reliability estimates of a binary item test with these parameters under the normal ogive model, an experiment was performed with I = 30, and N = 1000.

The theoretical test parameters and those obtained by parallel form method are compared in Table 7.4.

TABLE 7.4

Test Parameters of a Nine Item Test

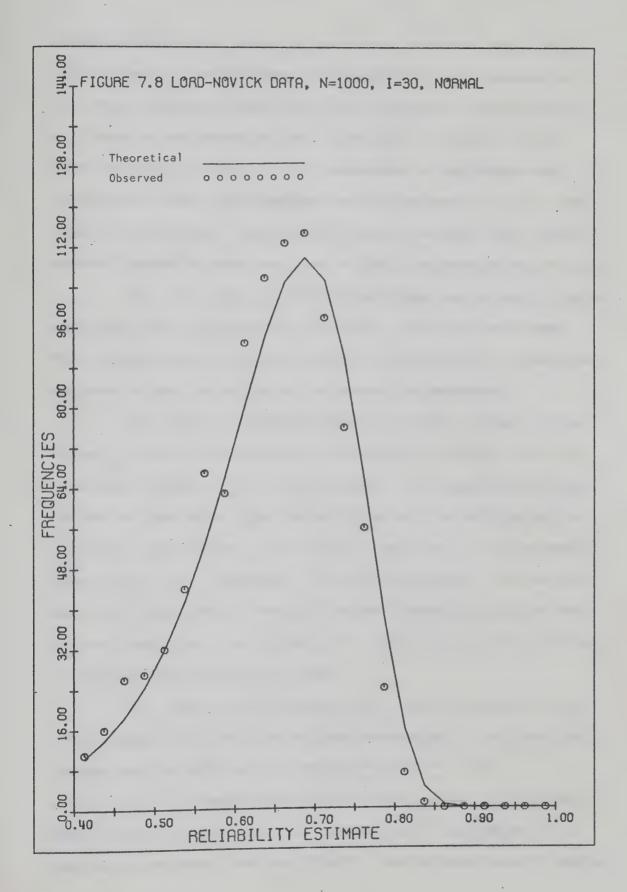
Methods	Mean	Variance	Reliability	KR20
Theoretical Parallel Form	4.4710 4.4774	4.0054 4.0023	0.6632	0.6498

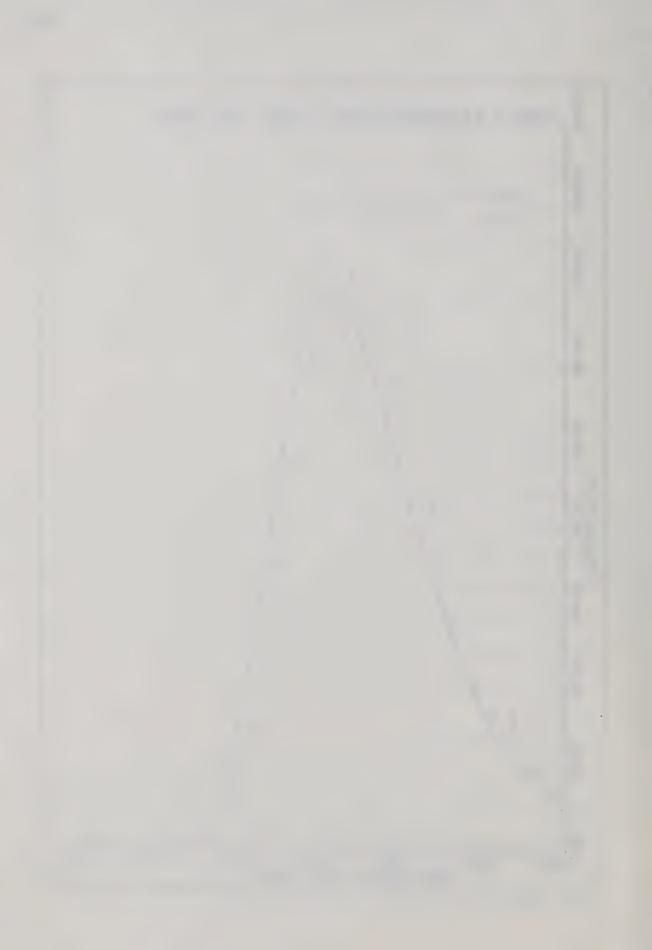
Therefore a user of this test may compare her observed test mean, variance, and KR20 with the values given in this table, and can make some conclusions about her sample group.

The shape of the distribution of reliability estimate based on (2.13) is compared with the theoretical distribution under the ANOVA and normal theory model in Figure 7.8. The distribution shows a systematic shift leftward probably due to heterogeneous difficulty parameters. The lower and upper 5% critical points of this distribution are 0.4412 and 0.7793 respectively while the theoretical values are 0.4466 and 0.7656 respectively. Therefore, if a user of the test found a reliability estimate of 0.79 with I = 30, it may be concluded that the reliability is significantly higher than the population value at the 5% level of significance.

7.5.0 Recommendations

As noted in Section 4.8 of Chapter Four, in the discussion of the methodological limitation of this study, the computer simulation experiments cannot be exhaustive and cover all possible combinations of models, parameters, and distributional assumptions. Also due to the limitations imposed by limited funds available for the computing





charges, the scope and extent of experiments have been restricted to certain special cases which may not always be directly relevant to real data. Because of these facts, the findings of this study will be limited to some extent in their generalization and application.

Therefore, the findings will, by circumstance, be exploratory and illustrative rather than comprehensive with the emphasis having been placed on methodology. Based on the findings and experience with the computer simulation techniques, the following recommendations are made:

- (a) The computer simulation techniques can be used to solve many statistical and psychometric problems in test and measurement theory and application. Further use of this technique is recommended and research must be carried out to improve the methodology.
- (b) Authors of published tests, or their reviewers, should attempt to specify the appropriate test model for a given test, and place such information in the test manuals. The manuals should also include the population dispersion or tetrachoric correlation matrix of true or latent scores or estimate of them as well as the parameter values such as error variances, difficulty and biserial correlations based on a large sample. The distributional characteristics of true or latent scores and error scores of the population for which the test is developed should also be included.
- (c) Some of the findings in this study are based on only a few parameter sets and distributional assumptions. Therefore, the findings must be confirmed by replicated studies with a wider range of parameter sets and with distributions of different shapes of true or latent and error scores, and if applicable, using real test score data. More specifically, the following aspects require

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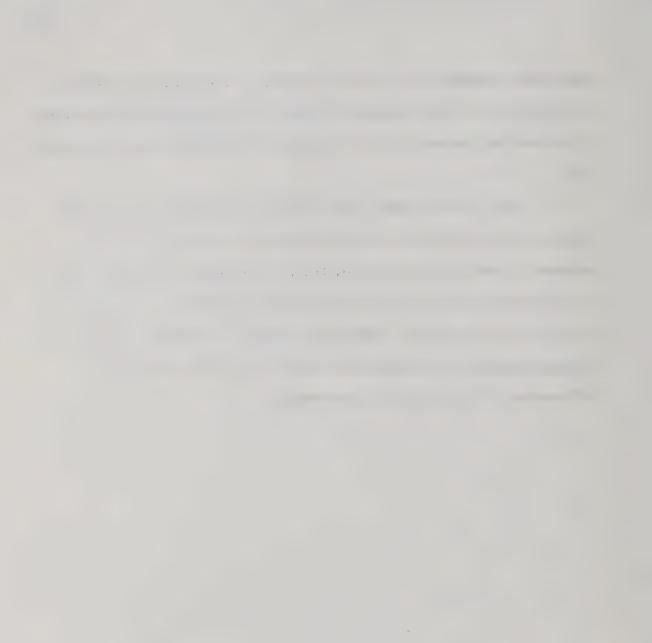
 $(x_1, x_2, \dots, x_n) = (x_1, \dots, x_n) + (x_1, \dots$

further investigation:

- (i) The effect of non-homogeneous true score variance, i.e., the distribution of reliability estimates under the congeneric model for a wider range of λ 's.
- (ii) The effects of non-homogeneous item difficulty parameters for the binary item test cases.
- (d) In this study, the size of sample is artificially fixed at I = 30. An investigation must be made to examine the effects of sample size to see how fast the estimate converges to its expected value with increasing sample size.
- (e) The investigation of this study was limited to Type 1 sampling situations only, but a similar method can be employed for Type 2 or Type 12 sampling situations possibly with a different type of ANOVA model.
- (f) The test score used in this study was a simple unweighted sum of J part test or item scores, although a weighted sum could have been easily employed. The effects of a weighted sum on the reliability estimate must be explored as an extension of this study.
- (g) In this study, one of the basic assumptions of test theory was assumed to be always valid. The assumption was one of independence of error and true scores. In practice this may be violated and the effects of such violation on the distribution of the estimate of reliability must be investigated. Computer simulation would provide an ideal method for such an investigation.
- (h) It is clear that Alpha coefficient as an estimate of reliability is inappropriate if the essentially τ equivalent

measurement assumption is violated too much. Therefore a new effort is necessary to find an appropriate means to estimate reliability under this condition, especially for the case of the multi-factor true score model.

(g) In this study, the investigations were limited to one sample and one reliability estimate cases, and comparisons of the estimate to the population value, but similar methods may be applied to investigate for the cases of more than one sample or reliability estimates either based on independent samples or repeated measures on the same sample to investigate the sampling distribution of the differences of the reliability estimates.



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APPENDIX A.1

LISTINGS OF COMPUTER PROGRAMS

RELO1 : Simulation Program for Continuous

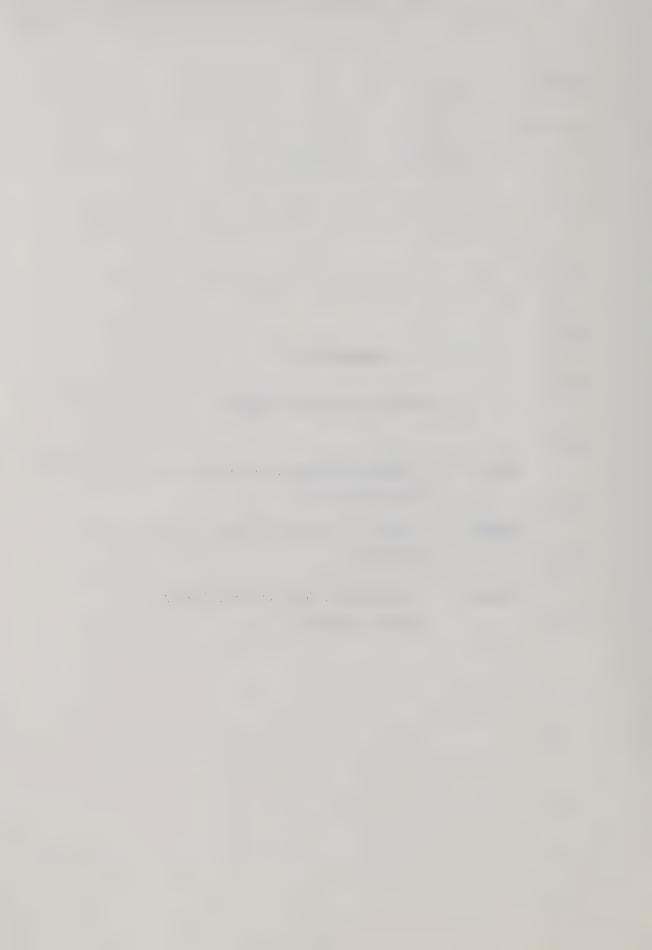
Part Test Case

RELO2 : Simulation Program for Binary Item

Test Case

RELOO : A Package of Sub-Programs Shared by

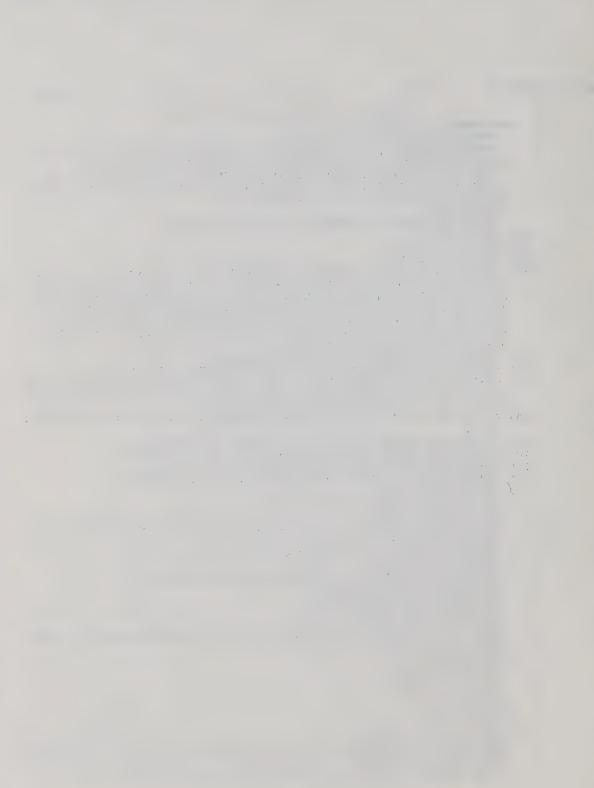
RELO1 and RELO2



```
C
C
                   DIVISION OF EDUCATIONAL RESEARCH SERVICES
    RELO1
C
                   UNIVERSITY OF ALBERTA
C
                                                    **********
C
    PURPOSE:
                   SIMULATES CONTINUOUS PART-TEST SCORES BASED ON MULTI-
C
                   FACTOR TRUE SCORE MODEL TO INVESTIGATE SAMPLING
C
                   DISTRIBUTION OF RELIABILITY ESTIMATES
C
    CARD INPUT:
C
                   1. TITLE (20A4)
C
                   2. PARAMETERS(1115, F5.5): NSAM, MI, MJ, NF. IX. IDIST. IDISE.
C
                       IPUNCE, IPLOT, MODE, LB, SIG
C
                       NSAM
                               NO OF SAMPLES SIMULATED
C
                       MI
                               NO OF
                                      SUBJECTS IN THE SAMPLE
                               NO OF PARTS
C
                       MJ
C
                       NF
                               NO OF FACTORS IN TRUE SCORE
C
                               ANY ODD INTEGER TO INITIATE RANDOM NUMBER
                       IX
C
                       IDIST
                               OPTION FOR THE DISTRIBUTION OF RANDOM
C
                               EFFECTS (TRUE SCORE)
C
                               0-NORMAL
                               1-SPECIFIED BY SUBPROGRAM DIST
C
                               OPTION FOR THE DISTRIBUTION OF ERROR
C
                       IDISE
C
                               O-NORMAL
C
                               1-SPECIFIED BY SUBPROGRAM DISE
                               OPTION FOR CARD OUT FUT OF FREQUENCIES
C
                       T PHINCH
C
                               O-NO CARD OUTPUTS
                               1-CARD OUTPUT REQUIRED
C
                               OPTION FOR PLOTS
                       TPL OT
C
C
                               O-NOT REQUIRED
                               1-REQUIRED
C
                               OPTION FOR ESTIMATION FORMULA
                      MODE
C
C
                               O-ALPHA FORMULA(BIASED)
                               1-KRISTCF CORRECTION(UNBIASED)
C
                               2-BOTH OF ABOVE
C
                               OPTION FOR THE NO OF CLASS INTERVALS FOR
                      1 B
C
                               THE FREQUENCY CALCULATION, 24, 36 OR 48,
C
                               ASSUMED 24
C
                               SIGNIFICANCE LEVEL FOR EACH TAIL, ASSUMED
                       SIG
C
                               0.05
C
                               FORMAT FOR THE INPUT VECTORS AND MATRIX
                   3. FMT
C
                               A VECTOR OF MEANS FOR EACH PART
                   4. FIX
C
                   5. ERR
                               A VECTOR OF STANDARD DEVIATION OF ERROR
C
                               SCORES FOR EACH PART-TEST
C
                               A FACTOR LOADING MATRIX OF SIZE MJ BY NF
                   6. FAC
C
                   7. A BLANK CARD
C
    REMARK:
C
                    1. CURRENTLY DIMENSIONED TO ACCOMODATE UP TO FOLLOWING
C
                      SIZE PARAMETERS
C
                       NS AM
                                                               5000
C
                                                               100
                       MI
C
                                                                 30
                       MJ.
C
                                                                 10
                       NF
C
                                                                48
                       LB
C
                   (FORTRAN) ANOV, BOXSN, CHIPRB, COUNT, DISCRP, DISP, EXAMPL,
    SUBPROGRAMS:
C
                   FISHER, FITTES, FST, MXOUT, PLOT, POPR, PUNCH, RELDIS, ROZB,
C
                   SIGTES, VARXX, VECRAN, VEOUT, DATA, DIST, DISE
C
```

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FORTRAN IV G CCMPILER
                               MAIN
                                                 09-15-71
                                                                  15:55.55
                                                                                  PAGE 0002
             C
                                  (*SSPLIB) BDTR, CDTR, DLGAM, NDTR, RANK
             C
                  PROGRAMMER:
                                  K.BAY
             C
                    NMAX=LARGER OF NSAM AND MI*MJ
             C
                    DIMENSION FAC(MJ*NF), ERR(MJ), VAR(MJ), DIS(MJ, MJ), FIX(MJ), BSUM(MJ),
             C
                   18SS(MJ), Y(MI*MJ), BB(MJ), FMS(NSAM *3), FREQ(LB *3), TEMP(MI*NF)
                    DIMENSION TITLE(20), FMT(20), LAB( 4), FAC( 300), ERR( 30), VAR( 30),
0001
                   1DIS( 900), FIX( 30), BSUM( 30), BSS( 30), Y( 3000), BB( 30), FMS( 15000)
                   2, FREQ(144), XBAR( 6), XVAR( 6), TEMP(1000)
0002
                    REAL*8 LAB
0003
                    CATA LAB/'SUBJECT', 'PARTTEST', 'ERROR', 'REL COF'/
0004
                100 FORMAT (20A4)
                101 FORMAT (1H1, 20A4)
0005
0006
                102 FORMAT (1115, F5.5)
0007
                103 FORMAT(/,10X, NO OF SAMPLES SIMULATED,15X, I4,/,10X, NO OF SUBJEC
                   ITS IN EACH SAMPLE', 11x, 12, /, 10x, 'NO OF PART-TESTS', 24x, 12, /, 10x,
                   2'NO CF FACTORS IN TRUE SCORE', 14X, 11, /, 10X, 'STARTING INTEGER RANDO
                   3M NUMBER*, 2X, 110, /, 10X, *OPTION FOR CARD OUTPUT*, 19X, 11, /, 10X,
                   4ºOPTION FOR PLOT", 26X, 11, /, 10X, "OPTION FOR ESTIMATION FORMULA",
                   512X,I1,/,10X, OPTICN FOR THE NO OF CLASS INTERVALS ,3X, [3,/,10X,
                   6'SIGNIFICANCE LEVEL',19X,F5.3,/)
                104 FORMAT (2X, 13, 5X, 2E14.6, 2X, 11, 2X, 2E14.6)
0008
0009
                105 FORMAT(/,1X, ********LAST SEED RANDOM NUMBER IX=*, I10)
                106 FORMAT(/,1x, DISCRIPTIVE STATISTICS FOR FIXED EFFECT ESTIMATES AND
0010
                   1 EXPECTED VALUES UNDER M.F. MODEL', /, 1X, 'PART', 7X, 'MEAN', 10X, 'EXP
                   2ECTED',6x,"|',5x,"VARIANCE',8X,"EXPECTED')
                107 FORMAT(1H1,23('@'),/,1X,'@',2X,'SUMMARY OF CUTPUT',2X,'@',/,1X,23(
0011
                108 FORMAT(10X, 'ERROR SCORE DISTRIBUTIONS ARE NORMAL')
0012
                109 FORMAT(10X, 'ERROR SCCRE DISTRIBUTIONS ARE NOT NORMAL')
0013
                110 FORMAT(10X, TRUE SCORE DISTRIBUTIONS ARE NORMAL )
0014
                111 FORMAT(1CX, TRUE SCORE DISTRIBUTIONS ARE NOT NORMAL')
0015
                 10 REAC(5,100) TITLE
0016
0017
                    IF(TITLE(1).EQ.TITLE(2)) GO TO 99
0018
                    WRITE(6,101) TITLE
                    READ(5,102) NSAM, MI, MJ, NF, IX, IDIST, IDISE, IPUNCH, IPLOT, MODE, LB, SIG
0019
                    IF(SIGLL.LE.O.O) SIG=0.05
2020
                    IF (LB.NE.24.AND.LB.NE.36.AND.LB.NE.48) LB=24
0021
                    IF(NF.LE.O) NF=1
0022
                    WRITE(6,103) NSAM, MI, MJ, NF, IX, IPUNCH, IPLOT, MODE, LB, SIG
0023
0024
                    IF(IDIST.EQ.O) WRITE(6,110)
                    IF(IDIST.EC.1) WRITE(6,111)
0025
                    IF(IDISE.EQ.O) WRITE(6,108)
0026
                    IF(IDISE.EQ.1) WRITE(6,109)
0027
                    CALL PCPR(MJ, NF, FAC, ERR, VAR, DIS, REL, ALPHA, TVAR, EVAR, FMT, FIX, GMEAN)
0028
                    TVAR=TVAR/(MJ*MJ)
0029
                    EVAR=EVAR/MJ
0030
                    THETA=TVAR/EVAR
0031
                    DIV=1.0+MJ*THETA
0032
                    CO 20 J=1, MJ
0033
                    BSUM(J)=0.0
0034
                 20 BSS(J)=0.0
0035
                    CALL VECRAN(Y, 300, IX)
0036
                    CALL EXAMPL(MI, MJ, NF, FAC, ERR, IDIST, IDISE, IX, Y, FIX, TEMP, BB, FMS, REL)
0037
                    DO 50 NTRIAL=1, NSAM
0038
                    CALL DATA(MI, MJ, NF, FAC, ERR, IDIST, IDISE, IX, Y, FIX, TEMP)
0039
```



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FORTRAN IV & COMPILER
                                MAIN
                                                  09-15-71
                                                                    15:55.55
                                                                                    PAGE 0003
 0040
                     CALL ANDV(Y, MI, MJ, FMSA, FMSB, FMSE, BB)
 0041
                     FMS(NTRIAL)=FMSA
0042
                     II=NTRIAL+NSAM
0043
                     FMS(II)=FMSB
0044
                     II=II+NSAM
0045
                     FMS(II)=FMSE
0046
                     DC 45 J=1, MJ
0047
                     BSUM(J) = BSUM(J) + BB(J)
0048
                 45 BSS(J)=BSS(J)+BB(J)**2
0049
                 50 CONTINUE
0050
                     DO 54 J=1,MJ
                 54 FIX(J)=FIX(J)-GMEAN
0051
0052
                     WRITE(6,107)
              C
                     CALL MXOUT(FMS, NSAM, 3,0,44,44HMEAN SQUARES: COL-1 MSA, COL-2 MSB, CO
                     NN=NSAM*3
0053
0054
                     XMAX=0.0
0055
                     CO 56 I=1,NN
0056
                 56 IF (FMS(I).GT.XMAX) XMAX=FMS(I)
0057
                     NN=XMAX/10.0+1.0
0058
                     XMAX=NN*10.0
0059
                     TINT=XMAX/LB
0060
                    CALL CCUNT(FMS, NSAM, 3, 0.0, TINT, LB, FREQ, XBAR, XVAR)
0061
                     XMIN=0.0
0062
                     XMAX=TINT*LB
0063
                     XBAR(4)=MJ*TVAR+EVAR
0064
                     O.O=XXXX
0065
                     DO 58 J=1,MJ
0066
                 58 XXXX=XXXX+FIX(J)**2
0067
                     CFA=MI-1
0068
                    DFB=MJ-1
                    DFE=(MI-1)*(MJ-1)
0069
0070
                    XXXX=XXXX/DFB
0071
                    XBAR(5) = EVAR + XXXX * MI
0072
                    XBAR(6)=EVAR
                    XVAR (4) = (2.0*(MJ*TVAR+EVAR)**2)/DFA
0073
                    XVAR(5) = ((EVAR+2.0*MI*XXXX
0074
                                                    )*2.0*EVAR)/DF8
                    XVAR(6) = (2.0 \times EVAR \times EVAR)/DFE
0075
                    CALL DISCRP(3, XBAR, XVAR, LAB(1), 52, 52H MEAN SQUARES AND EXPECTED VA
0076
                   ILUES UNDER ANOVA MODEL )
                    CALL VARXX(NSAM, MJ, BSUM, BSS)
0077
0078
                    WRITE(6, 106)
0079
                    DO 63 J=1, NJ
                    XX=0.0
0080
                    DO 61 M=1, MJ
0081
0082
                    D1=-1.0/MJ
                    IF(J.EQ.M) D1=D1+1.0
0083
0084
                    DO 60 K=1, NJ
                    D2=-1.0/MJ
0085
                    IF(J.EQ.K) D2=D2+1.0
0086
                    MK = NJ*(M-1)+K
0087
0088
                 60 XX=XX+D1*D2*DIS(MK)
0089
                 61 CONTINUE
0090
                    XX = XX/MI
                 63 WRITE(6, 104) J, BSUM(J), FIX(J), BSS(J), XX
0091
```

II=NSAM*2

0092

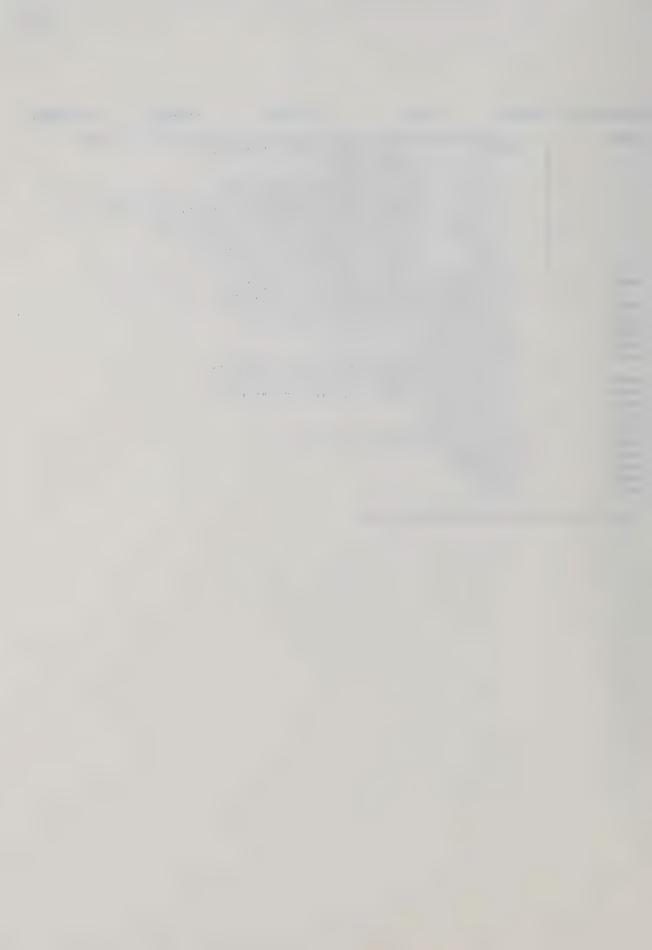
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0093	00 70	I=1,NSAM			
0094	11=11	+1			
0095	70 FMS(1)	=1.0-FMS(II)/F	MS(1)		
0096	. CALL I	RANK (FMS(1), FMS	(NSAM+1), NSAM)		
0097	1F (MOI	DE.NE.1) CALL R	ELDIS(FMS, NSAM, DF	A, DFE, FREQ, LB, REL	,TEMP,SIG,
	1XBAR,	(VAR, IPUNCH, IPL	OT, O, LAB)		
0098	IF (MOI	DE. NE.O) CALL R	ELDIS (FMS, NS AM, DF	A, DFE, FREQ, LB, REL	,TEMP,SIG,
	1XBAR,	KVAR, IPUNCH, IPL	OT,1,LAB)		
0099	WRITE	(6,105) IX			
0100	GO TO	10			
0101	99 STOP				
0102	END				
	2				

TOTAL MEMCRY REQUIREMENTS 015284 BYTES



```
FORTRAN IV & COMPILER
                                 CATA
                                                    09-15-71
                                                                       15:56.00
                                                                                        PAGE 0001
0001
                      SUBROUTINE DATA(MI, MJ, NF, FAC, ERR, IDIST, IDISE, IX, Y, FIX, TEMP)
               C
                   PURPGSE
                                    CREATES DATA MATRIX FOR RELOI
                                     SAMPLE SIZE
               C
                      MI
               C
                         ٧J
                                     NO OF PARTS
               C
                                     NO OF FACTORS'IN TRUE SCORE
                      NE
               C
                         FAC
                                    INPUT FACTOR LOADING MATRIX
                                    INPUT VECTOR OF STANDARD DEVIATION FOR ERRORS OPTION FOR TRUE SCORE DISTRIBUTION
                         ERR
               C
                         IDIST
               C
                                    OPTION FOR ERROR SCORE DISTRIBUTION
                         IDISE
                                  SEED ODD INTEGER RANDOM NUMBER
               C
                        IX
               Ċ
                         FIX
                                    INPUT FIXED EFFECT VECTOR
               C
                        TEMP
                                   WORKING MATRIX
 0002
                      DIMENSION FAC(MJ,NF), ERR(MJ), Y(MI,MJ), FIX(MJ), TEMP(MI,NF)
                      IF(IDISE.EQ.O) CALL SRAND(Y, (MI*MJ), IX)
IF(IDISE.EQ.O) CALL BCXSN(Y, (MI*MJ), IX)
               C
0003
                      IF(IDISE.EQ.1) CALL DISE(Y,MI,MJ,IX)
0004
0005
                      DO 20 I=1, MI
                      DO 20 J=1, MJ
 0006
                  20 Y(I, J)=FIX(J)+Y(I, J)*ERR(J)
 0007
                      IF(IDIST.EQ.O) CALL SRAND(TEMP,(MI*NF),IX)
IF(IDIST.EQ.O) CALL BOXSN(TEMP,(MI*NF),IX)
              C
8000
                      IF(IDIST.EQ.1) CALL DIST(TEMP, MI, NF, IX)
0009
0010
                      DO 30 I=1, MI
0011
                      CO 25 K=1,NF
                      CO 23 J=1, MJ
0012
                  23 Y(I,J)=Y(I,J)+FAC(J,K)*TEMP(I,K)
0013
                  25 CONTINUE
0014
0015
                  30 CONTINUE
                      RETURN
0016
0017
                      END
```

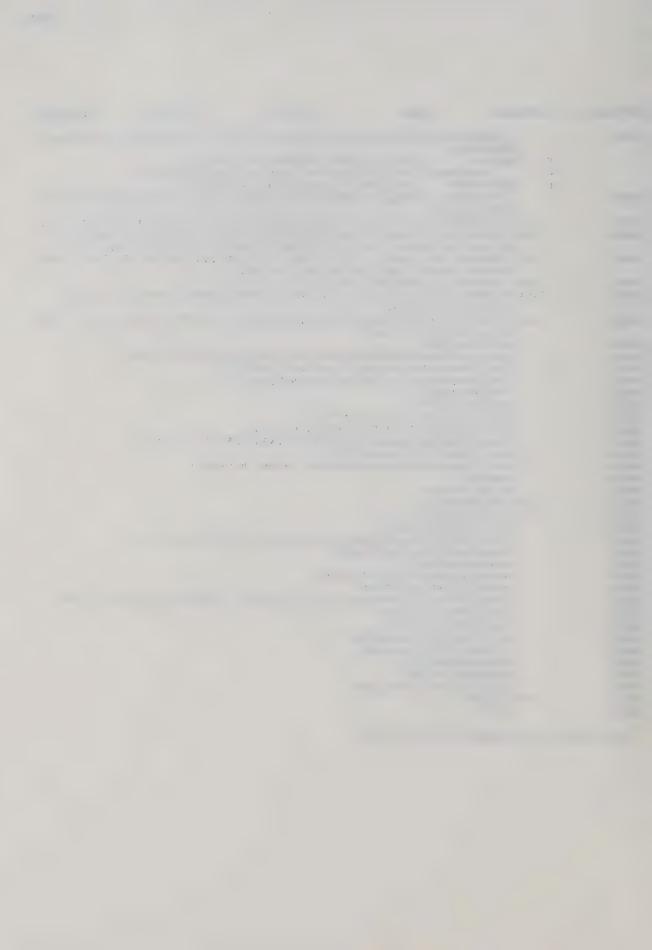
TOTAL MEMCRY REQUIREMENTS 00050E BYTES



```
FORTRAN IV & COMPILER
                               EXAMPL
                                                 09-15-71
                                                                  15:56.02
                                                                                  PAGE 0001
 0001
                     SUBROUTINE EXAMPL(MI, MJ, NF, FAC, EPR, IDIST, IDISE, IX, Y, FIX, TEMP, BB,
                   1FMS, REL)
              C
                  PURPOSE
                                   GIVES EXAMPLE OUTPUTS FOR RELOI
              C
                        ARGUMENTS THE SAME AS THE MAINLINE PROGRAM RELOI
              C
                  SUBPROGRAM
                                   DATA, MXOUT, ANOV, VEOUT, DISP, ROZB
 0002
                    DIMENSION FAC(MJ, NF), ERR(MJ), Y(MI, MJ), FIX(MJ), TEMP(MI, NF), BB(MJ),
                   1FMS(MJ,MJ)
 0003
                100 FORMAT(1H1,20('a'),/,1X,'a',3X,'EXAMPLE RUNS',3X,'a',/,1X,20('a'))
 0004
                101 FORMAT(/,1X, "MSA=",E14.6,2X, "MSB=",E14.6,2X, "MSE=",E14.6,2X, "F=",
                   1E14.6,2X, *ALPHA=*, F8.5,2X, *UNBIASED REL EST(ANOVA)=*, F8.5)
                102 FORMAT(/,1x, 'SAMPLE DISPERSION : SATURATION COEFF=',F9.5,3x, 'HOMOG
 0005
                   1ENEITY COEFF=',F9.5,5X, 'HOM/SAT=',F9.5)
 0006
                103 FORMAT(/,1X, GMEAN=1,E14.6)
                104 FORMAT (/, 1x, 'VARIANCE OF ALPHA ESTIMATE UNDER ANOVA=', F8. 5. 3x.
 0007
                   1'ESTIMATE=',F8.5)
 0008
                105 FORMAT(/,1x, *VARIANCE OF UNBIASED REL ESTIMATES UNDER ANOVA=*, F8.5
                   1,3X, 'ESTIMATE=',F8.5)
 0009
                    WRITE(6,100)
0010
                    CALL DATA(MI, MJ, NF, FAC, ERR, IDIST, IDISE, IX, Y, FIX, TEMP)
0011
                    CALL MXOUT(Y,MI,MJ,O,12,12HDATA MATRIX )
 0012
                    CALL ANOV(Y,MI,MJ,FMSA,FMSB,FMSE,BB)
                    FF=FMSA/FMSE
 0013
                    AL=1.0-1.0/FF
 0014
                    ALL=(2.0+(MI-3.0)*AL)/(MI-1.0)
0015
 0016
                    WRITE(6,101) FMSA, FMSB, FMSE, FF, AL, ALL
                    CALL VEOUT (BB, MJ, 28, 28HSAMPLE FIXED EFFECTS VECTOR )
 0017
                    CALL DISP(Y, MI, MJ, FMS, BB)
0018
0019
                    CALL VEOUT (BB, MJ, 20, 20HSAMPLE MEANS VECTOR )
                    SUM=0.0
 0020
                    CO 20 J=1,MJ
0021
                 20 SUM=SUM+BB(J)
0022
0023
                    SUM=SUM/MJ
                    WRITE(6, 103) SUM
0024
                    CALL MXOUT (FMS, MJ, MJ, O, 24, 24HSAMPLE DISPERSION MATRIX)
0025
                    CALL ROZB(FMS, MJ, SAT, HOM)
0026
                    ALPHA=HOM/SAT
0027
                    WRITE(6,102) SAT, HOM, ALPHA
0028
                    IF(MI.LE.5) GO TO 90
0029
                    VF=(2.0*(MI-1.0)*(MJ*MI-MJ-2.0))/((MI-5.0)*(MJ-1.0)*(MI-3.0)**2)
0030
                    VARA=VF*(1-REL)**2
0031
                    VARE=VF* (1-AL)**2
0032
                    WRITE(6,104) VARA, VARE
0033
                    C2=(MI-3.0)/(MI-1.0)
0034
                    VARA=VARA*C2*C2
0035
                    VARE=VARE*C2*C2
0036
                    WRITE(6,105) VARA, VARE
 0037
0038
                 90 RETURN
```

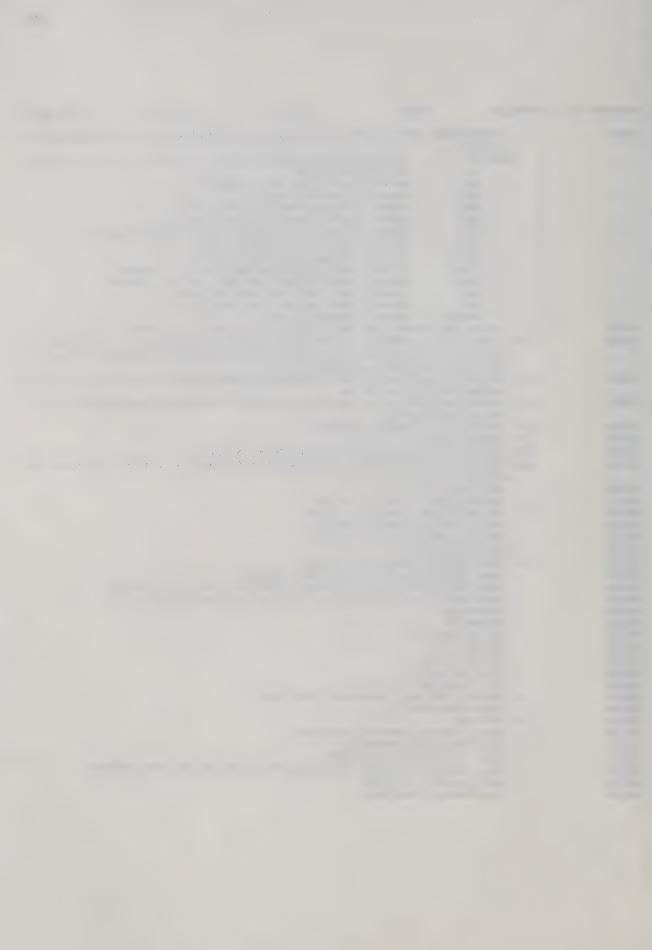
END TOTAL MEMCRY REQUIREMENTS CODAO4 BYTES

0039



```
FORTRAN IV & COMPILER
                               POPR
                                                09-15-71
                                                                  15:56.04
                                                                                  PAGE 0001
0001
                    SUBROUTINE POPR (MJ, NF, FAC, ERR, VAR, DIS, REL, ALPHA, TVAR, EVAR, FMT, FIX,
                   1GMEAN)
              C
                  PURPOSE
                                  PERFORMS BASIC COMPUTATIONS FOR POPULATION PARAMETERS
              C
                       MJ
                                  NO OF PART-TESTS
              C
                        NE
                                  NO OF FACTORS IN TRUE SCORE
              C
                        FAC
                                  FACTOR LOADING MATRIX
              C
                       ERR
                                  ERROR STANDARD DEVIATION VECTOR
              C
                       VAR
                                  OUTPUT VECTOR FOR VARIANCES OF PARTS
             C
                       DIS
                                  OUTPUT DISPERSION MATRIX OF PART-SCORE VECTOR
              C
                       REL
                                  OUTPUT POPULATION RELIABILITY
              C
                        ALPHA
                                  DUTPUT POPULATION RELIABILITY
                                  DUTPUT TRUE SCORE VARIANCE OF TEST SCORE
              C
                        TVAR
                                  DUTFUT ERROR SCORE VARIANCE OF TEST SCORE
              C
                        EVAR
             C
                       FMT
                                  FORMAT FOR INPUT VECTORS AND MATRIX
                       FIX
             C
                                  OUTPUT MEAN VECTOR FOR PARTS
             C
                       GMEAN
                                  DUTPUT GENERAL MEAN
0002
                    DIMENSION FAC(MJ,NF), ERR(MJ), VAR(MJ), DIS(MJ,MJ), FMT(20), FIX(MJ)
                100 FORMAT(/,1X, POPULATION PARAMETERS ,/,1X, RELIABILITY ,19X, F9.5./,
0003
                   11X, "ALPHA", 25X, F9.5, /, 1X, "TRUE SCORE VARIANCE", 11X, E14.6, /, 1X, "ERR
                   20R SCORE VARIANCE', 10X, E14.6)
0004
                101 FORMAT(/,1x, TRUE SCORE DISPERSION: SATURATION COEFF=",F9.5.5x. HO
                   1MOGENEITY COEFF=*, F9.5)
                102 FORMAT(1H1,37('a'),/,1X,'a',3X,'INFUT POPULATION PARAMETERS',5X,
0005
                   1'a',/,1X,37('a'))
                103 FORMAT(/,1X, GMEAN= ,E14.6)
0006
0007
                104 FORMAT(20A4)
0008
                105 FORMAT (/,/,1X, FORMAT FOR THE DATA ,5X, 20A4)
                106 FORMAT(/,1x, PART SCORE DISPERSION: SATURATION COEFF=1,F9.5,5x, HO
0009
                   1MOGENEITY COEF= 1, F9.5)
0010
                    WRITE(6.102)
                    READ(5,104) (FMT(I), I=1,20)
0011
                    WRITE(6,105) (FMT(I), I=1,20)
0012
                    READ(5, FMT) (FIX(J), J=1, MJ)
0013
                    READ(5, FMT)(ERR(J), J=1, MJ)
0014
0015
                    CO 10 I=1,MJ
                 10 REAC(5, FMT) (FAC(I, J), J=1, NF)
0016
                    CALL VEOUT(FIX, MJ, 12, 12 HMEANS VECTOR)
0017
                    CALL VEOUT (ERR, MJ, 32, 32 HERROR STANDARD DEVIATIONS VECTOR)
0018
                    CALL MXOUT (FAC, MJ, NF, 0, 24, 24 HFACTOR LOADING MATRIX
0019
                    TVAR=0.0
0020
                    EVAR=0.0
0021
0022
                    DO 15 J=1, NJ
                    VAR(J)=0.0
0023
                    DO 12 I=1, MJ
0024
                    DIS(1, J)=0.0
0025
                    CO 11 K=1,NF
0026
                 11 DIS(I, J)=DIS(I, J)+FAC(I,K)*FAC(J,K)
0027
                    TVAR=TVAR+DIS(I,J)
0028
                 12 CONTINUE
0029
                    VAR(J)=DIS(J,J)+ERR(J)*ERR(J)
0030 -
                 15 EVAR=EVAR+ERR(J)*ERR(J)
0031
                    CALL ROZB(DIS, MJ, SAT, HOM)
0032
                    CALL MXOUT (DIS, MJ, NJ, 0, 28, 28 HT RUE SCORE DISPERSION MATRIX)
0033
                    WRITE(6,101) SAT, HCM
0034
                    REL=TVAR/(TVAR+EVAR)
```

0035



```
FORTRAN IV & COMPILER
                               POPR
                                                09-15-71
                                                                 15:56.04
                                                                                  PAGE 0002
 0036
                    DO 16 J=1, MJ
 0037
                 16 DIS(J, J) = VAR(J)
 0038
                    CALL ROZB(DIS, MJ, SAT, HOM)
0039
                    CALL MXOUT (DIS, MJ, MJ, O, 20, 20HDISPERSION MATRIX
 0040
                    WRITE(6,106) SAT, HCM
 0041
                    ALPHA=HOM/SAT
 0042
                    WRITE(6,100) REL, ALPHA, TVAR, EVAR
 0043
                    GMEAN=0.0
 0044
                    DO 20 J=1, MJ
                 20 GMEAN=GMEAN+FIX(J)
 0045
0046
                    GMEAN=GMEAN/MJ
                    CO 21 J=1,MJ
 0047
                 21 FIX(J)=FIX(J)-GMEAN
 0048
                    WRITE(6,103) GMEAN
 0049
                    CALL VEOUT(FIX, MJ, 16, 16HFIXED EFFECTS
 0050
 0051
                    CALL VEOUT (VAR, MJ, 20, 20HVARIANCES OF PARTS )
 0052
                    DO 23 J=1,MJ
                 23 FIX(J)=FIX(J)+GMEAN
 0053
                    RETURN
 0054
 0055
                    END
```

TOTAL MEMCRY REQUIREMENTS 0008DC BYTES



FORTRAN	I۷	G	COMPIL	ER	DIST	09-15-71	15:56	5.10	p	AGE 0001
			C PUC	RPCSE TEMP MI NF IX	OUTPUT TO NO OF ROM NO OF COM SEED ODD	TANDARD RANDOM RUE SCORE MATRI WS OF TEMP LS OF TEMP	X I NUMBER	MATRIX	FOR	RELO1
0002 0003 0004 0005 0006 0007 0008			10 20	DIMENSION CALL VECRA DO 20 I=1, DO 10 J=1,	TEMP(MI,NF) N(TEMP,(MI* MI	NF),[X]				

TOTAL MEMCRY REQUIREMENTS 00025A BYTES



FORTRAN IV G COMPILER DISE 09-15-71 15:56.11 PAGE 0001 0001 SUBROUTINE DISE(Y, MI, MJ, IX) CREATE STANDARD RANDOM ERROR MATRIX Y FOR RELOI OUTPUT MATRIX C PURPOSE C NO OF ROWS OF Y C MI C NO OF COLS OF Y MJ C SEED ODD INTEGER RANDOM NUMBER IX C****THIS EXAMPLE PRODUCES UNIFORM ERROR SCORES 0002 DIMENSION Y(MI, MJ) 0003 CALL VECRAN(Y, (MI*MJ), IX) SQR=SQRT(12.0) 0004 0005 00 20 J=1, NJ DO 10 I=1, MI 0006 10 Y(I,J)=(Y(I,J)-0.5)*SQR0007 8000 20 CONTINUE 0009 RETURN 0010 END TOTAL MEMCRY REQUIREMENTS 000264 BYTES

5:56.11 10.5 RC=0



PAGE 0001

SIG

3. FMT

0.05

A VECTOR OF ITEM DIFFICULTIES 4. DIF A VECTOR OF BISERIAL CORRELATIONS 5.85 6. A BLANK CARD 1. CURRENTLY DIMENSIONED TO ACCOMODATE UP TO FOLLOWING

FORMAT FOR THE INPUT VECTORS

REMARK:

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

SIZE PARAMETERS 5000 NS AM

FREQUENCY CALCULATION, 24, 36 OR 48, ASSMED 24 SIGNIFICANCE LEVEL FOR EACH TAIL, ASSUMED

100 MΙ 30 MJ 48 LB

(FORTRAN) ANOV, BOXSN, CHIPRB, COUNT, DISCRP, DISP, EXAMPL, SUBPROGRAMS: FISHER, FITTES, FST, ITEMCO, MXOUT, PARALL, PLOT, POPR, PUNCH, RELDIS, ROZB, SIGTES, VARXX, VECRAN, VEOUT, DATA, DIST, DISE (*SSPLIB) BDTR, CDTR, DLGAM, NDTR, NDTRI, RANK

K.BAY PROGRAMMER:

NMAX=LARGER OF NSAM AND MI*MJ DIMENSION BS(MJ), ERR(MJ), VAR(MJ), DIS(MJ*MJ), DIF(MJ), BSUM(MJ). 1BSS(MJ), Y(MI*MJ), BB(MJ), FMS(NSAM*3), FREQ(LB*3), TEMP(MI), RR(MJ),

CALL EXAMPL(MI, MJ, BS, ERR, TEMP, RR, Y, IX, IDIST, IDISE, X, XBAR, BB, FMS,

20 CONTINUE

IREL, R, XVAR)

CALL VECRAN(Y, 100, IX)

DO 50 NTRIAL=1, NSAM

0039

0040

0041

.

The second

```
FORTRAN IV & COMPILER
                               MAIN
                                                 09-15-71
                                                                   15:54.53
                                                                                   PAGE 0003
0043
                    CALL DATA(MI, MJ, BS, ERR, RR, Y, X, TEMP, IX, IDIST, IDISE, XBAR, R, XVAR)
00 44
                    CALL ANOV(Y,MI,MJ,FMSA,FMSB,FMSE,BB)
0045
                    FMS(NTRIAL)=FMSA
0046
                    II=NTRIAL+NSAM
0047
                    FMS(II)=FMSB
0048
                    II=II+NSAM
0049
                    FMS(II)=FMSE
                    CO 45 J=1, MJ
0050
0051
                    BSUM(J) = BSUM(J) + BB(J)
0052
                 45 BSS(J)=BSS(J)+BB(J)**2
                 50 CONTINUE
0053
                    CALL MXOUT(FMS, NSAM, 3, 0, 44, 44HMEAN SQUARES: COL-1 MSA, COL-2 MSB, CO
              C
0054
                    CALL PARALL(R, XBAR, MI, MJ, NSAM, XVAR, TVAR2, EVAR2, REL2)
0055
                    WRITE(6,107)
0056
                    IF(IDIST.EQ.O.AND.ISISE.EQ.O) GO TO 53
0057
                    TVAR=TVAR2
0058
                    EVAR=EVAR2
0059
                    REL=REL2
0060
                    DO 51 J=1, MJ
0061
                 51 DIF(J)=XBAR(J)
0062
                 53 TVAR=TVAR/(MJ*MJ)
0063
                    EVAR=EVAR/MJ
0064
                    THETA=TVAR/EVAR
0065
                    DIV=1.0+MJ*THETA
0066
                    GMEAN=0.0
0067
                    DO 54 J=1, MJ
                 54 GMEAN=DIF(J)+GMEAN
0068
                    GMEAN=GMEAN/MJ
0069
0070
                    DO 55 J=1.NJ
                 55 DIF(J)=DIF(J)-GMEAN
0071
0072
                    NN=NSAM*3
0073
                    XMAX=0.0
0074
                    DO 56 I=1, NN
                 56 IF(FMS(I).GT.XMAX) XMAX=FMS(I)
0075
0076
                    NN=XMAX/10.0+1.0
0077
                    XMAX=NN*10.0
                    TINT=XMAX/LB
0078
                    CALL CCUNT (FMS, NSAM, 3, 0.0, TINT, LB, FREQ, XBAR, XVAR)
0079
                    XMIN=0.0
0080
0081
                    XMAX=TINT*LB
                    XBAR (4) = MJ * TVAR + EVAR
0082
                    0.0=XXXX
0083
                    DO 58 J=1, NJ
0084
                 58 XXXX=XXXX+DIF(J)**2
0085
                    DFA=MI-1
0086
                    DFB=MJ-1
0087
                    DFE=(MI-1)*(MJ-1)
0088
                    XXXX=XXXX/DFB
0089
                    XBAR(5) = EVAR+XXXX*MI
0090
                    XBAR(6)=EVAR
0091
                    XVAR (4)=(2.0*(MJ*TVAR+EVAR)**2)/DFA
0092
                    XVAR(5)=((EVAR+2.0*MI*XXXX )*2.0*EVAR)/DF8
0093
                    XVAR (6) = (2.0*EVAR*EVAR) / DFE
0094
                    CALL DISCRP(3, XBAR, XVAR, LAB(1), 52, 52H MEAN SQUARES AND EXPECTED VA
0095
                   ILUES UNDER ANOVA MODEL )
```



FORTRAN IV	G COMPILER	MAIN	09-15-71	15:54.53	PAGE 0004
0096	CALL VA	ARXX(NSAM, MJ, B	SUM, BSS)		
0097	WRITE(, 106)			
0098	00 63 ,	J=1, MJ			
0099	X X = O . O				
0100	DO 61 A	(=1, MJ	•		
0101	01=-1.0	/MJ			
0102	IF(J.E)	0. M) D1=D1+1.0			
0103	DO 60 H	(=1,MJ			
0104	D2=-1.0)/MJ			
0105	IF(J.E	.K) D2=D2+1.0			
0106	MK=+J*(M-1)+K			
0107	60 XX=XX+[1*D2*DIS(MK)			
0108	61 CONTINU	JE			
0109	XX=XX/				
0110	63 WRITE(6	,104) J,BSUM(J),DIF(J),BSS(J),X	X	
0111	II=NSAM				
0112		[=1,NSAM			
0113	[] = [[+]				
0114		=1.0-FMS(II)/F			
0115			(NSAM+1),NSAM)		**************************************
0116		E.NE.1) CALL R /AR, IPUNCH, IPL	ELDIS(FMS, NS AM, DFA	, DFE, FREQ, LB, KE	L, IEMP, 51G,
0117			ELDIS(FMS, NSAM, DFA	.DFE .FREQ.LB.RE	L.TEMP.SIG.
OLLY		/AR, IPUNCH, IPL		,	
0118		, 105) IX			
0119	GO TO				
0120	99 STOP				
0121	END				
0121	CND				

TOTAL MEMCRY REQUIREMENTS 017A4C BYTES



```
FORTRAN IV & COMPILER
                                CATA
                                                 09-15-71
                                                                  15:55.01
                                                                                   PAGE 0001
0001
                    SUBROUTINE DATA(MI, MJ, BS, ERR, RR, Y, X, TEMP, IX, IDIST, ISISE, XBAR, R,
                    1XVAR)
              C
                  PURPOSE
                                   CREATES DATA MATRIX FOR RELO2
              C
                        MI
                                   SAMPLE SIZE
              C
                        MJ
                                  NO OF ITEMS
              C
                        BS
                                   INPUT VECTOR OF BISERIAL CORRELATIONS
              C
                        FRR
                                   A VECTOR OF STANDARD DEVIATION OF ERRORS
              C
                                   A VECTOR OF THRESHOLD CONSTANTS FOR EACH ITEM
                        RR
                        Y
                                   DATA MATRIX
              0000000
                        X
                                   WORKING VECTOR
                        TEMP
                                   A WORKING VECTOR
                        IX
                                   SEED RANDOM NUMBER
                        IDIST
                                   OPTION FOR TRUE SCORE DISTRIBUTION
                                   OPTION FOR ERROR SCORE DISTRIBUTION
                        IDISE
                        XBAR
                                   SUM OF SCORES FOR EACH ITEM
                                   INTER ITEM SUM OF PRODUCTS
                        R
              C
                                   A VECTOR OF PARALLEL ITEM SUM OF PRODUCTS
                        YVAR
                    DIMENSION R(MJ*(MJ+1)/2), XBAR(2*MJ)
0002
                    DIMENSION BS(MJ), ERR(MJ), RR(MJ), Y(MI, MJ), X(MI, MJ), TEMP(MI), R(1),
                   1XBAR(1), XVAR(MJ)
0003
                    LM#IM=MM
0004
                     IF(IDISE) 10,10,12
               " 70 CALL BOXSN(Y,MM,IX)
0005
0006
                    CALL BOXSN(X,MM,IX)
0007
                    GO TO 15
8000
                 12 CALL DISE(Y, MI, MJ, IX)
                    CALL DISE(X, MI, MJ, IX)
0009
0010
                 15 IF(IDIST) 16,16,18
0011
                 16 CALL BOXSN(TEMP, MI, IX)
                    GO TO 19
0012
                 18 CALL DIST(TEMP, MI, IX)
0013
                 19 CONTINUE
0014
0015
                    00 70 I=1, MI
                    DO 20 J=1, MJ
0016
0017
                    CUT=RR(J)
                    TR=BS(J) *TEMP(I)
0018
                    YY=TR+ERR(J)*Y(I,J)
0019
                    V(I,J)=0.0
0020
                    IF(YY.GE.CUT) Y(I, J)=1.0
0021
                    YY=TR+ERR(J)*X(I,J)
0022
                    X(I,J)=0.0
0023
                    IF(YY.GE.CUT) X(I,J)=1.0
0024
0025
                 20 CONTINUE
                    DO 30 J=1, NJ
0026
                    XBAR(J) = XBAR(J) + Y(I,J)
0027
0028
                    JJ=MJ+J
                 30 XBAR(JJ)=XBAR(JJ)+X(I,J)
0029
                    IR=0
0030
                    DO 50 J=1, MJ
0031
                    DO 40 K=1,J
0032
0033
                    IR=IR+1
                 40 R(IR)=R(IR)+Y(I,K)*Y(I,J)
0034
                 50 XVAR(J)=XVAR(J)+Y(I,J)*X(I,J)
0035
                 70 CONTINUE
0036
```

RETURN

FORTRAN IV G COMPILER

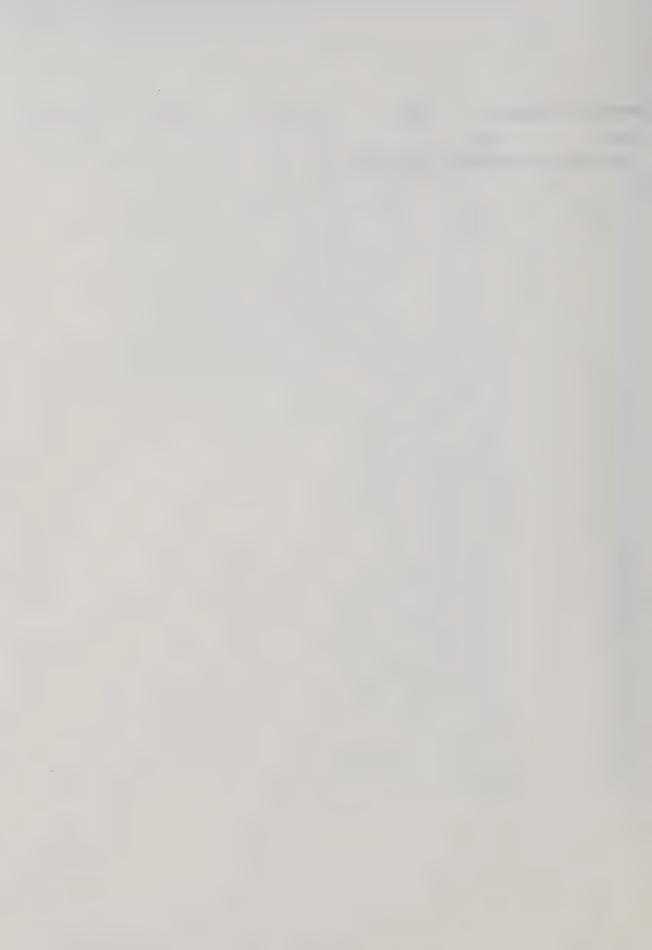
DATA

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0038

END

TOTAL MEMCRY REQUIREMENTS 000730 BYTES



VF=(2.0*(MI-1.0)*(MJ*MI-MJ-2.0))/((MI-5.0)*(MJ-1.0)*(MI-3.0)**2)

ALPHA=HOM/SAT

WRITE(6,102) SAT, HOM, ALPHA

IF(MI.LE.5) GO TO 90

0027

0028

0029

			- 7		t	
	t					U, ")
				1 2	. 2,	i e
†		٩	0.7	ı		
	*					
						*
						1

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FORTRAN	I۷	C	COMPIL	ER EXAMPL	09-15-71	15:55.03	PAGE 0002
0031				VARA=VF*(1-REL)**2 VARE=VF*(1-AL)**2			
0033				WRITE(6,104) VARA, VARE			
0034	•			C2=(MI-3.0)/(MI-1.0)			
0035				VARA=VARA+C2+C2 VARE=VARE+C2+C2			
0037				WRITE(6, 105) VARA, VARE			
0038			90	RETURN			
0039				END			
TOTAL	MEN	ICF	Y REQU	JIREMENTS 000A58 BYTES			



```
FORTRAN IV G COMPILER
                               ITEMCO
                                                09-15-71
                                                                  15:55.06
                                                                                  PAGE 0001
0001
                    SUBROUTINE ITEMCO(X,Y,RXY,D1,D2,COV)
              C
                  PURPOSE
                                  CALCULATE INTER-ITEM COVARIANCE FOR RELOZ BASED ON
              C
                                  TCHEBYCHEFF-HERMITE POLINOMIALS UNDER NORMAL OGIVE
              C
                                  MODEL
              C
                       Х
                                  THRESHOLD CONST FOR FIRST ITEM
              C
                       Υ
                                  THRESHOLD CONST FOR SECOND ITEM
              C
                       RXY
                                  INTER ITEM TETRACHORIC CORRELATION
              C
                       D1
                                  NORMAL DENSITY AT Z=X
              C
                                  NORMAL DENSITY AT Z=Y
                       D2
              C
                       COV
                                  OUTPUT COVARIANCE
              C
               200 FORMAT(1X, 13, E16.8)
0002
                    REAL*8 X1, X2, Y1, Y2, RRR, DDD, RN, U, V, X3, Y3, DD2, FI
0003
                    U = X
0004
                    V = V
                    X1=1.0
0005
0006
                    X2=X
0007
                    Y1=1.0
0008
                    Y2=Y
0009
                    FI=2.0
0010
                    RN=DLOG(FI)
                    RRR=RXY
0011
                    DDD=RRR+(U*V*RRR*RRR)/2.0
0012
0013
                    RRR=DLCG(RRR)
0014
                    DO 10 I=3,20
                    FI=I
0015
0016
                    X3=U*X2-(FI-2.0)*X1
0017
                    X1 = X2
                    X2=X3
0018
                    Y3=V*Y2-(FI-2.0)*Y1
0019
                    Y1=Y2
0020
                    Y2=Y3
0021
                    RN=RN+DLOG(FI)
0022
                    DD2=X3*Y3*(DEXP(FI*RRR-RN))
0023
                    000=000+002
0024
                    COV=DDD*D1*D2
             C
                    WRITE(6,200) I,COV
0025
                 10 CONTINUE
                    CCV=DDD*D1*D2
0026
                    RETURN
0027
                    END
0028
```

TOTAL MEMORY REQUIREMENTS 000386 BYTES



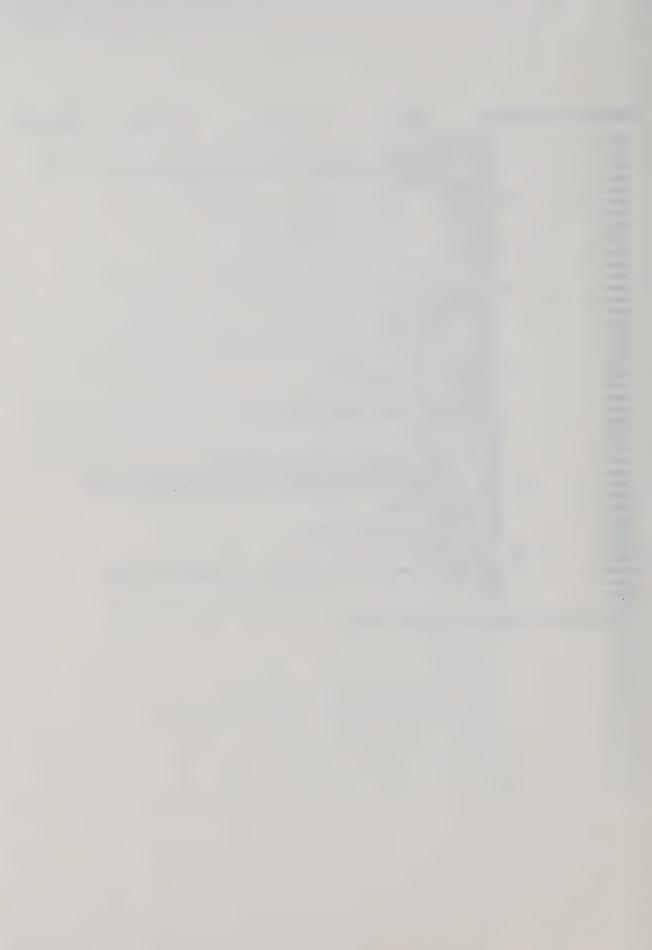
```
FORTRAN IV G COMPILER
                                PARALL
                                                  09-15-71
                                                                   15:55.07
                                                                                    PAGE 0001
0001
                     SUBROUTINE PARALL(R, XBAR, MI, MJ, NSAM, XVAR, FC, FERR, COR)
              C
                  PURPOSE
                                   CALCULATE TEST VARIANCE AND COVARIANCE BY PARALLEL
              C
                                   METHOD
              C
                                   INPUT INTER ITEM SUM OF PRODUCTS
              C
                                   INPUT SUM OF ITEM SCORES
                        XBAR
              C
                        MI
                                   SAMPLE SIZE
              C
                        MJ
                                   NO OF ITEMS IN THE TEST
                        NSAM
                                   NO OF SIMULATION RUNS
              C
                        XVAR
                                   SUM OF PRODUCTS OF PARALLEL ITEMS
              C
                                   DUTPUT TRUE SCORE VARIANCE
                        FC
              C
                        FERR
                                   OUTPUT ERROR SCORE VARIANCE
              C
                        COR
                                   OUTPUT RELIABILITY BETWEEN PARALLEL TESTS
              C
                     DIMENSION R(MJ*(MJ+1)/2), XBAR(2*MJ)
0002
                     DIMENSION R(1), XBAR(1), XVAR(MJ)
0003
                100 FORMAT(1H1,60('a')/,1X,'a',2X, 'ESTIMATION OF POPULATION PARAMETERS
                    1 BY PARALLEL METHOD', 2X, 00', /, 1X, 60('0'), /, 1X, 0 MEAN', 16X, E14.6, /,
                   21X, "VARIANCE", 12X, E14.6, /, 1X, "TRUE VARIANCE", 7X, E14.6, /, 1X, "ERROR
                   3VARIANCE , 6X, E14.6, /, 1X, RELIABILITY, 10X, F9.6, /, 1X, KR20, 17X,
                    4F9.6,/,1X, 'NO OF CASES',11X,18)
0004
                    NNN=(NSAM+1)*MI
0005
                     DEN=NNN-1.0
0006
                    FC=0.0
                    FV=0.0
0007
8000
                    FD=0.0
0009
                     IR=0
0010
                    DO 15 J=1, MJ
                    DO 14 K=1, J
0011
0012
                     IR=IR+1
                     R(IR) = (R(IR) - (XBAR(K) * XBAR(J)) / NNN) / DFN
0013
                    FV=FV+R(IR)
0014
0015
                 14 CONTINUE
0016
                    FD=FD+R(IR)
0017
                     L+LM=LL
                    XVAR(J) = (XVAR(J) - (XBAR(J) * XBAR(JJ) / NNN)) / DFN
0018
                    FC=FC+XVAR(J)
0019
0020
                 15 CONTINUE
                    FC=2.0*(FV-FD)+FC
0021
                    FV=2.0*(FV-FD)+FD
0022
                    F20=(*J*(1.0-FD/FV))/(MJ-1.0)
0023
                    FMEAN=0.0
0024
                    DO 20 J=1, MJ
0025
                    XBAR(J)=XBAR(J)/NNN
0026
                 20 FMEAN=FMEAN+XBAR(J)
0027
                    COR=FC/FV
0028
                    FFRR=FV-FC
0029
                    WRITE(6,100) FMEAN, FV, FC, FERR, COR, F20, NNN
0030
                    CALL VEOUT (XBAR, MJ, 12, 12HMEAN VECTOR )
0031
                    CALL VEGUT (XVAR, MJ, 28, 28 HPARALLEL ITEM COVARIANCES
0032
                    CALL MXOUTIR, MJ, NJ, 1, 32, 32 HWITHIN TEST DISPERSION MATRIX
0033
                    RETURN
0034
0035
                    END
```

TOTAL MEMCRY REQUIREMENTS CC0692 BYTES



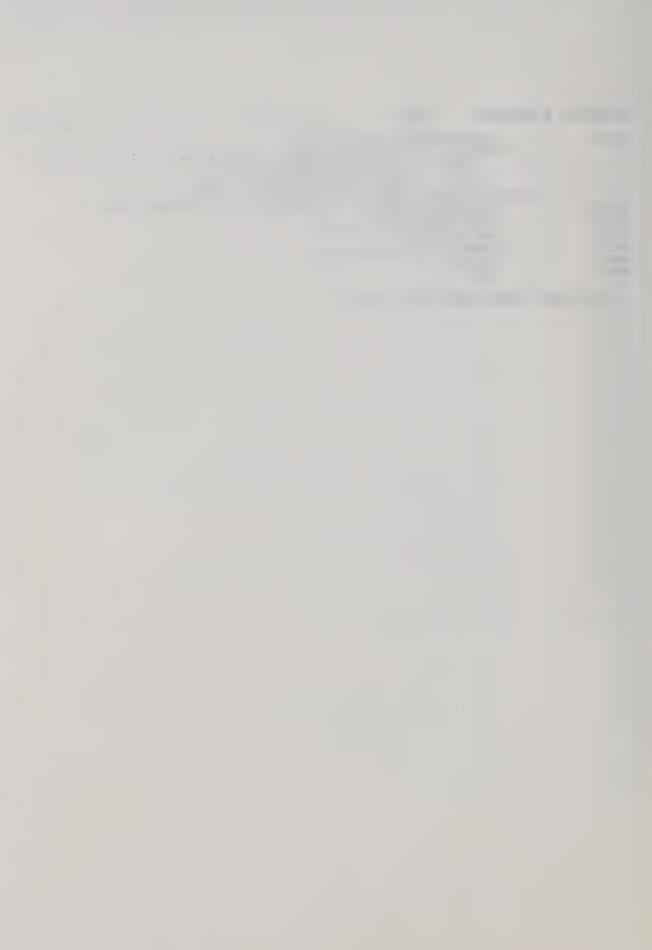
```
FORTRAN IV & COMPILER
                               POPR
                                                 09-15-71
                                                                  15:55.08
                                                                                  PAGE 0002
 0033
                    00 30 I=1,J
 0034
                    RXY=BS(I)*BS(J)
 0035
                    CALL ITEMCO(RR(I), RR(J), RXY, TEMP(I), TEMP(J), DIS(I, J))
 0036
                    DIS(J,I)=DIS(I,J)
               . 30 CONTINUE
 0037
 0038
                 31 CONTINUE
 0039
                    SUM=0.0
 0040
                    C0V=0.0
 0041
                    SSS=0.0
 0042
                    REL=0.0
 0043
                    DO 33 J=1, MJ
 0044
                    DO 32 K=1,J
 0045
                 32 REL=REL+DIS(K, J)
0046
                    SUM=SUM+DIF(J)
                    TEMP(J)=DIS(J,J)
 0047
 0048
                    COV=COV+TEMP(J)
0049
                    DIS(J,J)=PP(J)
0050
                    SSS=SSS+PP(J)
0051
                 33 CONTINUE
                    TVAR=2.0*(REL-COV)+SSS
0052
                    REL=REL*2-COV
0053
0054
                    REL=REL/TVAR
                    ALPHA=(MJ*(1.0-SSS/TVAR))/(MJ-1.0)
0055
                    SSS=TVAR*REL
0056
0057
                    EVAR=TVAR-SSS
0058
                    WRITE(6,101)
                    WRITE(6,102) SUM, TVAR, SSS, EVAR, REL, ALPHA
0059
                    CALL VEOUT(TEMP, MJ, 28, 28 HPARALLEL ITEM COVARIANCES
0060
0061
                    CALL MXOUT (DIS, MJ, MJ, 0, 28, 28 HINTER ITEM DISPERSION MATRIX)
0062
                    00 51 J=1, MJ
                    PP(J)=SQRT(PP(J))
0063
                    DO 50 K=1,J
0064
                    R(J,K) = DIS(J,K)/(PP(J)*PP(K))
0065
                 50 R(K,J)=R(J,K)
0066
                 51 CONTINUE
0067
                    CALL MXOUT(R.MJ,MJ,0,32,32HINTER ITEM CORRELATION MATRIX
0068
0069
                    RETURN
                    END
0070
```

TOTAL MEMCRY REQUIREMENTS OCODAE BYTES



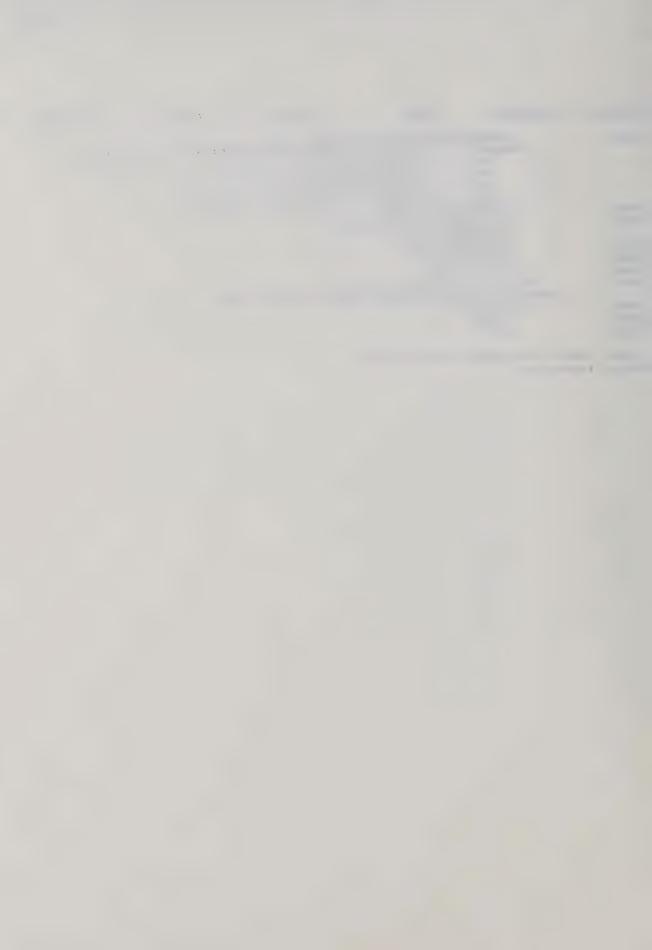
FORTRAN IV	G COMPILER	DIST	09-15-71	15:55.13	PAGE 0001		
0001	C PURPOSE C TEMP C MI C IX	OUTPUT SAMPLE SEED OF	STANDARD RANDOM TRUE SCORE VECTO SIZE, LENGTH OF DO INTEGER RANDOM	TEMP			
0002	DIMENSIO	TEMP(MI)					
0003	CALL VECRAN(TEMP, MI, IX)						
0004	CO 10 I=1, MI						
0005	10 TEMP(I)=-	-ALCG(TEMP()	[]]-1.0				
0006	RETURN						
0007	END						

TOTAL MEMCRY REQUIREMENTS 0001D4 BYTES



```
FORTRAN IV G COMPILER
                              DISE
                                                09-15-71
                                                                               PAGE 0001
                                                                15:55.13
0001
                    SUBROUTINE DISE(Y, MI, MJ, IX)
                                CREATE STANDARD RANDOM ERROR MATRIX Y FOR RELOZ
GUTPUT MATRIX
             C
                  PURPOSE
             C
                       Υ
             C
                       MI
                                  NO OF ROWS OF Y
             С
                       MJ
                                  NO OF CCLS OF Y
             C
                       IX
                                  SEED ODD INTEGER RANDOM NUMBER
                    DIMENSION Y(MI, MJ)
 0002
0003
                    CALL VECRAN(Y, (MI*MJ), IX)
             C
                    SQR=SQRT(12.0)
0004
                    SQR=SQRT(12.0)
                    DO 20 J=1, MJ
0005
                    DO 10 I=1, MI
0006
                 10 Y(I,J)=(Y(I,J)-0.5)*SQR
0007
             C****THIS EXAMPLE PRODUCES UNIFORM ERROR SCORES
0008
                 20 CONTINUE
0009
                    RETURN
                    END
0010
 TOTAL MEMCRY REQUIREMENTS 000264 BYTES
```

15:55.14 14.494 RC=0



SUBROUTINE PACKAGE RELOO



```
FORTRAN IV G COMPILER
                             ANOV
                                                09-15-71
                                                                 15:55.18
                                                                                 PAGE 0001
0001
                    SUBROUTINE ANOV(Y, MI, MJ, FMSA, FMSB, FMSE, BB)
             C
                  PURPOSE
                                  CALCULATE MEAN SQUARES AND PART-TSEST MEANS FOR RELOI
             C
                       Υ
                                  INPUT DATA MATRIX
             C
                       MI
                                  SAMPLE SIZE
             C
                                  NO OF PARTS
                       MJ
                                  MEAN SQUARES FOR SUBJECT EFFECTS
             C
                       FMSA
             C
                       FMSB
                                  MEAN SQUARES FOR ITEM EFFECTS
             C
                                  MEAN SQUARES FOR ERRORS
                       FMSE
                                  OUTPUT ITEM MEAN VECTOR
             C
                       BB
 2000
                    DIMENSION Y(MI, MJ), 88(MJ)
0003
                    S1=0.0
0004
                    S2=0.0
0005
                    $3=0.0
0006
                  · $4=0.0
                    DO 15 I=1, MI
0007
0008
                    FMSA=0.0
                    CO 12 J=1.MJ
0009
0010
                 12 FMSA=FMSA+Y(I,J)
                    S4=S4+FMSA
0011
                 15 S2=S2+FMSA**2
0012
0013
                    FMSB=S4/(MI*MJ)
0014
                    S2=S2/MJ
                    S4=(S4*S4)/(MI*MJ)
0015
                    DO 30 J=1, MJ
0016
0017
                    FMSA=0.0
                    DO 25 I=1, MI
0018
                    S1=S1+Y(I, J) **2
0019
0020
                 25 FMSA=FMSA+Y(I,J)
                    BB(J)=FMSA/MI-FMSB
0021
                    S3=S3+FMSA**2
0022
                 30 CONTINUE
0023
                    S3=S3/MI
0024
                    FMSA=(S2-S4)/(MI-1.0)
0025
                    FMSB=(S3-S4)/(MJ-1.0)
0026
                    FMSE=(S1-S2-S3+S4)/((MI-1.0)*(MJ-1.0))
0027
                    RETURN
0028
```

END TOTAL MEMORY REQUIREMENTS 0004CA BYTES

```
FORTRAN IV G COMPILER
                              BOXSN
                                               09-15-71
                                                                15:55.19
                                                                                PAGE 0001
0001
                    SUBROUTINE BOXSN(Z,N,IX)
                 PURPOSE
             C
                                 GENERATE STANDARD RANDOM NORMAL VECTOR
             C
                       Z
                                 OUTPUT VECTOR OF RANDOM NUMBERS
                                 LENGTH OF Z
             C
                       N
             C
                       IX
                                  SEED ODD INTEGER RANDOM NUMBER
             CC
                  SUBPROGRAMS
                                  VECRAN
                  METHOD
                                  BOX-MULLER, ANN. MATH. STAT. 1959
             C
                    DIMENSION Z(2*NN) NN=(N+1)/2
0002
                    DIMENSION Z(1)
0003
                    PAI=6.283185307
                    NN = (N+1)/2
0004
0005
                    CALL VECRAN(Z, (NN*2), IX)
                    DO 20 I=1,NN
0006
                    XX=PAI*Z(1)
0007
                    II = I + NN
8000
0009
                    YY=SQRT(-2.0*ALOG(Z(II)))
0010
                    Z(I)=YY*COS(XX)
                    Z(II)=YY*SIN(XX)
0011
                 20 CONTINUE
0012
0013
                    RETURN
                    END
0014
```

TOTAL MEMCRY REQUIREMENTS 00027E BYTES



```
FORTRAN IV G COMPILER
                               CHIPRB
                                                09-15-71
                                                                 15:55-20
                                                                                 PAGE 0001
 0001
                    FUNCTION CHIPRB (CHI, NDF)
             C
                  PURPOSE
                                  CALCULATE PROBABILITY OF CHI-SQUARE VARIATE EXCEEDING
             C
                                  INPUT VALUE
              C
                       CHI
                                  INPUT VALUE
              C
                       NDF
                                  DEGREES OF FREEDOM
              C
                  PROGRAMMER
                                  D. FLATHMAN
                    EXTERNAL ERF, SQRT
 0002
 0003
                    REAL NORMAL
 0004
                    INTEGER F
 0005
                    LOGICAL BIGX, EVEN
 0006
                    NORMAL(X)=0.5*(1.0+ERF(0.7071068*X))
 0007
                    F=NOF
 8000
                    X=CHI
 0009
                    CHIPRB=1.0
 0010
                    IF(X.LE.O..OR.F.LT.1) RETURN
                    A=0.5*X
 0011
 0012
                    BIGX=A.GT.10.
                    EVEN=(2*(F/2)-F).EQ.0
 0013
0014
                    IF(EVEN.OR.(F.GT.2.AND..NOT.BIGX)) Y=EXP(-A)
0015
                    IF(EVEN) S=Y
                    IF(.NOT.EVEN) S=2.0*NORMAL(-SQRT(X))
 0016
                    CHIPRB=S
0017
                    IF(F.LE.2) RETURN
 0018
 0019
                    X=0.5*(F-1.0)
                    IF(EVEN) Z=1.0
0020
0021
                    IF(.NOT.EVEN) Z=0.5
                    IF(.NOT.BIGX) GO TO 2
0022
 0023
                    IF(EVEN) E=0.
                    IF(.NOT.EVEN) E=0.5723649
0024
                    C=ALOG(A)
0025
                    E=ALOG(Z)+E
0026
               1
                    S = EXP(C*Z-A-E)+S
0027
                    Z=Z+1.0
0028
                    IF(Z.LE.X) GO TO 1
0029
0030
                    CHIPRB=S
                    RETURN
0031
                    IF(EVEN) E=1.0
0032
               2
                    IF(.NOT.EVEN) E=0.5641896/SQRT(A)
0033
                    C=0 .
0034
                    E=E*A/Z
0035
              3
                    C=C+E
0036
0037
                    Z=Z+1.0
                    IF(Z.LE.X) GO TO 3
0038
                    CHIPRB=C*Y+S
0039
                    RETURN
0040
0041
                    END
```

TOTAL MEMCRY REQUIREMENTS 00055E BYTES



```
FORTRAN IV & COMPILER
                               COUNT
                                                09-15-71
                                                                  15:55.23
                                                                                  PAGE 0001
 0001
                    SUBROUTINE COUNT(X, LX, NV, XMIN, TINT, LB, FREQ, XBAR, XVAR)
              C
                  PURPOSE
                                  CALCULATE FREQUENCY DISTRIBUTIONS
              C
                        Х
                                   INPUT DATA MATRIX
              C
                       LX
                                  NO OF OBSERVATIONS
              C
                        NV
                                  NO OF VARIABLES
              Č
                        MIMX
                                   INPUT MINIMUM VALUE ASSUMED
              C
                        TINT
                                   INPUT CLASS INTERVAL
              C
                                   INPUT NO OF CLASS INTERVALS
                       LB
                       FREQ
                                  OUTPUT FREQUENCY DISTRIBUTIONS
              С
                       XBAR
                                  OUTPUT MEAN VECTOR
              C
                        XVAR
                                  OUTPUT VARIAGE VECTOR
 0002
                    DIMENSION X(LX,NV), FREQ(LB,NV), XBAR(NV), XVAR(NV)
 0003
                    SJAX=XMIN+TINT*L8
 0004
               100 FORMAT(/,1X, MAXIMUM=",E14.6,3X, MINUMUM=",E14.6,3X, CLASS INTERVA
                   1L=1.E14.6)
 0005
                    WRITE(6,100) XMAX, XMIN, TINT
 0006
                    DO 15 J=1,NV
 0007
                    CO 10 I=1, LB
 8000
                 10 FREQ(I, J)=0.0
                    XBAR(J)=0.0
 0009
 0010
                 15 XVAR(J)=0.0
 0011
                    DO 80 J=1,NV
 0012
                    DO 70 I=1,LX
                    XBAR(J)=XBAR(J)+X(I,J)
0013
                    XVAR(J) = XVAR(J) + X(I,J) * X(I,J)
0014
 0015
                    XXL=XMIN
                    DO 60 K=1, LB
0016
0017
                    XXU=XXL+TINT
                    IF(X(I,J).GE.XXL.AND.X(I,J).LT.XXU) GO TO 68
0018
0019
                 60 XXL=XXU
                    GO TO 70
 0020
                 68 FREQ(K, J)=FREQ(K, J)+1.0
 1500
 0022
                 70 CONTINUE
0023
                 80 CONTINUE
                    CALL VARXX(LX, NV, XBAR, XVAR)
0024
                    CALL MXOUT (FREQ, LB, NV, 0, 24, 24HFREQUENCY DISTRIBUTIONS )
             C
0025
                    RETURN
                    END
0026
```

TOTAL MEMORY REQUIREMENTS 00055A BYTES



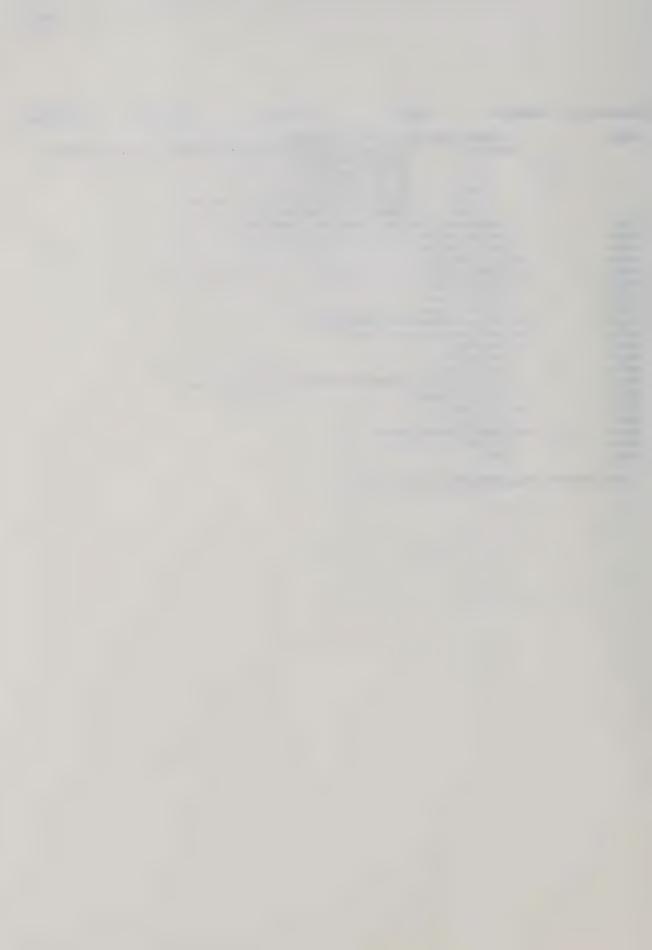
```
FORTRAN IV G COMPILER
                                CISCRP
                                                 09-15-71
                                                                                   PAGE 0001
                                                                   15:55.24
 0001
                     SUBROUTINE DISCRP(N, XBAR, XVAR, LAB, NUMHOL, TITLE)
                  PURPOSE
              C
                                   OUTPUT DISCRIPTIVE TABLE
              C
                        N
                                   NO OF VARIABLES
              CC
                        XBAR
                                   MEAN VECTORS
                        XVAR
                                   VARIANCES
              C
                        LAB
                                   LABELS
              C
                        NUMHOL
                                   NO OF CHARACTERS IN TITLE(MULTIPLE OF 4)
                        TITLE
                                   TITLE OF THE TABLE
                100 FORMAT(1HO, DESCRIPTIVE STATISTICS FOR 1,20A4)
 0002
                101 FORMAT(1H0,20X, "MEAN", 15X, "|", 10X, "VARIANCE", /, 1X, 11X, "OBSERVED",
 0003
                    17X, 'EXPECTED', 5X, '|', 5X, 'OBSERVED', 8X, 'EXPECTED')
                102 FORMAT(1X, A8, 1X, 2E14.6, 2X, 1, 3X, 2E14.6)
 0004
 0005
                     DIMENSION XBAR(N), XVAR(N), LAB(N), TITLE(20)
 0006
                     REAL*8 LAB
 0007
                     NN=(NUMHCL+3)/4
                     WRITE(6,10C) (TITLE(J),J=1,NN)
 0008
 0009
                     WRITE(6,101)
 0010
                     DO 10 I=1,N
 0011
                     II = I + N
                     WRITE(6,102) LAB(I), XBAR(I), XBAR(II), XVAR(II), XVAR(II)
 0012
                 10 CCNTINUE
 0013
 0014
                     RETURN
                     END
 0015
```

TOTAL MEMORY REQUIREMENTS 000368 BYTES

. . .

```
FORTRAN IV G COMPILER
                                CISP
                                                  09-15-71
                                                                    15:55.26
                                                                                     PAGE 0001
0001
                     SUBROUTINE DISP(Y, MI, MJ, S, XBAR)
              C
                   PURPOSE
                                   CALCULATE SAMPLE DISPERSION MATRIX AND MEAN VECTOR
              C
                        Υ
                                    INPUT DATA MATRIX
              CCCC
                        MI
                                   NO OF RCWS OF Y
                        MJ
                                    NO OF COLS OF Y
                        S
                                   OUTPUT SAMPLE DISPERSION MATRIX
                        XBAR
                                    SAMPLE MEAN VECTOR
 0002
                     DIMENSION Y(MI, MJ), S(MJ, MJ), XBAR(MJ)
0003
                     DO 15 J=1, MJ
                     00 10 K=1, MJ
0004
                  10 S(K, J)=0.0
0005
0006
                  15 XBAR (J)=0.0
0007
                     DO 30 I=1, MI
8000
                     00 25 J=1, MJ
0009
                     CO 20 K=1,J
                 20 S(K, J) = S(K, J) + Y(I, K) * Y(I, J)
0010
                  25 XBAR(J) = XBAR(J) + Y(I, J)
0011
                  30 CONTINUE
0012
0013
                     00 50 J=1, MJ
                     DO 45 K=1,J
0014
                     S(K_{*}J) = (S(K_{*}J) - (XBAR(K) * XBAR(J)) / MI) / (MI-1.0)
0015
                  45 S(J,K) = S(K,J)
0016
0017
                  50 CONTINUE
                     DO 60 J=1, MJ
0018
                  60 XBAR(J)=XBAR(J)/MI
 0019
0020
                     RETURN
0021
                     END
```

TOTAL MEMCRY REQUIREMENTS OCO4FE BYTES



FORTRAN	I۷	G	COMPILE	R	FISHER	09-15-71	15:55.28	PAGE 0001
0001					INPUT NUM	ABILITY LEVEL WI BERATOR D.F. OMINATOR D.F.	TH GIVEN D.F. AN	D F-RATIO
0002				ORMAT(/	,/,1H0, *ERROR	IN FUNCTION FISH	HER: AN INPUT PARA	METER IS INV
0003			101 F	ORMAT(1	X, INPUT F-RAT	TO IS LESS THAN	0.0 F=*,E16.8)	
0004		٠	102 F		X, "NUMERATOR D		1.0 CR GREATER	THAN 200,000
0005				ORMAT (1	•	D.F.IS LESS THA	N 1.0 OR GREATER	THAN 200,00
0006							IS INVALID DUE TO SET AS TO -1.0E75	
0007						ALULATING GAMMA		
0008		•		=DFM/2.				
0009			8	=DFN/2.	0			
0010			F	B= ((DFM	*FR)/DFN)/(1.0	+(DFM*FR)/DFN)		
0011			(CALL BOT	R(FB,A,B,PRO,D	, IER)		
0012			1	F(IER.E	Q2) WRITE(6,	100)		
0013			1	F(FR.LT	.0.0) WRITE(6,	101) FR		
0014						T.200000) WRITE(
0015						T.200000) WRITE	(6,103) DFN	
0016					Q.2) WRITE(6,1			
0017						1.1) WRITE(6,105))	
0018				ISHER=1	.O-PRO			
0019			f	RETURN				
0020			8	ND				

TOTAL MEMORY REQUIREMENTS 0004FO BYTES



```
FORTRAN IV G COMPILER
                               FITTES
                                                 09-15-71
                                                                  15:55.30
                                                                                   PAGE 0001
0001
                     SUBROUTINE FITTES(X, N, NT)
              C
                  PURPOSE
                                  PERFORMS CHI-SQUARE GOODNESS OF FIT TEST
              C
                                   INPUT FREQUNCY MATRIX
                       X
              C
                                   COL-1 EXPECTED FREQUENCIES
              C
                                  COL-2 OBSERVED FREQUENCIES
              C
                        N
                                   NO OF CLASS INTERVALS OR NO OF THE ROW OF X
              C
                        NSAM
                                   SAMPLE SIZE
              C
                  SUBPROGRAM
                                   CHIPRB
0002
                    CIMENSION X(N,2)
0003
                100 FORMAT(/,1x, CHI-SQ GOODNESS OF FIT TEST: ,3x, CHI=, ,E14.6, 3x, NDF
                   1=', 15, 3X, 'PROB=', F8.4)
 0004
                    CHI=0.0
0005
                    NDF=0
                    XT=0.0
0006
0007
                    YT=0.0
 8000
                    1=1
0009
                 12 XX=0.0
0010
                    YY=0.0
0011
                 15 YY=YY+X(I,2)
0012
                    XX=XX+X(I,1)
0013
                     IF(XX.GE.5.0) GO TO 16
0014
                    I = I + 1
                    IF(I.LE.N) GO TO 15
              C
                    GO TO 15
0015
 0016
                 16 NDF=NDF+1
                    CHI=CHI+((XX-YY)**2)/XX
 0017
0018
                    XT = XT + XX
0019
                    YT = YT + YY
0020
                    XR=NT-XT
                    I = I + 1
0021
                    YR=NT-YT
0022
                    IF(XR.GE.10.0.AND.I.LE.N) GO TO 12
              C
                    IF(XR.GE.10.0) GO TO 12
0023
                    IF(XR.GT.0.0) GO TO 20
0024
                    NDF=NDF-1
0025
                    GO TO 25
0026
                 20 CHI=CHI+((XR-YR)**2)/XR
0027
                 25 PRO=CHIPRB(CHI, NDF)
0028
0029
                    WRITE(6,100) CHI, NDF, PRO
0030
                    RETURN
0031
                    END
```

TOTAL MEMCRY REQUIREMENTS 0003CC BYTES

```
FORTRAN IV & COMPILER
                               FST
                                                09-15-71
                                                                                 PAGE 0001
                                                                 15:55.31
 0001
                    FUNCTION FST(DF1,DF2,P,PRE)
              C
                    PURPOSE
                                  CALCULATE F STATISTICS WHEN DEGREES OF FREEDOM AND
              C
                                  PROBABILITY ARE GIVEN
              C
                        DF1
                                  DEGREES OF FREEDOM FOR NUMERATOR
              C
                        DF2
                                  DEGREES OF FREEDOM FOR DENOMINATOR
              Č
                       P
                                  PROBABILITY LEVEL
              C
                       PRE
                                  PRECISION LEVEL FOR OUTPUT F RATIO
                    SUBPROGRAM
                                  FISHER
 0002
                    IF (DF1.LE.O.O.OR.DF2.LE.O.O.OR.P.LE.O.O) GO TO 999
                100 FORMAT (1HO, DEGREES OF FREEDOM OR PROBABILITY IS LESS OR EQUAL
 0003
                   1TO ZERO RETURNS TO MAIN WITH FST=0.0')
 0004
                    X1 = 1.0
 0005
                    X2 = 0.0
 0006
                 10 F=(X1+X2)/2.0
 0007
                    FR = DF2 * ((1.0 - F) / (DF1 * F))
                    PRO=FISHER(OF1, DF2, FR)
 8000
 0009
                    ER=P-PRO
              C 101 FORMAT(1X, 4F12.6)
                    WRITE(6,101) F, FR, PRC, ER
                    IF (ABS(ER) . LE. PRE)
                                         GO TO 99
 0010
                    IF (P.LT.PRO) X1=F
 0011
                    IF(P.GT.PRC) X2=F
 0012
                    GO TO 10
 0013
 0014
                 99 FST=FR
                    RETURN
 0015
                999 WRITE(6,100)
 0016
                    FST=0.0
 0017
                    RETURN
 0018
 0019
                    END
```

TOTAL MEMCRY REQUIREMENTS 000330 BYTES



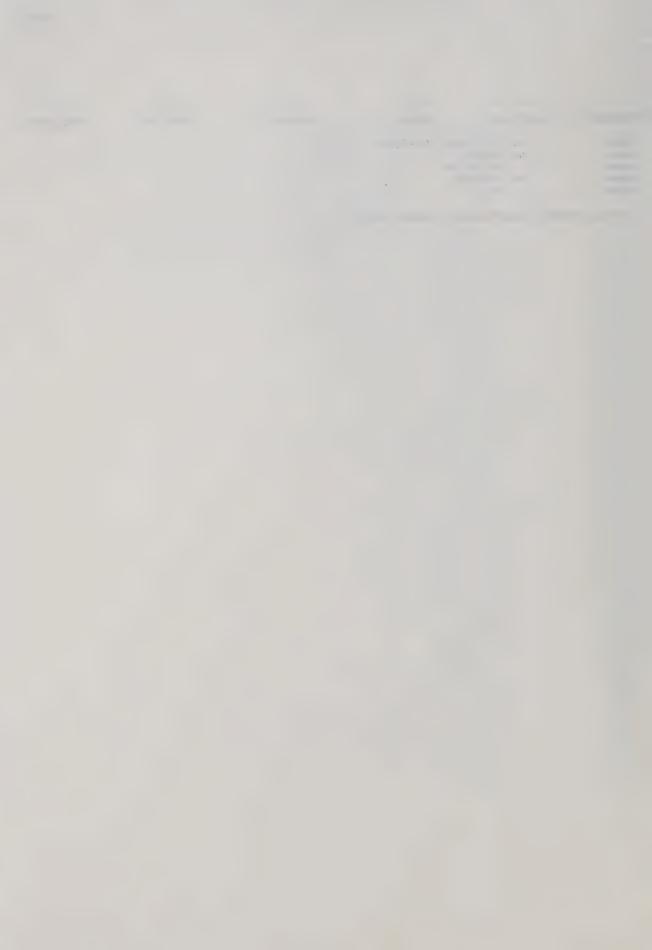
PAGE 0001



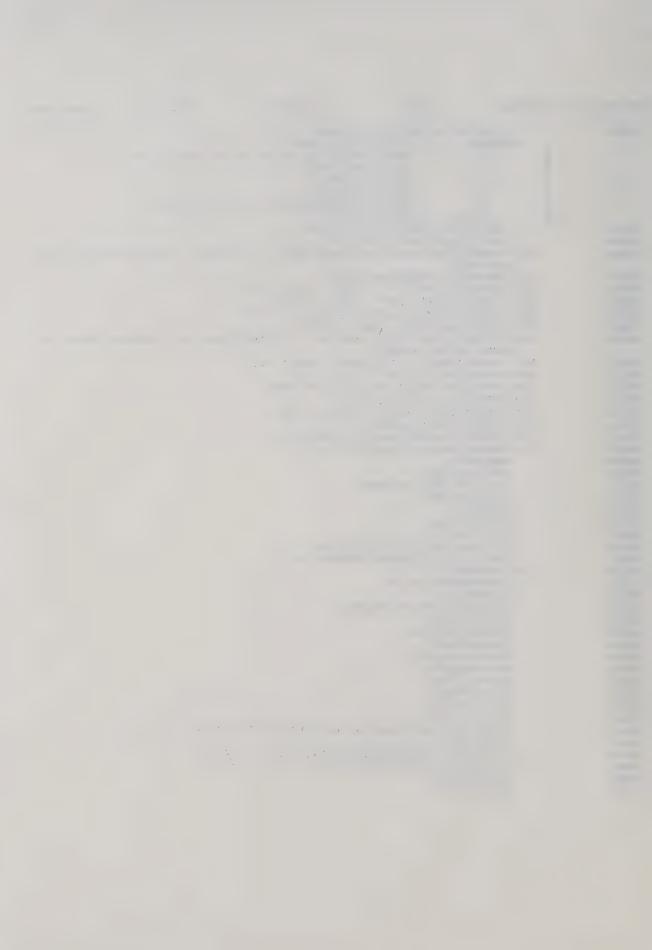
FORTRAN IV 6 COMPILER MXOUT 09-15-71 15:55.35 PAGE 0002

0046 85 IF(JT-M) 9C,95,95 0047 90 J=JT+1 0048 GO TO 10 0049 95 RETURN 0050 END

TOTAL MEMCRY REQUIREMENTS 0005A0 BYTES



```
FORTRAN IV G COMPILER
                               PLOT
                                                09-15-71
                                                                 15:55.37
                                                                                PAGE 0001
 0001
                    SUBROUTINE PLOT (X, A, N, NSAM)
                  PURPOSE
                                  GIVES PLOT FOR RELOI
              C
                       Х
                                  INPUT MATRIX OF RELATIVE FREQUENCIES(%)
             C
                                  COL-1 EXPECTED
             C
                                  COL-2 · OBSERVED
              C
                       A
                                  WORKING VECTOR
             C
                                  NO OF CLASSES (LIMITED TO 24,36 OR 48)
                       N
             C
                       NSAM
                                  SAMPLE SIZE
0002
                    DIMENSION X(N,2),A(N),SIG(4)
                    DATA SIG/ . . , * * , * + * , * + * , * * /
0003
0004
                100 FORMAT (1H1,34( °% ),/,1X, °% PLOT OF FREQUENCY DISTRIBUTION % ./.1X.
                   134('%'))
0005
                101 FORMAT(4x, *FREQUENCY(%)*)
0006
               102 FORMAT(1X, F7.3, *-|*,24(* *,A1, * *))
0007
                103 FORMAT(9X, 11, 24(1 , A1, 1
                                                 * ) )
                0008
                105 FORMAT (4X, 12(F7.1, 3X), F7.1)
0009
0010
                106 FORMAT(/,1X, "NOTE: ",3X,"(.) EXPECTED FREQ; (*) OBSERVED FREQ; (+)
                  10VERLAPPING POINT*)
0011
                107 FORMAT(1X, F7.3, '-| ', 36( ' ', A1, ' '))
                108 FORMAT(9X, 11, 36(1 1, A1, 1))
0012
                109 FORMAT(3X, 'REL', 3X, '|', 36('--|'))
0013
0014
                110 FORMAT (4X, 13(F7.1, 2X))
                111 FORMAT(1x, F7.3, *-| *, 48(A1, * *))
0015
               112 FORMAT(9X, 11, 48(A1, 1 1))
0016
                113 FORMAT(3X, 'REL', 3X, '| ', 48('-|'))
0017
0018
                114 FORMAT(4X,12(F7.1,1X),F7.1)
0019
                    NNN=N-36
0020
                    WRITE(6,100)
0021
                    CALL FITTES(X, N, NSAM)
0022
                    WRITE(6,101)
                    XMAX=0.0
0023
                    DO 10 I=1,N
0024
                    CO 10 J=1,2
0025
                    X(I,J) = (X(I,J) * 100.0) / NSAM
0026
                    IF(X(I,J).GT.XMAX) XMAX=X(I,J)
0027
0028
                 10 CONTINUE
                    NN=XMAX/10.0+1.0
0029
                    XU=NN*10.0
0030
                    IF(XU.GT.100.0) XU=100.0
0031
                    DELT=XU/50.0
0032
                    DELTH=DELT/2.0
0033
0034
                    XU=XU+DELTH
                    DO 50 I=1,10
0035
                    XM=XU-DELTH
0036
0037
                    DO 40 J=1,5
                    XL=XU-DELT
0038
                    DO 20 K=1, N
0039
                    A(K)=SIG(4)
0040
                    IF(X( K,1).GE.XU.OR.X( K,1).LT.XL) GO TO 12
0041 .
                    A(K)=SIG(1)
0042
                12 IF(X( K,2).GE.XU.OR.X( K,2).LT.XL) GO TO 20
0043
                    IF(A(K).EQ.SIG(1))GD TO 14
0044
                    A(K) = SIG(2)
0045
                   GO TO 20
0046
```



FORTRAN IV	G COMPI	LER	PLOT	09-15-71	15:55.37	PAGE 0002
0047 0048 0049 0050		A(K)=SIG(3 CONTINUE XU=XL IF(NNN) 25				
0051 0052 0053	25		WRITE(6,102)	XM, (A(K), K=1,N) (A(K), K=1,N)		
0054 0055 0056	30		WRITE(6,107) WRITE(6,108)	XM,(A(K),K=1,N) (A(K),K=1,N)		
0057 0058		IF(J.EQ.1) IF(J.GT.1)	WRITE(6,111) WRITE(6,112)	XM, (A(K), K=1,N) (A(K), K=1,N)		
0059 0060 0061		CONTINUE CONTINUE A(1)=-0.2				
0062 0063	5.1	DELT=0.1 CO 51 I=2				
0064 0065		A(I) = A(I-I) $IF(NNN) = 52$	2,54,56			
0066 0067 0068	52	WRITE(6,10 WRITE(6,10 GO TO 58)4))5)(A(I),I=1,1;	3)		
0069 0070	54)9) 10) (A(I),I=1,	13)		,
0071 0072 0073	56	GO TO 58 WRITE(6,1) WRITE(6,1)	(3). (4)(A(I),I=1,1)	3)		
0074 0075	58	CONTINUE WRITE(6,10 RETURN				
0076 0077		END				

TOTAL MEMCRY REQUIREMENTS 000874 BYTES



FORTRAN IV G COMPILER PUNCH 09-15-71 15:55.42 **PAGE 0001** 0001 SUBPOUTINE PUNCH(FREG, LB, NV) C PURPOSE GIVES CARD OUTPUT FOR RELOI C NO OF ROWS OF FREQ LB NO OF CCLS OF FREQ С NV 0002 DIMENSION FREQ(LB, NV) 100 FORMAT (12, 3X, 5F10.4) 0003 DO 20 I=1,LB 0004 0005 20 WRITE(7,10C) I, (FREQ(I,J), J=1,NV) 0006 RETURN END 0007

TOTAL MEMCRY REQUIREMENTS 000200 BYTES



25 PL=PU

0031

FORTRAN	I۷	G	COMPILER	RELDIS	09-15-71	15:55.42	PAGE	0002
0032			FRE	Q(LB,1)=NSAM*PL				
0033			CAL	L CCUNT(FMS(1,1),N	SAM, 1,-0.2, DELT,	LB, FREQ(1,2), XBAR	,XVAR)	
0034			XBA	R(2)=REL				
0035			IF(ID.EQ.0) $XBAR(2)=-$	2.0/(DFA-2.0)+(D	FA*REL)/(DFA-2.0)		
0036			XVA	R(2)=((1.0-REL)**2) *2.0 * (DF A* *2) * (DFE+DFA-2.0)		
0037			XVA	R(2)=(C2*C2*XVAR(2)) / (DFE* (DF A-4.0)*(DFA-2.0)**2)		
0038			CAL	L DISCRP(1, XBAR, XV	AR, LAB(4), 24, 24H	RELIABILITY ESTI	MATES 1)
0039			CAL	L MXOUT(FREQ, LB, 2,	0,28,28HC EMPARIS	ON OF RELIABILITY)	
0040			IF(IPUNCH.EQ.1) CALL	PUNCH (FREQ, LB, 2)			
0041			CAL	L SIGTES(FMS, NS AM,	DFA, DFE, SIG, REL,	ID)		
0042			IF(IPLOT.EQ.1) CALL P	LOT(FREQ, TEMP, L8	, NSAM)		
0043			RET	URN .				
0044			END					

TOTAL MEMCRY REQUIREMENTS 000898 BYTES



FORTRAN IV & COMPILER ROZB 09-15-71 15:55.46 **PAGE 0001** 0001 SUBROUTINE ROZB(DIS, MJ, SAT, HOM) C CALCULATE SATURATION AND HOMOGENEITY COEFFICIETS PURPOSE CC DIS INPUT DISPERSION MATRIX MJ SIZE OF DIS C SAT OUTPUT SATURATION COEFFICIENT С OUTPUT HOMOGENEITY COEFFICIENT 0002 DIMENSION DIS(MJ,MJ) 0003 TEMP=0.0 0004 0.0=MDH 00 20 J=1, MJ 0005 00 10 K=1, MJ 0006 0007 10 TEMP=TEMP+DIS(K,J) 0008 20 HCM=HOM+DIS(J.J) SAT=TEMP/(HOM*MJ) 0009 HOM=(TEMP-HOM)/(HOM*(MJ-1.0)) 0010 0011 RETURN END. 0012

TOTAL MEMCRY REQUIREMENTS 000288 BYTES



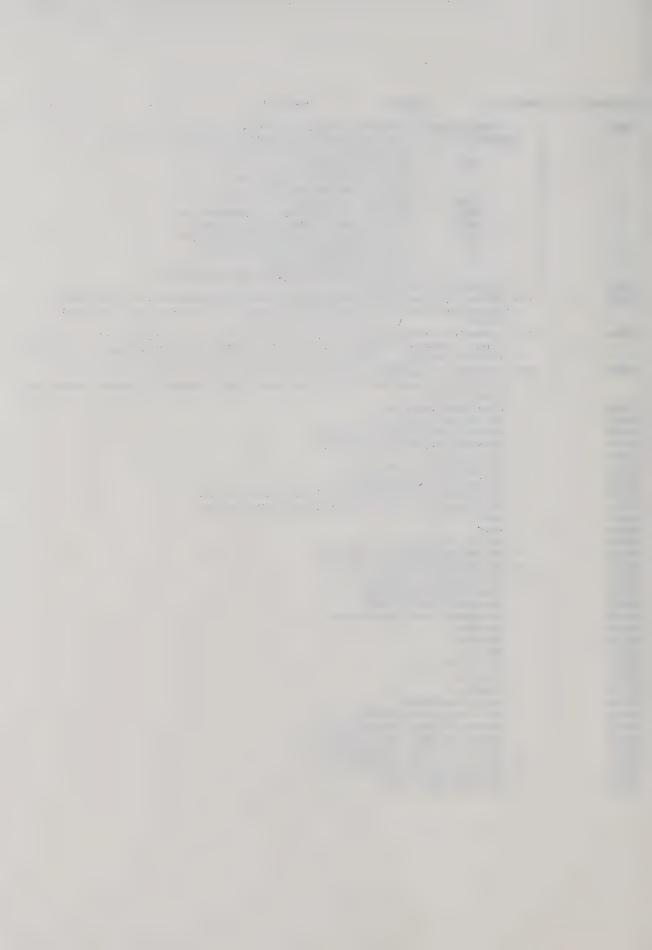
SU=(FNU+FNUU)/2.0

SL=(FNL+FNLL)/2.0

0035

0036

0037



FORTRAN IV & COMPILER

SIGTES

09-15-71

15:55.47 PAGE 0002

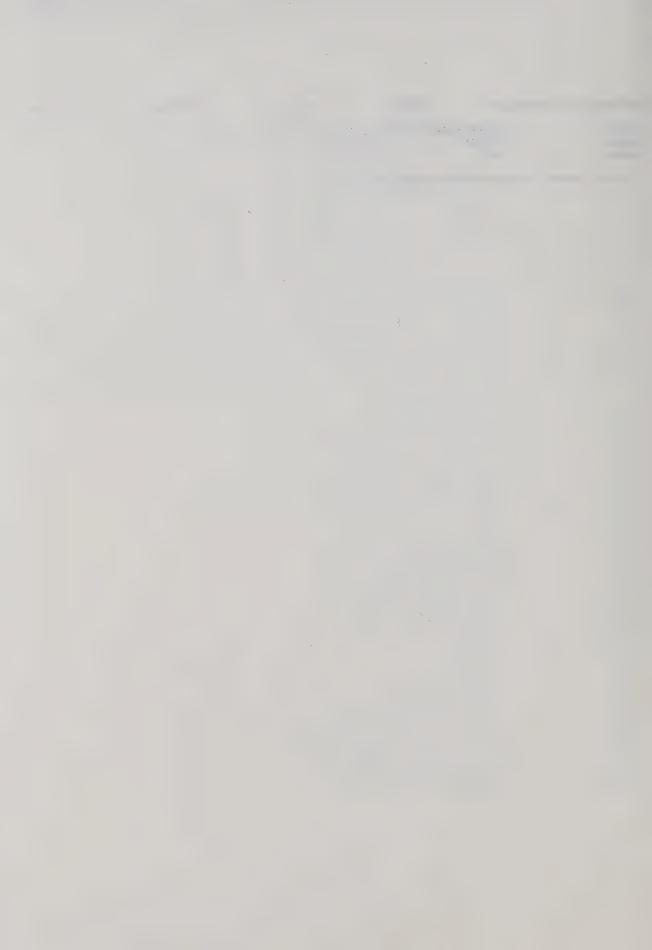
0038 0039

WRITE(6,102) ML, EML, MU, EMU, SL, SU RETURN

0040

END

TCTAL MEMORY REQUIREMENTS 000838 BYTES



FORTR AN	I۷	G	COMPIL	ER	VARXX		09-1	5-71	15:5	5.49	PAGE	0001
0001				SUBROUTINE								
				RPOSE	CALUCU	JLATE	MEANS	AND V	ARIANCE VEC	TORS		
			C	N	SAMPLE	SIZE						
			C	NV	NO OF	VARIA	BLES					
			C	XBAR	INPUT	SUM O	F VARI	ABLES	, REPLACED	BY MEANS		
			С	XVAR	INPUT	SUM DI	F SQUA	RES,	REPLACED BY	VARIANCES		
0002				DIMENSION	XBAR(NV);	XVAR (NV)					
0003				CO 10 J=1,	NV							
0004				XVAR(J)=()	(VAR(J)-()	(BAR (J	* XBAR	(3))/	N)/(N-1.0)			
0005			10	XBAR(J)=XB	AR(J)/N							
0006				RETURN								
0007				END								

TOTAL MEMCRY REQUIREMENTS 000222 BYTES



```
FORTRAN IV G COMPILER VECRAN
                                             09-15-71
                                                              15:55.50
                                                                             PAGE 0001
 0001
                   SUBROUTINE VECRAN(Z, N, IX)
             C
                 PURPOSE
                                COMPUTES N UNIFORM RANDOM NUMBERS BETWEEN 0.0 AND 1.0
                                 USING SSP RANDU METHOD
OUTPUT RANDOM VECTOR
             C
             C
                                 LENGTH OF Z
             C
                       N
             C
                      IX
                                SEED ODD INTEGER RANDOM NUMBER
                               NONE
                 SUBPROGRAM
                   DIMENSION Z(N)
 0002
 0003
                   DO 20 M=1.N
                  IX=IX*65539
 0004
 0005
                    IF(IX) 5,6,6
                 5 IX=IX+2147483647+1
 0006
 0007
                 6 Y= I X
                   Y=Y*.4656613E-9
 8000
                20 Z(M)=Y
 0009
 0010
                   RETURN
 0011
                    END
```

TOTAL MEMCRY REQUIREMENTS COOLFE BYTES



```
FORTRAN IV & COMPILER
                                VEOUT
                                                  09-15-71
                                                                    15:55.50
                                                                                    PAGE 0001
 0001
                     SUBROUTINE VEOUT (A, N, NUMH, TITLE)
              C
                   PURPOSE
                                   PRINTS UP A VECTOR
              C
                        Α
                                   INPUT VECTOR
              C
                        N
                                   LENGTH OF A
              C
                        NUMH
                                   NO OF CHARACTERS IN TITLE (MULTIPLE OF 4)
              C
                        TITLE
                                   TITLE OF THE VECTOR
                     DIMENSION A(N), TITLE (20)
 0002
 0003
                 100 FORMAT (/, 1X, 20A4)
 0004
                101 FORMAT(1X, 10(5X, 12,6X))
                 102 FORMAT(1X, 10E13.5)
 0005
 0006
                     NN=(NUMH+3)/4
 0007
                     WRITE(6,100) (TITLE(I), I=1,NN)
 0008
                     M=N
 0009
                     IF(N.GT.10) M=10
 0010
                     WRITE(6,101) (I,I=1,M)
                     WRITE(6,102) (A(I),I=1,M)
 0011
                     IF(N.LE.10) GO TO 30
 0012
                     WRITE(6,101) (I,I=11,N)
WRITE(6,102) (A(I),I=11,N)
 0013
 0014
                  30 RETURN
 0015
                     END
 0016
```

TOTAL MEMCRY REQUIREMENTS 000354 BYTES 15:55.52 17.673 RC=0



APPENDLX A.2

EXAMPLE OUTPUTS

RELO1 : Votaw-Jöreskog Example Data

RELO2 : Load-Novick Item Parameters



```
VOTAW-JORESKOG EXAMPLE DATA, CONGENERIC,N=2000,1=10,J=4,NORMAL

NO OF SUBJECTS IN EACH SAMPLE

NO OF PART-TESTS

NO OF FACTORS IN TRUE SCORE
STARTING INTEGER RANDOM NUMBER
OPTION FOR CARD OUTPUT
OPTION FOR PLOT
OPTION FOR THE NO OF CLASS INTERVALS
SIGNIFICANCE LEVEL
TRUE SCORE DISTRIBUTIONS ARE NORMAL

0.050
```



```
0.91478
                                                                                                                                                                                                                                                                                                                     0.51972
                                                                                                                                                                                                         0.121404E 02
0.120045E 02
0.205209E 02
HOMOGENEITY COEFF=
                                                                                                                                                                                                                                                                                                                    HOMOGENEITY COEF=
                                                                                                                                                                                                                                                                            0.207021E 02
0.121404E 02
0.120045E 02
0.218707E 02
                                                                                                                                                                                               0.207021E 02
0.121404E 02
                                                                                                                                                                                                                                                                      J
                                                                                                                                                                                                                                                                               002 002 002 002
                                                                                                                                                                                                                                                                                                                                                                                                                                        0.21871E 02
                                                                                                                                                                                                 02
01
01
02
                                                                                       01
                                                                                                                                                                                                                                                                     C- 3
0.121105E (
0.710200E (
0.227390E (
0.120045E
                                                                                                                                                                                                0.121105E
0.710200E
0.702250E
                                                                                                                                                                                                                              0.120045E
0.9360B
                                                                                                                                                                                                                                                                                                                     0.63979
                                                                                       0.11618E
                                                                                                                                                                                                                                                                                                                                                                                                           0.0
                                                                                                                                                                                                                                                                                                                                                          0.208225E 03
0.422714E 02
                                                          0.0
                                                                                                                                                                                                0.122476E 02 0.
0.718240E 01 0.
0.710200E 01 0.
0.121404E 02 0.
s. SATURATION COEFF=
                                                                                                                                                                                                                                                                              0.122476E 02 0.
0.282019E 02 0.
0.710200E 01 0.
0.121404E 02 0.
                                                                                                                                                                                                                                                                                                                                        0.83125
                                                                                                                                                                                                                                                                                                                                                                                                                                        0.22739E 02
                                                                                        0.39644E 01
0.0
                                                                    ERROR STANDARD DEVIATIONS VECTOR
                             (4F5.4)
                                                                                                                                                                                 TRUE SCORE DISPERSION MATRIX C- 2
                                                                                                                                                                                                                                                                                                                                                                                                                                        0.28202E 02
                                                                                        0.20459E 01 0.45847E 01
                                                                                                                                                                                                                                                                             R- 1 0.25C7C6E 02
R- 2 0.122476E 02
R- 3 0.121056 02
R- 4 0.207C21E 02
PART SCORE DISPERSION: S
                                                                                                                                                                                                                                          TRUE SCORE DISPERSION:
                                                                                                             FACTOR LOADING MATRIX
                                                                                                                                                                                                   020
                                                                                                                                                                                                                                                                                                                                                                      ERROR SCORE VARIANCE
GMEAN= 0.0
                                                                                                                               010
                                                                                                                                                                                                                                                                                                                                                             TRUE SCORE VARIANCE
                                                                                                                                                                                                                                                                                                                                                                                                            VARIANCES OF PARTS
                            FORMAT FOR THE DATA
                                                          0.0
                                                                                                                                                                                                                      0.121105E
0.207021E
                                                                                                                              0.457C00E
                                                                                                                                                 0.265000E
                                                                                                                                                                                                            0.122476E
                                                                                                                                                                                                                                                                DI SPERSION MATRIX
                                                                                                                                                                                                   0.208849E
                                                                                                                                                                                                                                                                                                                                                                                                                                         0.25071E 02
                                                                                                                                                                                                                                                                                                                                                                                         FIXED EFFECTS
                                                                                                                                                                                                                                                                                                                                          RELIABILITY
                                         MEANS VECTOR
                                                                                                                                                                                                                                                                                                                                                 AL PHA
                                                             0.0
                                                                                                                                7 4 4 L
```



UNBIASED REL EST (ANOVA)= 0.71994	0.63992
AL PHA= 0.63993	0 TT= 0
H H O	HOM/SAT≈
21E 01	0.30762
01 01 01 01 01 01 02 01 02 01	E 02 E 00 E 01 E 02 HF 02 1796 TE = 0
C- 4 0.315894E 01 -0.325838E 01 -0.318824E 01 0.122313E 01 0.247397E 01 0.104001E 01 -0.558746E 01 -0.52734E 01 -0.52782E 01 -0.433714E 01	AMPLE DISPERSION MATRIX C C C 3 C C 4 C C C C C C C C C C C C C
01 01 00 00 00 00 01 01 01 01 01 01 01 0	9E 01 8E 01 7E 01 HOMO EST
C- 3	C = 3 C1E 02 0.144443E 01 C1E 02 0.144443E 01 43E C1 0.768107E 01 37E C0 0.549751E 01 C0EFF 0.48072 HDM CRANOVA 0.02371 ES ATES UNDER ANDVA 0.01
01 01 01 01 01 01 01 01 01 01 01 01 01 0	53E 01 01E 02 43E C1 3 TE C0 C0E FF= ER ANOVA
C- 2 -0.549026E 01 -0.541119E 01 -0.833126E 01 -0.833126E 01 -0.834020TE 00 0.440201E 01 0.548926E 01 0.648926E 01 0.181339E 01 -0.375924E 01 ECTOR 3 E 01 -0.58680E 0	DISPERSION MATRIX C-2 0.174050E 02 0.205353E 01 0.205353E 01 0.17930LE 02 0.500189E 01 0.144443E C0 0.11896E 02 0.521637E C0 DISPERSION : SATURATION COEFF. E OF ALPHA ESTIMATE UNDER AND
01 -0 00 -0 00 -0 00 -0 01 -0 01 01 01 00 00 00 00 00 00 01 -0 01 01 00 00 00 00 00 01 01 00 01 00 00 00	N MATR E 02 E 01 DE 01 DE 02 DN : S/ HA EST
ATA MATRIX - 1 0.898699E 01 -0.589026E 01 0.240342E 01 - 2 -0.659240E 00 -0.541119E 01 -0.618265E 01 - 3 -0.187743E 00 -0.114643E C1 -0.463635E 01 - 4 0.815396E 00 -0.833126E 01 -0.412630E 00 - 5 0.343811E 01 -0.889207E 00 0.358485E 00 - 6 0.77583E 01 0.440201E 01 0.3504485E 00 - 7 0.227846E 01 0.340946E 01 0.179335E 01 - 8 0.307808E 00 0.648926E 00 -0.122800E 01 - 8 0.307808E 00 0.648926E 00 -0.122800E 01 - 9 0.250911E 01 0.12369E 01 0.942052E 00 - 8 0.27646E 01 0.12005E 01 -0.58680E 00 -0.13691E 00 - 19242E 01 -0.12005E 01 -0.58680E 00 -0.13691E 00 - 6 0.16093E 01 -0.15154E 01 -0.90171E 00 -0.45182E 00	SAMPLE DISPERSION MATRIX C-2 R-1 0.174050E 02 0.2053/ R-2 0.205355E 01 0.1793/ R-3 0.560189E 01 0.1444/ R-4 0.111896E 02 0.5526 SAMPLE DISPERSION : SATURATION VARIANCE OF ALPHA ESTHATE UND
DATA MATRIX C- R- 1 0.66 R- 3 -0.1 R- 4 0.8 R- 5 0.3 R- 6 0.2 R- 9 -0.2 R- 10 -0.2 R- 10 -0.2 R- 10 0.32 SAMPLE FIX SAMPLE FIX C- 10 0.15092 C- 10 0.16093E C- 10 0.16093E	SAMPLE R- 2 R- 3 R- 3 SAMPLE VARIAN



MODEL CLASS INTERVAL = 0.645833E 01 DESCRIPTIVE STATISTICS FOR MEAN SQUARES AND EXPECTED VALUES UNDER ANDVA MODEL 0.566122E 00 0.140119E 01 0.114170E 01 0.416785E 00 0.572055E 00 0.144065E 01 0.112026E 01 0.428632E 00 MINUMUM= 0.0 0000 0.140543E-01 0.225583E-C1 -0.359699E-01 -0.646006E-C3



	01 0.250000E-01	
	0.425398E INTERVAL=	
	-0.2= CLASS	
aaaaaaaaaaaaaaaaaaaaaaaaaaa a RELIABILITY STUDY aaaaaaaaaaaaaaaaaaaaaaaaa	ESTIMATION IS BASED ON ALPHA FORMULA(ANDVA,BIASED) EXPECTED FREQUENCY OF RELIABILITY ESTIMATES BELOW -0.2= 0.425398E 01 MAXIMUM= 0.99999E 00 MINUMUM= -0.2C0000E 00 CLASS INTERVAL= 0.250000E-01	

EXPECTED 0.237113E-01

TIMATES	VARIANCE DBSERVED 0.319032E-01	
Y ES	suspensive cases	•
LIT	00	001 001 002 003 003 003 003 003 003 003 003 003
REL I ABIL	PECTED 83034E	2 000000000000000000000000000000000000
FOR	0.72	100011111000000000000000000000000000000
S	MEAN 00	
STIC	3.6	1A8 1 000 000 000 000 000 001 001 0
STATI	085ERVE 0.76058	0F REL 358701E 3368701E 4386252E 540137E 601053E 601053E 601053E 1749652 110720E 11072
TIV		
RIPTIVE	COF	AR 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
DESC	REL	



		UPPER BGUND= 0.925005 UPPER B(EST)= 0.922186
		LOWER B(EST) = 0.514130 LOWER B(EST) = 0.468784
		4.40%
		80
		DFA= 9. DFE= 27.
		DF E= THAN
		9. GREATER
		.050 DFA= 9. 6.25%; GREATE
0.7800C0E 02 0.100000E 02	0.0	ALPHA ESTIMATES SIGLEVEL(EACH)=0.050 NO OF CASES LESS THAN LOWER B= 125 6
022	00	SIGI
0.864394E 0.134865E	0.100255E 00	ALPHA ESTIMATES NO OF CASES LESS
R- 46 R- 47	R- 48	ALPHA NO OF



0000000				•	• ** ** ** ** **	* •	•	• •	* * *	# # # # # # # # # # # # # # # # # # #
P.R.OB.8									*	• 1
									i	+ + + + + + + + + + + + + + + + + + +
0.881404E 02										* * * + - - - - - - - - - -
######################################										# # # + + + + + + + + + + + + + + + + +
	18.000-	16.000-1	14.000-	12.000-1	10.000-1	8 .000	9	0000	2 000-2	REL -0.



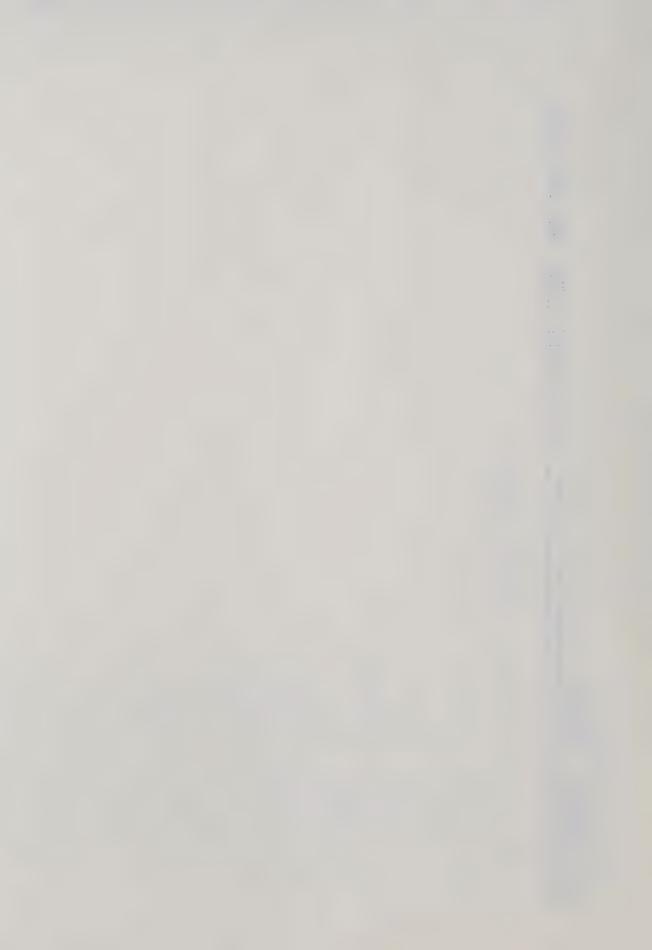
01 0.250000E-01
.UNBIASED) DW -0.2= 0.425398E CLASS INTERVAL=
OF CORRECTION(ANDVA. SILITY ESTIMATES BELG UMUM= -0.200000E 00
assasasassassasasasasasasasasasasasasa
accaca a REL I easaalaa ESTIMAT EXPECTE MAXIMUM

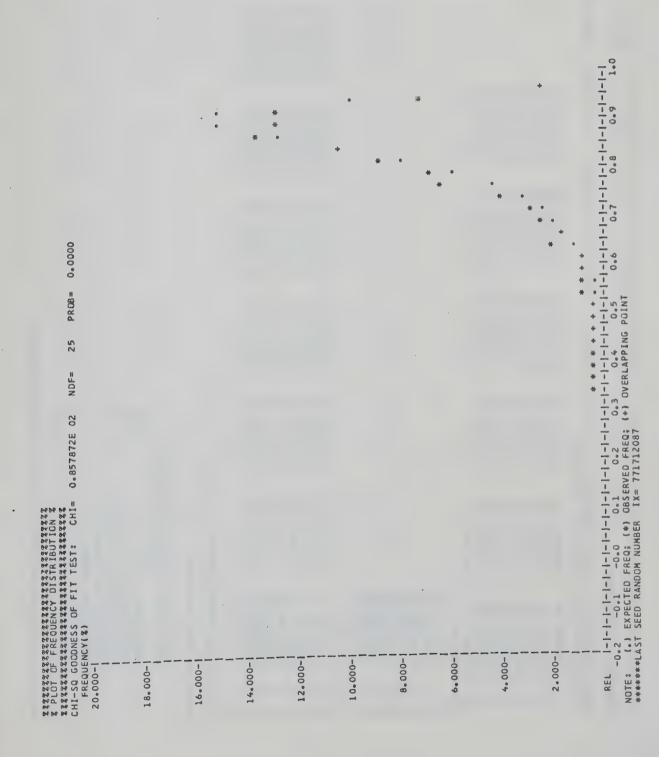
DESCRIPTIVE STATISTICS FOR RELIABILITY ESTIMATES

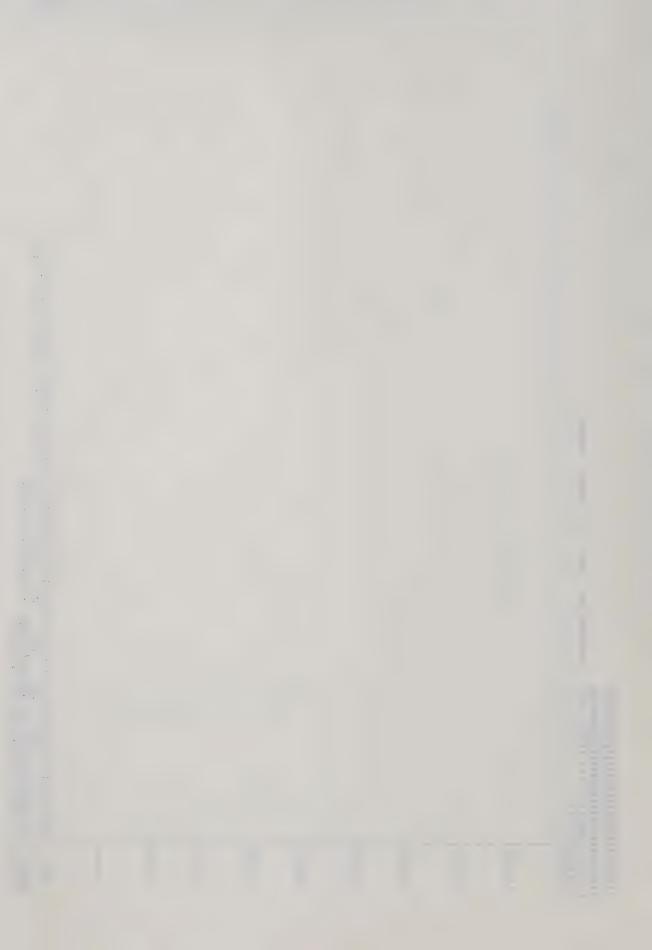
LIIT ESIIMAIES	OBSERVED EXPECTED 0.193338E-01 0.143439E-01		··•				01							01		01	01	~ 7								01	01	01	0.2	02	02	02	200	20	200	0.02		50.	53	53	200	60	7.7
FUR RELIABILITY E	EXPECTED 0.831249E		00E 0	000	0.0		OE	0.0	U	ם מ	n in	1	0.0	30E		30E	300	00 F	30E) C	11 LL	3 0	000	DOF	300E	300	300 E	U U	000	OOE	00E	00E	00 E	000	000 000 000 000 000 000 000 000 000 00	0 0	200	л (OO (000	000	00 E	000	100
STATISTICS	OBSERVED 0.813762E 00	C-1	0.252795E 01	لتا د	ш	ш	ш	ш	u i	ا لد	u u	ıщ	ш	Ш	ш	Ä	Ш	W !	H L	ח ה	n n	1 40	7 17	1 14	발	7 E	3 t	2 u	+ O	9	1 E	36	ZE	25	9 10	, r	7 5	2 2	8 1	2	9 6	7 2	d
DESCRIPTIVE	REL COF	IPARIS	N- 0	1 w	4	S	9	_	∞ (δ ;	011	12	13	14	15	16	17	8	19	20	22	22	25	25.	26	27	. 28	. 29	ر ا ا	32	- 33	- 34	- 35	. 36	. 37	00 C	77.	0 4	147	- 42	- 43	++	u,



```
UPPER BOOUND= 0.941671
UPPER B(EST)= 0.939478
                                                                           27. LOWER BOUND= 0.622101
4.40% LOWER B(EST)= 0.586832
R- 46 0.200904E 03 0.145000E 03
R- 47 0.497977E 02 0.500000E 02
R- 48 0.735044E 00 0.100000E 01
ADJUSTED ALPHA ESTIMATES SIG LEVEL(EACH)=0.050 DFA= 9. DFE=
NO DF CASES LESS THAN LOWER B= 125 6.25%; GREATER THAN UPPER B= 88
```







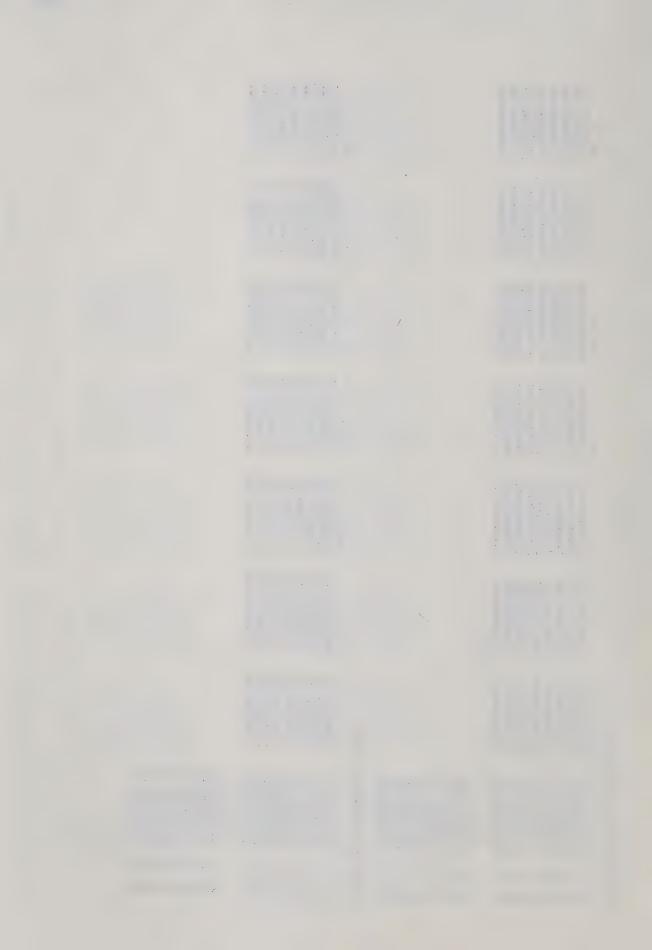
, ERROR(NO)
, LATENT(NO),
1=15, 3=9,
RS, N=1000,
AND NOVICK PARAMETERS,
NOVICK
AND
LORD

				C-8 0.259700E 0 0.380010E 0 0.290970E 0 0.315350E 0 0.339200E 0 0.252280E 0 0.280900E 0			4984	
				C- 7 0.233240E 00 0.341292E 00 0.261324E 00 0.283220E 00 0.304640E 00 0.255280E 00			KR20=0.64984	9 0.11260E-01
				C- 6 0.313600E 00 0.45880E 00 0.351360E 00 0.351360E 00 0.379520E 00 0.409600E 00 0.339200E 00 0.339200E 00 0.316800E 00		DIFF. INDEX 0.266301E 01 0.117857E 01 0.760452E 00 0.279700E 00 -0.290948E 00 -0.95823E 00 -0.159441E 01 -0.239425E 01	8E 01 REL=0.66324	8 0.24188E-01
				C-5 0.291550E 00 0.426615E 00 0.326655E 00 0.352835E 00 0.384805E 00 0.283220E 00 0.315350E 00		DISC. POWER 0.562105E 00 0.102859E 01 0.656838E 00 0.73646E 00 0.740302E 00 0.832927E 00 0.541250E 00 0.655002E 00	ERROR VAR= 0.134888E	6 0.65247E-01 0.30161E-01
				C- 4 0.290570E 00 0.425181E 00 0.325557E 00 0.351649E 00 0.379520E 00 0.314290E 00 0.314290E 00		THRES CONS. 0.130488E 01 0.845037E 00 0.417488E 00 0.165862E 00 0.725737E-01 -0.186207E 00 -0.845034E 00	0.265655E 01 E	5 0.57335E-01 0.6
10000 15 777 1 1 1 2 48 0.650	ARE NORMAL		MATRIX	C- 3 0.269010E 00 0.393633E 00 0.301401E 00 0.325557E 00 0.351366 00 0.261324E 00 0.261324E 00		VARIANCE 0.867839E-01 0.15939E 00 0.22375E 00 0.24554E 00 0.244524E 00 0.24524E 00 0.159399E 00 0.159399E 00	IVE MODEL 01 TRUE VAR=	c1 C.55859E-01
SAMPLES SIMULATED SUBJECTS IN EACH SAMPLE ITEMS NG SEED RANDOM NUMBER FOR CARD CUTPUT FOR PLOT FOR PLOT FOR PLOT FOR CLASS INTERVALS ICANCE LEVEL	SCORE DISTRIBUTIONS ARE PERCENTIONS ARE	TERS (9F5.5)	CORRELATION	C- 2 0.351330E 00 0.514089E 00 0.425181E 00 0.425181E 00 0.458830E 00 0.341292E 00 0.354915E 00		DIFFICULTY 0.960000E-01 0.199000E 00 0.434000E 00 0.471000E 00 0.574000E 00 0.676000E 00 0.801000E 00	UNDER NCRMAL OGIVE VAR= 0.400542E 01	ACES 3 3 3E-C1 0.41851E-C1
NO OF SAMPLES SIMULATED NO OF SUBJECTS IN EACH SON O OF ITEMS STARTING SEED RANDEM NUME OFFICE FOR PLOT CPTICN FOR PLOT CPTICN FOR ESTIMATION FOR OPTITON FOR CARSS INTERV.	TRUE SCORE DI ERROR SCORE D	FORMAT FOR ITEM PARAMETERS	ITEM TETRACHORIC	C- 1 0.24c10CE 00 0.351330E 00 0.26910E C0 0.291550E 00 0.291550E 00 0.23240E 00 0.259700E 00	C-242550E 00 C-242550E 00 C-274315E 00 C-29535E 00 0-294525E 00 C-28560E 00 C-28560E 00 C-28560E 00	AR AMETERS BIS COR 0.49000CE 00 0.7170CCE 00 0.5930CCE 00 0.5950CE 00 0.4960CCE 00 0.4960CCE 00 0.4960CCE 00	POPULATION PARAMETERS MEAN= 0.447100E 01	PARALLEL ITEM CCVARIANCES 0.84335E-02 0.48553E-01
		FORMAT	INTER	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	111 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	POPULA MEAN=	PARALI 0.84

00000000



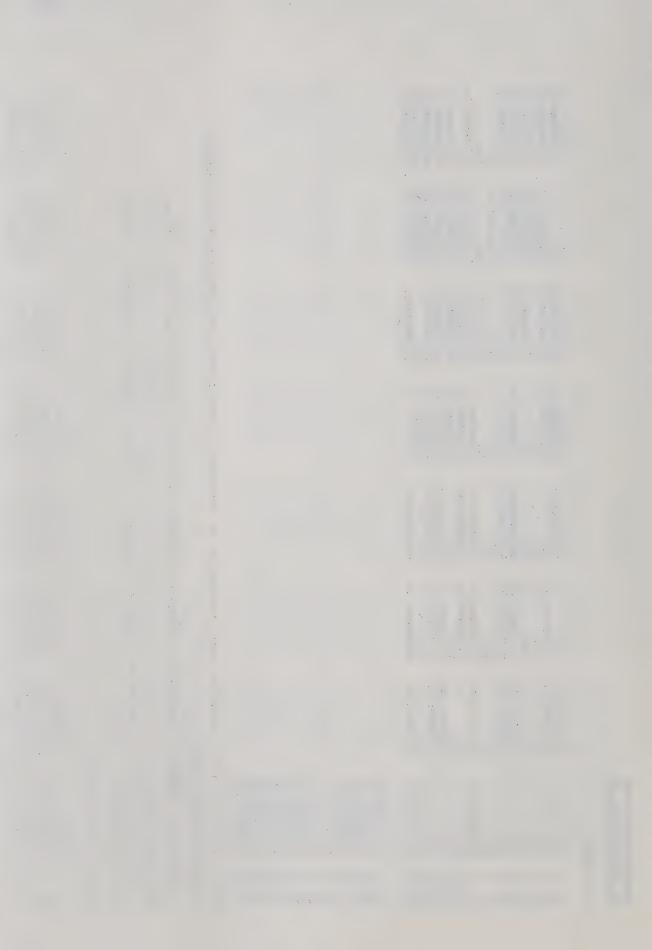
	C- 8 0.105217E-01 0.253891E-01 0.2381887E-01 0.383725E-01 0.26539F-01 0.159399E 00 0.164002E-01		C- 8 0.894592E-01 0.159280E 00 0.171161E 00 0.174750E 00 0.12735E 00 0.100000E 01
	C- 7 0.131971E-01 0.319959E-01 0.399012E-01 0.40617E-01 0.219024E 00 0.266539E-01 0.177800E-01		C- 7 0.95723E-01 0.17240E 00 0.152316E 00 0.17623E 00 0.100395E 00 0.100000E 01 0.142650E 00
	C- 6 0.198603E-01 0.485968E-01 0.595758E-01 0.507093E-01 0.44624E 00 0.44627E 00 0.24524E 00 0.252626E-01		0.13634E 00 0.246152E 00 0.215822E 00 0.243084E 00 0.1000000 01 0.190395E 00 0.194365E 00 0.198359E 00
	C- 5 0.198224E-01 0.484471E-01 0.485011E-01 0.565456E-01 0.249159E 00 0.249159E 00 0.348256E-01 0.348256E-01		C-5 0.134803E 00 0.24101E 00 0.205412E 00 0.228564E 00 0.245955E 00 0.174453E 00 0.174453E 00
	C- 4 0.198965E-01 0.486104E-01 0.245644E 00 0.545545E-01 0.399012E-01 0.338688E-01 0.220045E-01		C- 4 0.136271E 00 0.245659E 00 0.205174E 00 0.100000E 01 0.228564E 00 0.17223E 00 0.17223E 00 0.175226 00
	C- 3 0.178805E-01 0.434545E-01 0.223756E 0C 0.481019E-01 0.504828E-01 0.337193E-01 0.281987E-01 0.181952E-01		C- 3 0.12813E 00 0.230094E 00 0.10000E 01 0.20517E 00 0.21582E 00 0.15216E 00 0.15216E 00
MATRIX	C- 2 0.199748E-01 0.159399E 00 0.434545E-01 0.48471E-01 0.48568E-01 0.319559E-01 0.253891E-01 0.159269E-01	MATRIX	C- 2 0.169832E 00 0.100000E 01 0.236034E 00 0.24565E 00 0.246152E 00 0.11246E 00 0.115926 00 0.123656E 00
ITEM DISPERSICA	C- 1 0.867839E-01 0.193748E-01 0.19865E-01 0.19865E-01 0.19863E-01 0.198603E-01 0.198603E-01 0.198637E-02 C- 4 0.664337E-02 C- 5 0.664337E-02 C- 5 0.664337E-02 C- 5 0.664337E-02 C- 5 0.66437E-01 0.181952E-01 C-220645E-01	ITEM CORRELATION	C- 1 0.100000E 01 0.165812E 00 0.128313E 00 0.136271E 00 0.13634E 00 0.13634E 00 0.957223E-01 0.6996592E-01 0.699626E-01 0.699626E-01 0.699626E-01 0.11762E 00 0.117764E 00 0.117764E 00 0.117764E 00 0.117764E 00 0.117764E 00 0.117764E 00
INTER		INTER I	7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2



	C-8 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.0 0.0 0.0 0.0 0.100000E 01 0.0 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01		0.81647					C-8 0.285715E-01 0.114286E 00 0.428572E-01 0.428572E-01
	C- 7 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.0 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01		REL EST(ANOVA)=	9 00 0.31111E 00	9 00 0.93333E 00			C-7 0.285715E-01 -0.285714E-01 0.4285714E-01 -0.285714E-01 0.571429E-01
	C- 6 0.100000E 01 0.100000E 01 0.100000E 01 0.00000E 01 0.100000E 01		0.78588 UNBIASED	8 18 00 0.17778	8 00 = 00 0.80000E			C-6 0.380953E-01 0.809524E-01 0.809524E-01 0.809524E-01
	C- 5 0.100000E 01 0.0 0.100000E 01 0.0 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01		01 KR20=	6 0.11111E 00 0.17778E	6 0.73333E 00 0.80000E			C- 5 -0.142857E-01 0.857143E-01 0.857143E-01 0.857143E-0
	C- 4 0.100000E 01 0.0 0.0 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01		E 00 F= 0.467038E	-0.22222E-01 0.1	5 0.60000E 00 0.			C- 4 0.666667E-01 0.19523E 00 0.19523E 00 0.26667E 00 0.857143E-01
	C- 3 0.0 0.1 0.0 0.1 0.0 0.100000E 01 0.0 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01 0.100000E 01		MSE= 0.142064E	4 -0.88889E-01	4 00 0.53333E 00			C- 3 0.66667E-01 0.19523E 00 0.19523E 00 0.19528E 00
	C- 2 C-100000E 01 C-0 C-100000E 01 C-100000E 01 C-100000E 01		MSB= 0.816666E 00	/ECTOR 3 3 7E-01 -0.88889E-01	3 00 0.53333E		XIX	C- 2 0.666667E-01 0.26667E 00 0.155238E 00 0.195238E 00 0.897143E-01
MATRIX	C- 1 0.0 2 0.0 3 0.0 6 0.0 6 0.0 0.0 0 10 0.0 0 11 0.0 0 12 0.0 0 13 0.0 0 14 0.0 0 15 0.1000CCCE 01	C- 9 1 0.100000E 01 2 C.100000E 01 4 0.100000E 01 5 0.100000E 01 6 0.100000E 01 7 0.0 0.100000E 01 10 0.100000E 01 11 0.100000E 01 12 C.100000E 01 13 0.100000E 01 14 C.100000E 01 15 C.100000E 01 16 0.100000E 01 17 0.100000E 01 18 0.100000E 01 18 0.100000E 01 19 0.100000E 01 19 0.100000E 01	0.663491E 00	AMPLE FIXED EFFECTS VECTOR 1 2 -0.48889E 00 -0.88889E-01	SAMPLE MEANS VECTCR 1 0.13333E CO 0.53333E	AN= C.622222E 00	SAMPLE DISPERSION MATRIX	C- 1 0.1238C9E 00 2 0.66667E-01 3 C.66667E-01 4 C.66667E-01 5 -C.142 E57E-01
DATA	RA-110 RA-120 RA-110 RA-111 RA-111 RA-114 RA-114	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	MSA=	SAM	SAM	GMEAN	SAM	44444

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acceddescacasacasasaga a EXAMPLE RUNS adacasasagasaga



0.14295-01 0.171429E 00 0.571429E-01										
0.171429E-01 0.171429E 00 0.285715F-01 -0.142857E-01										
0.209524E 00 0.142858E-01 0.142858E-01 0.523810E-01								HOM/SAT= 0.78588		
0.100000E 00 0. 0.571429E-01 0. 0.571429E-01 0.										
								0.28968		0.01015
0.809524E-01 -0.285714E-01 0.428572E-01 0.380953E-01								HOMOGENEITY COEFF= 0.28968	ESTIMATE= 0.01382	11 ESTIMATE= 0.01015
0.809524E-01 0.428572E-01 0.428572E-01 0.380953E-01								0.36861 HOMO		ER ANOVA= 0.025
0.809524E-01 -0.285714E-01 0.114286E 00 0.380953E-01								SAMPLE DISPERSION : SATURATION COEFF=	VARIANCE CF ALPHA ESTIMATE UNDER ANDVA= 0.03418	VARIANCE OF UNBIASED REL ESTIMATES UNDER ANOVA = 0.02511
C.380953E-C1 0.285715E-01 C.285715E-01 C.952387E-02	C- 9 0.952387E-02	C.380953E-01 C.380953E-C1	C.380553E-01	C.523810E-01	-C.142857E-01	C.571429E-01	0.666667E-01	DISPERSION : S	CE CF ALPHA EST	CE OF UNBIASED
0 × 80		2 m	44		1	00	6 -	AMPLE	ARIAN	ARIAN
~ ~ ~ ~	ď	7 7	4 0	K &	R-	R-	R-	S	>	>

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0.346575E-01
0.304775E-01
0.395566E-01
0.277025E-01
0.162708E 00
                                                                                                                                                                                        0.991945E-02
                                                                                                                                                                                                  0.260814E-01
                                                                                                                                                                                                           0.282287E-01
                                                                                                                                                                                  J
                                                                                                                                              0.87083E-02 0.48487E-01 0.41387E-01 0.54685E-01 0.55598E-01 0.63736E-01 0.30410E-01 0.26373E-01 0.99993E-02
                                                                                                             00
                                                                                                                                                                                                                     0.411540E-01
0.382344E-01
0.429300F-01
                                                                                                                                                                                                   0.305593F-01
                                                                                                                                                                                                                                                0.220295E 00
                                                                                                                                                                                                                                                       0.277025E-01
0.146291E-01
                                                                                                                                                                                         0.122824E-01
                                                                                                                                                                                                             0.347098E-01
                                                                                                             0.88019E
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                                                                                                              0. 79547E 00
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0.520097E-01
0.629970E-01
                                                                                                                                                                                                                               0.592914E-01
0.244388E 00
0.429300E-01
0.395566-01
                                                                                                                                                                                            0.189699E-01
                                                                                                               0.67239E 00
                                                                                                                                                                                                                       0.533376E-01
0.248759E 00
0.592914E-01
0.382344E-01
0.304775E-01
                                                                                                                                                                                             0.189250E-01
0.491804E-01
                                                                                                                                                                                                               0.493367E-01
                                                                                                               0.57502E 00
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0.533376E-01
0.629970E-01
0.411540E-01
0.346575E-01
                                                                                                                                                                                               0.198933E-01
0.467094E-01
0.480815E-01
                                                                                                                 0°46454E 00
0.223009E
0.48C815E-01
0.493367E-01
0.520097E-01
                                                                                                                  0.43157E 00
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0.183737E-01
                                                                                                                                                                                                         0.428272E-01
                                                                                                                                                                                         C- 3
0.175817E-01
                                                                                                                     0.33566E 00
                                                                                                                                                                                                                                              C.459484E-01
0.305593E-01
C.260814E-01
0.163475E-01
                                                                                                                                                                                                           0.159891E 00
                                                                                                                                                                                                                    C.428272E-01
0.467C94E-01
                                                                                                                                                                                                                                     0.491804E-01
                                                                                                                                                                                                   0.203735E-01
                             01
                                     1001
                                              0.263039E
                                     0.398767E
                             0.445068E
                                                               0.659631
                                                                                                                                                                         WITHIN TEST DISPERSION MATRIX
                                                                                                                     0.19980E 00
                                                                                                                                      PARALLEL ITEM CCVARIANCES
                                                                                                                                                                                                                                                                                                                                                       C.146291E-01
0.156557E-01
0.105465E 00
                                                                                                                                                                                                                                                                 C.991945E-02
C.731126E-02
                                                                                                                                                                                                                                                                                                    C.731126E-02
                                                                                                                                                                                                                                                                                                             C.163475E-01
                                                                                                                                                                                                                                                                                                                     0.183737E-01
                                                                                                                                                                                                                                                                                                                              C.225386E-C1
O.210272E-01
                                                                                                                                                                                                                                                                                                                                               C.236761E-01
                                                                                                                                                                                                                                               C.185699E-01
                                                                                                                                                                                                     C.868199E-01
C.203735E-01
                                                                                                                                                                                                                      C.175817E-01
C.198933E-01
                                                                                                                                                                                                                                        C.189250E-01
                                                       ERROR VARIANCE
                                                                                                                       0.96037E-01
                                                 TRUE VARIANCE
                                                                   RELIABILITY
                                                                                   NO OF CASES
                                                                                                      MEAN VECTOR
                                        VARIANCE
                                                                                                                                                                                                                                                                                                       654321
                                                                                                                                                                                                        10 m 4 m 9 m
                                                                            KR20
                                                                                                                                                                                                                                                                                                       * 1 1 1 1 1 1 1 1 1
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			Ti .
			MODEL
CLASS INTERVAL= 0.208333£ 00	ND EXPECTED VALUES UNDER ANOVA MODEL	VARIANCE EXPECTED 0.1936.03E-01 0.280450E-01 0.674.78E-01 0.838956E-01 0.261996E-C3 0.406131E-03	TIMATES AND EXPECTED VALUES UNDER M.F. VARIANCE 0.555131E-02 0.657102E-02 0.101086E-01 0.111262E-01 0.102499E-01 0.102542E-01 0.881981E-02 0.652150E-02 0.652150E-02 0.652150E-02 0.652150E-02 0.652150E-02
MAXIMUM= 0.100000E 02 MINUMUM= 0.0	DESCRIPTIVE STATISTICS FOR MEAN SQUARES AND EXPECTED VALUES UNDER ANOVA MODEL	MEAN EXPECTED 1 CONTROL 1	DISCRIPTIVE STATISTICS FOR FIXED EFFECT ESTIMATES AND EXPECTED VALUES UNDER M.F. EXPECTED ACAN



FSTIMATION IS BASED ON ALPHA FORMULA (ANDVA, BIASED)

0.250000E-01 0.522107E 01 CLASS INTERVAL= -0° 5= EXPECTED FREQUENCY OF RELIABILITY ESTIMATES BELCM MINUMUM= -0.2000C0E 00 00 3565656°0 MAXIMUM=

DESCRIPTIVE STATISTICS FOR RELIABILITY ESTIMATES

0.349162E-01 EXPECTED VAR I ANCE 0,319971E-01 OB SERVED 00 EXPECTED 0.602903E MEAN 0.599975E 00 OBSERVED REL COF

CCMPARISCN OF RELIABILITY

010 01 01 10 01 0.0 0.0 0.1 0.1 0.300COCE 0.8COCOOE 0.0 0.0 0.200000E 0.300COOE C.400000E 0.500000E 0.10000E 0.3000CE C.400000E C.168568E C.193447E C.395900E C.990212E C.2556C9E C.341797E C.459439E C.534123E C.147176E 0.222385E 0.256175E C.128729E C.767112E C.870764E C.676930E C.598371E 10 113 113 114 116 119 20

0.360000E C.750C00E 0.710000E 0.790000E C. 900000E 0.1600COE 0.260000E 0.37000E C. SCOCCCE 0.500COOE 0.800000E O.180CCCE 0.160CCOE 0.150000E 0.250000E C.390COCE 0.420COOE 02 02 020 02 0000 0.847512E C.991344E

0.1

C.621986F 0.7255CZE C.116101E C.136085E

02 0.528896E 0.361113E C.159593E C.187183E C.257CCOE C. 300362E 0.349560E C.405E83E C.467727E 0.534252E C.6 C2558E C.669530E C.727401E C.767285E C.777565E C.745869E C.662886E C.219453E 444444 2222

0.870COOE 0.75000E

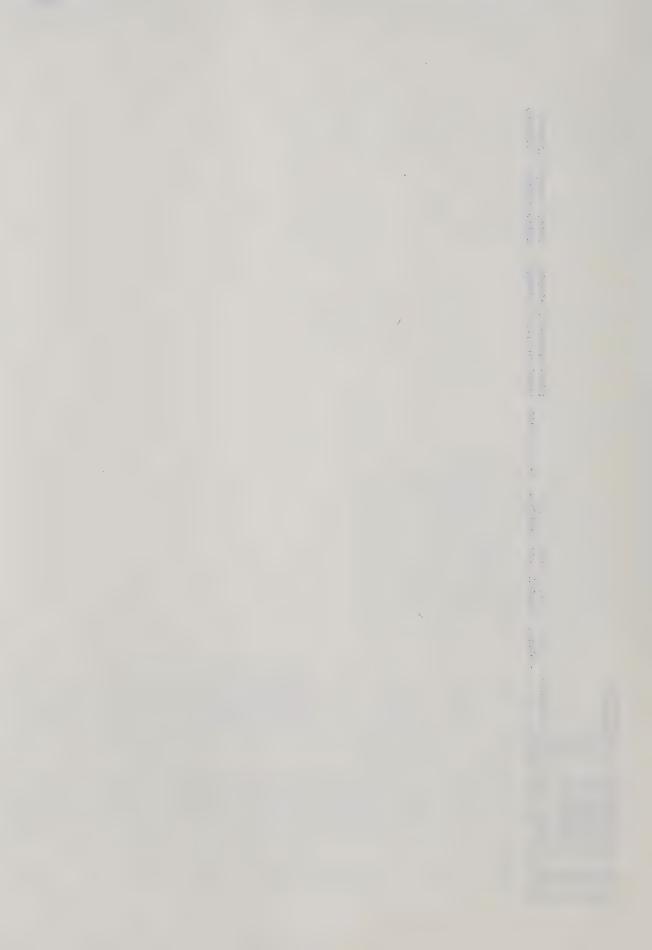
0.820000E

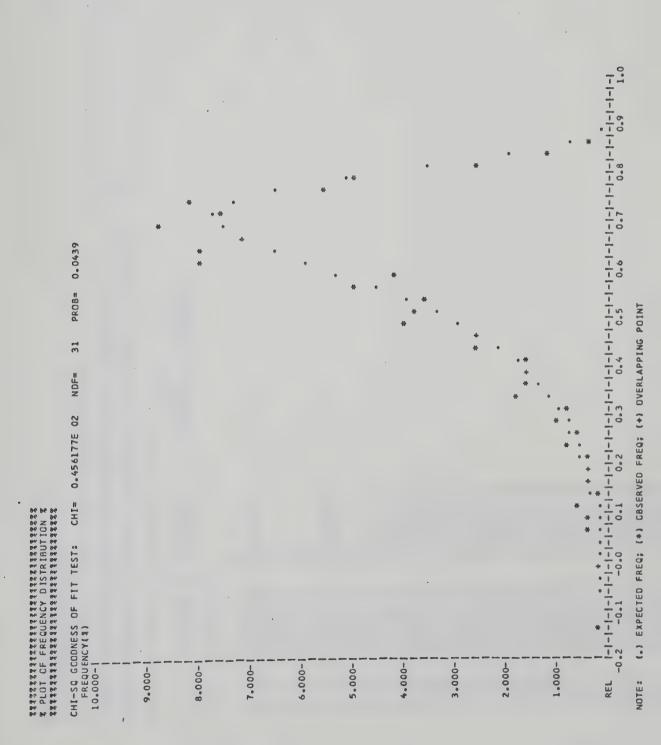
0.560000E

0.260000E



						UPPER BOUND= 0.808942	UPPER B(EST)= 0.796666
						.050 CFA= 14. DFE= 112. LOWER BOUND= 0.257551 UPPER BOUND= 0.808942	LOWER B(EST)= 0.290827
							2.90%
							29
						112.	JPPER B=
						DFE=	THAN C
						0.050 CFA= 14. DFE= 112.	GREATER
						CFA=	.00%
0.110CCCE 02 0.300000E 01	0.0	0.0	0.0	0.0	0.0	SIGLEVEL(EACH)=0.050	40
02	01	00	-02	+0-		SIGLE	THAN 1
C.195656E 02 C.743502E 01	C.160366E 01	C.1337538	0.196695E-02	C.596C46E-04	0.0	ESTIMATES	NO OF CASES LESS THAN LOWER B=
R- 42 R- 43	R- 44	R- 45	R- 46	R- 47	R- 48	ALPHA	NO OF







ESTIMATION IS BASED ON KRISTOF CORRECTION(ANDVA, UNBIASED)

MAXIMUM= 0.959999E 00 MINUMUM= -0.200000E 00 CLASS INTERVAL= 0.250000E-01 EXPECTED FREQUENCY OF RELIABILITY ESTIMATES BELCW -0.2= 0.522107E 01

DESCRIPTIVE STATISTICS FOR RELIABILITY ESTIMATES

OBSERVED EXPECTED 0.657105E 00 0.659631E 00 MEAN REL COF

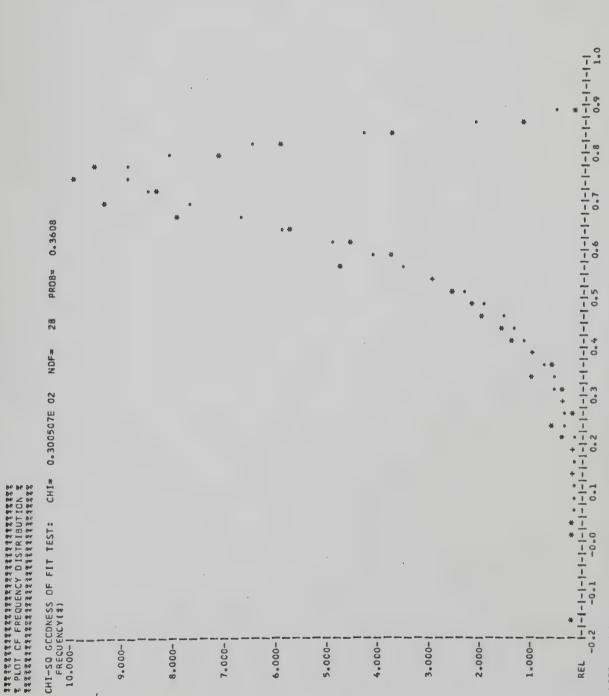
CCMPARISON OF RELIABILITY

	01					100				01		010	01	01	01	70	70	10	0	02	02	02	05	05	02	02	020	2 6	70	70	2 0	0.5	05	02	02	02	70
117	() · ·	000	0 0		0.	0 0			0		0	2000002	4000000	000009	1000001	0.400000E	300000	900000	0000009	100000	130000	.150000	.20000	.210000	.250000	.30000	480000	0000085	0000000	0000016.	. 190000	240000	.84000C	000066	.950000	.720000	.590000
ABIL	000	800	000	00	000	000	010	01	01	01	01	010	01	0	01	010	70	0	07	01	05	02	02	02	02	02	020	200	70	20	20	02	02	02	02	02	20
ISCN OF RELI	263560E 316441E	1085E 2703E	4 12844E 542819E	624478E	719565E	832021E	111884E	130212E	151902E	177658E	208282E	244E38E	288522E	340E85E	403786E	479501E	57079BE	681144E	814652E	576372E	.117233E	140983E	169718E	204423E	246159E	296C31E	,355C71E	42403CE	502901E	,590509E	568333E	774779E	853160E	901400E	.857648E	820366E	,660273E
TAK	~ ~	m 4 11	v 0	-	8	9		12	13	14	12	16	11	18	19	20	77	22	23	24	25	26	27	28	29	30	31	35	33	34	35	36	37	38	39	40	7 4 1
2	22	4 4 6	x x	å.	2	<u>.</u> .	<u>_</u>	4	2	<u>۳</u>	2	7	2	2	ď	2 0	X (2	<u>*</u>	4	4	8	2	2	7	<u>*</u>	<u>.</u>	¥ c	¥ 1	× (X i	4	ď	2	2	2	¥



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UPPER BOOUND= 0.836236
UPPER B(EST)= 0.825714
                                                                                                                                                                     LOWER BUND= 0.363615
LOWER B(EST)= 0.392137
                                                                                                                                                                     112.
R- 42 0.438172E 02 0.380000CE 02
R- 43 C.214796E C2 0.120000E 02
R- 44 C.641647E 01 0.200000E 01
R- 45 C.820398E 00 0.0
R- 45 C.8203998E 00 0.0
R- 46 C.218749E-01 0.0
R- 47 C.0 0.0
R- 48 C.596046E-04 0.0
R- 48 C.596046E-04 0.0
R- 48 C.595076E-04 0.0
ADJUSTED ALPHA ESTIMATES SIG LEVEL(EACH)=0.050 DFA= 14. DFE= NO DF CASES LESS THAN LOWER B= 40 4.00%; GREATER THAN UPPER B= 29
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NOTE: (.) EXPECTED FREG; (*) CBSERVED FREG; (+) OVERLAPPING POINT









B30002